

MASH TL-3 TESTING AND EVALUATION OF A STEEL BRIDGE RAIL WITH PICKETS



Test Report 9-1002-12-2

Cooperative Research Program

TEXAS A&M TRANSPORTATION INSTITUTE THE TEXAS A&M UNIVERSITY SYSTEM COLLEGE STATION, TEXAS

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16. Abstract			
TxDOT has a need for a steel bridge rail that anchors to a concrete curb with an aesthetic appearance using steel pickets. Bridge railings that use pickets (concrete and steel) have exhibited undesirable safety			

performance characteristics. The purpose of this portion of the project was to design and evaluate a steel bridge rail with pickets that would meet the strength and safety performance criteria for Test Level 3 (TL-3) of MASH. The bridge rail tested for this project was similar to the Wyoming 2-tube bridge rail that was successfully crash tested under NCHRP Report 350 criteria (Texas Transportation Institute [TTI] Project No. 472610-4, dated May 1996). Details from the Wyoming 2-Tube design were incorporated and used in the design of the new TxDOT Picket Rail.

The TxDOT Picket Rail evaluated and presented herein met all the safety performance criteria for MASH TL-3 and is suitable for implementation on new bridge construction.

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MASH TL-3 TESTING AND EVALUATION OF A STEEL BRIDGE RAIL WITH PICKETS

by

William F. Williams, P.E. Associate Research Engineer Texas Transportation Institute

Roger P. Bligh, P.E. Research Engineer Texas Transportation Institute

and

Wanda L. Menges Research Specialist Texas Transportation Institute

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DISCLAIMER

This research was performed in cooperation with the Texas Department of Transportation (TxDOT) and the Federal Highway Administration (FHWA). The contents of this report reflect the views of the authors, who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official view or policies of the FHWA or TxDOT. This report does not constitute a standard, specification, or regulation, and its contents are not intended for construction, bidding, or permit purposes. In addition, the above listed agencies assume no liability for its contents or use thereof. The United States Government and the State of Texas do not endorse products or manufacturers. Trade or manufacturers' names appear herein solely because they are considered essential to the object of this report. The engineer in charge of the project was Roger P. Bligh, P.E. (Texas, #78550).

TTI PROVING GROUND DISCLAIMER

The results of the crash testing reported herein apply only to the article being tested.



Wanda L. Menges, Research Specialist Deputy Quality Manager

Richard A. Zimmer, Senior Research Specialist Test Facility Manager Quality Manager Technical Manager

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CHAPTER 1. INTRODUCTION

1.1 INTRODUCTION

This project was set up to provide Texas Department of Transportation (TxDOT) with a mechanism to quickly and effectively evaluate high-priority issues related to roadside safety devices. Roadside safety devices shield motorists from roadside hazards such as non-traversable terrain and fixed objects. To maintain the desired level of safety for the motoring public, these safety devices must be designed to accommodate a variety of site conditions, placement locations, and a changing vehicle fleet. Periodically, there is a need to assess the compliance of existing safety devices with current vehicle testing criteria and develop new devices that address identified needs.

Under this project, roadside safety issues are identified and prioritized for investigation. Each roadside safety issue is addressed with a separate work plan, and the results are summarized in an individual test report.

1.2 BACKGROUND

The American Association of State Highway Transportation Officials (AASHTO) published the *Manual for Assessing Safety Hardware (MASH)* in October 2009 (1). *MASH* supersedes *National Cooperative Highway Research Program (NCHRP) Report 350* (2) as the recommended guidance for the safety performance evaluation of roadside safety features.

1.3 OBJECTIVES/SCOPE OF RESEARCH

TxDOT has a need for an aesthetic steel bridge rail that incorporates steel pickets and anchors to a concrete curb. The purpose of this portion of the project was to design and evaluate a steel bridge rail with pickets that would meet the strength and safety performance criteria for Test Level 3 (TL-3) of *MASH*. The bridge rail tested for this project was similar to the Wyoming 2-tube bridge rail that was successfully crash tested under *NCHRP Report 350* criteria (Texas Transportation Institute [TTI] Project No. 472610-4, dated May 1996) (*3*). Details from the Wyoming 2-tube design were incorporated and used in the design of the new TxDOT Picket Rail.

The testing reported here assesses the performance of the TxDOT Picket Rail according to the safety-performance evaluation guidelines included in *MASH* for TL-3. Two tests are required to evaluate the bridge rail: one test with a 2425 lb vehicle and a second test with a 5000 lb pickup truck, both impacting the critical impact point of the length of need of the bridge rail at a nominal impact speed and angle of 62 mi/h and 25 degrees, respectively. The report includes details of the TxDOT Picket Rail, details of the crash tests performed, and evaluation of the tests according to *MASH*.

CHAPTER 2. SYSTEM DETAILS

2.1 TEST ARTICLE DESIGN AND CONSTRUCTION

The TxDOT Picket Rail consists of three tubular steel rail elements supported by fabricated steel plate posts. The overall length of the test installation was 92 ft and consisted of 12 posts spaced 8 ft on centers. The total height of the bridge rail is 36 inches above the pavement surface. The steel bridge rail was anchored to a 14-inch wide by 9-inch high cast-in-place concrete curb. The concrete curb was anchored to a cast-in-place 8-inch thick concrete deck cantilever. The width of the cantilever was 30 inches. Mr. John Holt with TxDOT provided detailed design information on the bridge rail.

The top rail element was an A500 Grade B 4-inch diameter pipe (0.174-inch wall thickness). The lower two rail elements were A500 Grade B HSS6 $\times 2\times \frac{1}{4}$ steel tubes. The heights from the pavement surface to the top of the rail elements were 18 inches, 28 inches, and 36 inches for the lower, middle, and top rail elements, respectively. Each rail element was attached to each post using a ¹/₂-inch diameter A36 bent U-Bolt. The steel posts consisted of two ³/₄-inch thick plates welded to a ³/₄-inch thick base plate. The steel plates used to fabricate the steel posts were 9 inches wide at the base, 3³/₄ inches wide at the top, and 26 inches high (including the width of the ³/₄-inch thick baseplate). The post plates were notched 3¹/₄ inches for the lower two rail elements and $2\frac{1}{4}$ inches for the top rail element. The post base plates consisted of 12-inch \times 14-inch \times ³/₄-inch thick A572 Grade 50 material. The posts were anchored to the concrete curb using four $\frac{7}{8}$ -inch diameter $\times 10\frac{1}{2}$ inches long A325 bolts with a ¹/₄-inch thick anchor plate. These anchor bolts were cast in the curb, with the top of the concrete deck supporting the hex heads. Steel pickets were located on the field side face of the bridge rail. These pickets consisted of $\frac{5}{8}$ -inch square $\times 22^{\frac{3}{4}}$ -inch long A36 steel bars that were located on 6-inch centers and were bolted to the rail in panel sections measuring approximately 73 inches long.

For this project, a concrete bridge deck cantilever and curb was constructed immediately adjacent to an existing concrete runway located at the TTI Proving Ground test facility. The total length of the installation was 92 ft long. The bridge deck cantilever was 30 inches wide and 8 inches thick. Reinforcement in the deck consisted of two layers of reinforcing steel placed in the transverse and longitudinal directions. The top transverse reinforcement consisted of #5 bars located on 6-inch centers. Longitudinal reinforcement in the bottom layer consisted of fthree #4 bars on 9-inch centers. The bottom transverse reinforcement consisted of four #5 bars, three of which were spaced on 12-inch centers, with the two bars closest to the field side edge of the deck spaced approximately 3½ inches on centers. Vertical reinforcement in the top consisted of #5 stirrups located on 6-inch centers. Two longitudinal #5 bars were located within the top corners of the curb stirrups. For additional information on the bridge railing test installation, please refer to Figures 2.1 and 2.2, and Appendix A. Figure 2.3 shows photographs of the installation before testing.



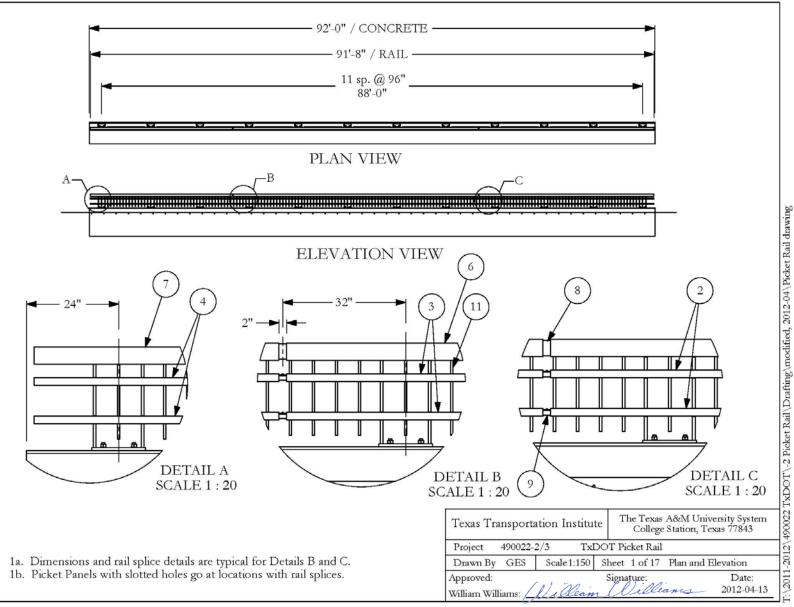


Figure 2.1. Details of the TxDOT Picket Rail Installation.

4

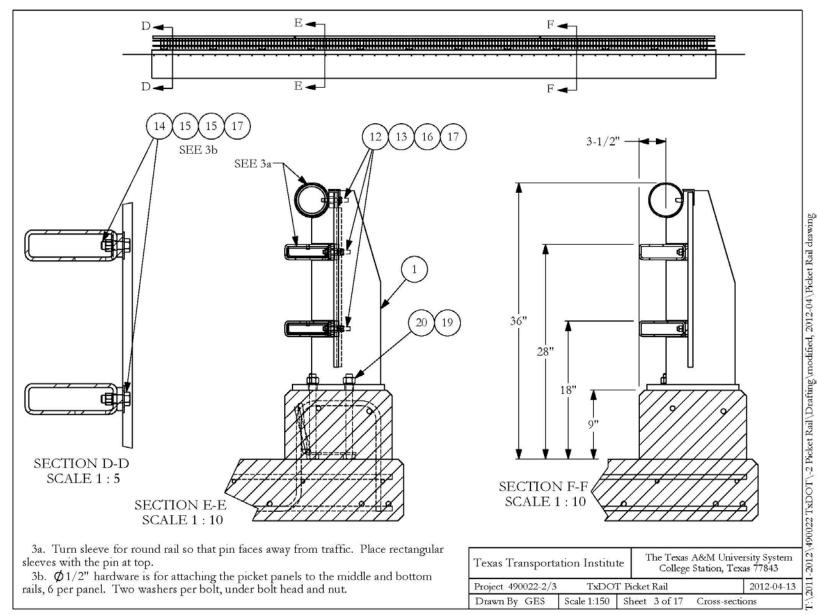


Figure 2.2. Cross Section of the TxDOT Picket Rail Installation.



Figure 2.3. TxDOT Picket Rail before Testing.

2.2 MATERIAL SPECIFICATIONS

All reinforcement used in the concrete deck had a specified yield strength of 60 ksi. The concrete deck and curb has a specified concrete strength of 4000 psi. Concrete compressive strength tests were performed on the day of the first crash test. The tests performed at 19 days of age on the concrete deck, resulted in an average compressive strength of 5506 psi. The tests performed at 11 days of age on the concrete curb resulted in an average compressive strength of 3837 psi.

CHAPTER 3. TEST REQUIREMENTS AND EVALUATION CRITERIA

3.1 CRASH TEST MATRIX

According to *MASH*, two tests are recommended for evaluation of longitudinal barriers to test level three (TL-3).

- *MASH* Test 3-10: A 2425 lb vehicle impacting the critical impact point (CIP) of the length of need (LON) of the barrier at a nominal impact speed and angle of 62 mi/h and 25 degrees, respectively. This test investigates a barrier's ability to successfully contain and redirect a small passenger vehicle.
- *MASH* Test 3-11: A 5000 lb pickup truck impacting the CIP of the LON of the barrier at a nominal impact speed and angle of 62 mi/h and 25 degrees, respectively. This test investigates a barrier's ability to successfully contain and redirect light trucks and sport utility vehicles.

Both of these tests were performed on the Picket Rail. The critical impact points for each test were determined using *MASH* guidelines. Target impact point for *MASH* test 3-10 was 3.6 ft upstream of post 9; for *MASH* Test 3-11, it was 4.3 ft upstream of post 4.

The crash test and data analysis procedures followed the guidelines presented in *MASH*. Chapter 4 presents brief descriptions of these procedures.

3.2 EVALUATION CRITERIA

The crash test was evaluated in accordance with the criteria presented in *MASH*. The performance of the TxDOT Picket Rail is judged on the basis of three factors: structural adequacy, occupant risk, and post impact vehicle trajectory. Structural adequacy is judged on the ability of the TxDOT Picket Rail to contain and redirect the vehicle. Occupant risk criteria evaluate the potential risk of hazard to occupants in the impacting vehicle and, to some extent, other traffic, pedestrians, or workers in construction zones, if applicable. Post-impact vehicle trajectory is assessed to determine potential for secondary impact with other vehicles or fixed objects, creating further risk of injury to occupants of the impacting vehicle and/or risk of injury to occupants in other vehicles. The appropriate safety evaluation criteria from Table 5-1 of *MASH* were used to evaluate the crash tests reported here, and are listed in further detail under the assessment of each crash test.

CHAPTER 4. CRASH TEST PROCEDURES

4.1 TEST FACILITY

The full-scale crash test reported here was performed at Texas A&M Transportation Institute (TTI) Proving Ground, an International Standards Organization (ISO) 17025 accredited laboratory with American Association for Laboratory Accreditation (A2LA) Mechanical Testing Certificate 2821.01. The full-scale crash test was performed according to TTI Proving Ground quality procedures and according to the *MASH* guidelines and standards.

The TTI Proving Ground is a 2000-acre complex of research and training facilities located 10 miles northwest of the main campus of Texas A&M University. The site, formerly an Air Force base, has large expanses of concrete runways and parking aprons well-suited for experimental research and testing in the areas of vehicle performance and handling, vehicle-roadway interaction, durability and efficacy of highway pavements, and safety evaluation of roadside safety hardware. The site selected for construction and testing of the TxDOT Picket Rail evaluated under this project was along the edge of an out-of-service apron. The apron consists of an unreinforced jointed-concrete pavement in 12.5 ft by 15 ft blocks nominally 6 inches deep. The apron is over 50 years old, and the joints have some displacement, but are otherwise flat and level.

4.2 VEHICLE TOW AND GUIDANCE PROCEDURES

The test vehicles were towed into the test installation using a steel cable guidance and reverse tow system. A steel cable for guiding the test vehicles was tensioned along the path, anchored at each end, and threaded through an attachment to the front wheel of the test vehicle. An additional steel cable was connected to the test vehicle, passed around a pulley near the impact point, through a pulley on the tow vehicle, and then anchored to the ground such that the tow vehicle moved away from the test site. A two-to-one speed ratio between the test and tow vehicle existed with this system. Just prior to impact with the installation, the test vehicle was released to be free-wheeling and unrestrained. The vehicle remained free-wheeling, i.e., no steering or braking inputs, until the vehicle cleared the immediate area of the test site, at which time brakes on the vehicle were activated to bring it to a safe and controlled stop.

4.3 DATA ACQUISITION SYSTEMS

4.3.1 Vehicle Instrumentation and Data Processing

The test vehicles were instrumented with a self-contained, on-board data acquisition system. The signal conditioning and acquisition system is a 16-channel, Tiny Data Acquisition System (TDAS) Pro that Diversified Technical Systems, Inc. produced. The accelerometers, measuring the x, y, and z axis of vehicle acceleration, are a strain gauge type with linear millivolt output proportional to acceleration. Angular rate sensors, measuring vehicle roll, pitch, and yaw rates, are ultra small, solid state units designs for crash test service. The TDAS Pro hardware and software conform to the latest SAE J211, Instrumentation for Impact Test. Each of the 16

channels is capable of providing precision amplification, scaling, and filtering based on transducer specifications and calibrations. During the test, data are recorded from each channel at a rate of 10,000 values per second with a resolution of one part in 65,536. Once the data are recorded, internal batteries will back these up inside the unit should the primary battery cable be severed. Initial contact of the pressure switch on the vehicle bumper provides a time zero mark as well as initiating the recording process. After each test, the data are downloaded from the TDAS Pro unit into a laptop computer at the test site. The Test Risk Assessment Program (TRAP) software then processes the raw data to produce detailed reports of the test results. Each of the TDAS Pro units is returned to the factory annually for complete recalibration. Accelerometers and rate transducers are also calibrated annually with traceability to the National Institute for Standards and Technology.

TRAP uses the data from the TDAS Pro to compute occupant/compartment impact velocities, time of occupant/compartment impact after vehicle impact, and the highest 10-millisecond (ms) average ridedown acceleration. TRAP calculates change in vehicle velocity at the end of a given impulse period. In addition, maximum average accelerations over 50-ms intervals in each of the three directions are computed. For reporting purposes, the data from the vehicle-mounted accelerometers are filtered with a 60-Hz digital filter, and acceleration versus time curves for the longitudinal, lateral, and vertical directions are plotted using TRAP.

TRAP uses the data from the yaw, pitch, and roll rate transducers to compute angular displacement in degrees at 0.0001-s intervals and then plots yaw, pitch, and roll versus time. These displacements are in reference to the vehicle-fixed coordinate system with the initial position and orientation of the vehicle-fixed coordinate systems being initial impact.

4.3.2 Anthropomorphic Dummy Instrumentation

An Alderson Research Laboratories Hybrid II, 50th percentile male anthropomorphic dummy, restrained with lap and shoulder belts, was placed in the driver's position of the 1100C vehicle. The dummy was uninstrumented. Use of a dummy in the 2270P vehicle is optional according to *MASH*, and there was no dummy used in the test with the 2270P vehicle.

4.3.3 Photographic Instrumentation and Data Processing

Photographic coverage of each test included three high-speed cameras: one overhead with a field of view perpendicular to the ground and directly over the impact point; one placed behind the installation at an angle; and a third placed to have a field of view parallel to and aligned with the installation at the downstream end. A flashbulb activated by pressure-sensitive tape switches was positioned on the impacting vehicle to indicate the instant of contact with the installation and was visible from each camera. The films from these high-speed cameras were analyzed on a computer-linked motion analyzer to observe phenomena occurring during the collision and to obtain time-event, displacement, and angular data. A mini-DV camera and still cameras recorded and documented conditions of the test vehicle and installation before and after each test.

CHAPTER 5. MASH TEST 3-10 CRASH TEST RESULTS

5.1 **TEST DESIGNATION AND ACTUAL IMPACT CONDITIONS**

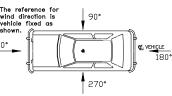
MASH Test 3-10 involves an 1100C vehicle weighing 2425 lb \pm 55 lb impacting the bridge rail at an impact speed of 62.2 mi/h ± 2.5 mi/h and an angle of 25 degrees ± 1.5 degrees. The target impact point was 3.6 ft upstream of post 9. The 2005 Kia Rio used in the test had a test inertial mass of 2431 lb and gross static mass of 2597 lb. The actual impact speed and angle were 62.0 mi/h and 24.9 degrees, respectively. The actual impact point was 3.7 ft upstream of post 9. Target impact severity (IS) was 56.0 kip-ft, and actual IS was 59.2 kip-ft, which was 5.7 percent greater than the target IS.

5.2 **TEST VEHICLE**

A 2005 Kia Rio, shown in Figures 5.1 and 5.2, was used for the crash test. Test inertia weight of the vehicle was 2431 lb, and its gross static weight was 2597 lb. The height to the lower edge of the vehicle bumper was 8.50 inches, and it was 22.75 inches to the upper edge of the bumper. Table C1 in Appendix C gives additional dimensions and information on the vehicle. The vehicle was directed into the installation using the cable reverse tow and guidance system, and was released to be free-wheeling and unrestrained just prior to impact.

5.3 WEATHER CONDITIONS

The test was performed on the morning of April 9, 2012. Weather conditions at the time of testing were as follows: wind speed: 2 mi/h; wind direction: The reference for wind direction is vehicle fixed as 905 82 degrees with respect to the vehicle (vehicle was traveling in a southwesterly direction); temperature: 74°F, relative humidity: ٥۰ 72 percent.



5.4 **TEST DESCRIPTION**

The 2005 Kia Rio, traveling at an impact speed of 62.0 mi/h, impacted the TxDOT Picket Rail 3.7 ft upstream of post 9 at an impact angle of 24.9 degrees. At approximately 0.019 s, the vehicle began to redirect, and at 0.029 s, the right front tire blew out. Maximum deflection of 0.9 inch on the top rail occurred at 0.051 s. At 0.067 s, the front passenger window shattered, and at 0.167 s, the vehicle was traveling parallel with the bridge rail at a speed of 52.2 mi/h. The rear of the vehicle contacted the bridge rail at 0.168 s. At 0.256 s, the vehicle lost contact with the bridge rail and was traveling at an exit speed and angle of 51.1 mi/h and 6.5 degrees, respectively. Brakes on the vehicle were applied 1.16 s after impact, and the vehicle subsequently came to rest 195 ft downstream of impact and 21 ft toward traffic lanes. Figures C1 and C2 in Appendix C show sequential photographs of the test period.



Figure 5.1. Vehicle/Installation Geometrics for Test No. 490022-2.



Figure 5.2. Vehicle before Test No. 490022-2.

5.5 DAMAGE TO TEST INSTALLATION

Figures 5.3 and 5.4 show damage to the TxDOT Picket Rail. Cracks in the curb radiated from the front and rear anchor bolts toward the field side at post 9, and from the rear anchor bolt on the upstream side of post 10. Tire marks were evident on the traffic face of all the horizontal metal rail elements from 3.7 ft upstream of post 9 for a length of 10.0 ft. There was no evidence of contact on the vertical pickets. Working width was 10.7 inches, and maximum dynamic deflection of the horizontal metal rail element was 0.9 inch. Residual permanent deformation was minimal and not measureable.

5.6 VEHICLE DAMAGE

Figure 5.5 shows damage to the vehicle. The right front strut and strut tower were deformed. The front bumper, hood, right front tire and wheel rim, right front fender, right front door and door glass, right rear door, right rear wheel rim, right rear quarter panel, and rear bumper were also damaged. Maximum exterior crush to the vehicle was 11.0 inches in the side plane at the right front corner at bumper height. The right side floor pan was also deformed, with a maximum occupant compartment deformation of 3.0 inches. Figure 5.6 shows the interior of the vehicle. Exterior vehicle crush and occupant compartment measurements are shown in Appendix C, Tables C2 and C3.

5.7 OCCUPANT RISK FACTORS

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk. In the longitudinal direction, the occupant impact velocity was 22.0 ft/s at 0.074 s, the highest 0.010-s occupant ridedown acceleration was 5.7 Gs from 0.178 to 0.188 s, and the maximum 0.050-s average acceleration was -12.8 Gs between 0.023 and 0.073 s. In the lateral direction, the occupant impact velocity was 33.5 ft/s at 0.074 s, the highest 0.010-s occupant ridedown acceleration was 12.2 Gs from 0.181 to 0.191 s, and the maximum 0.050-s average was -19.4 Gs between 0.017 and 0.067 s. Theoretical Head Impact Velocity (THIV) was 43.7 km/h or 12.1 m/s at 0.073 s; Post-Impact Head Decelerations (PHD) was 13.2 Gs between 0.181 and 0.191 s; and Acceleration Severity Index (ASI) was 2.39 between 0.017 and 0.067 s. Figure 5.7 summarizes these data and other pertinent information from the test. In Appendix C, Figures C3 through C9 present Vehicle angular displacements and accelerations versus time traces.



Figure 5.3. Vehicle/Installation after Impact for Test No. 490022-2.



Figure 5.4. Installation after Test No. 490022-2.



Figure 5.5. Vehicle after Test No. 490022-2.

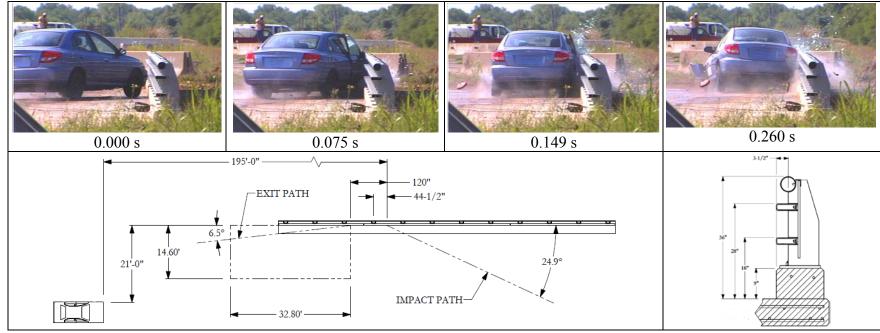


Before Test

After Test



Figure 5.6. Interior of Vehicle for Test No. 490022-2.



General Information

Concret Information	Impact Conditions
General Information	Impact Conditions
Test Agency Texas A&M Trar	
Test Standard Test No MASH Test 3-10	0
TTI Test No 490022-2	Location/Orientation .
Test Date 2012-04-09	Exit Conditions
Test Article	Speed
Type Bridge Rail	Angle
Name TxDOT Picket Ra	ail Occupant Risk Values
Installation Length 92.0 ft	Impact Velocity
Material or Key Elements Three tubular ste	el rail elements with Longitudinal
vertical pickets n	nounted on steel plate Lateral
posts anchored of	on concrete deck and curb Ridedown Acceleration
Soil Type and Condition Concrete bridge	
Test Vehicle	Lateral
Type/Designation 1100C	THIV
Make and Model 2005 Kia Rio	PHD
Curb 2373 lb	ASI
Test Inertial 2431 lb	Max. 0.050-s Average
Dummy 166 lb	Longitudinal
Gross Static 2597 lb	Lateral
	Vertical

Speed	<u>6</u> 2.0 mi/h
Angle	24.9 degrees
Location/Orientation	3.7 ft upstream of
Exit Conditions	post 9
Speed	51.1 mi/h
Angle	6.5 degrees
Occupant Risk Values	•
Impact Velocity	
Longitudinal	22.0 ft/s
Lateral	33.5 ft/s
Ridedown Accelerations	
Longitudinal	5.7 G
Lateral	
THIV	43.7 km/h
PHD	13.2 G

ASI2.39

Longitudinal.....-12.8 G Lateral.....-19.4 G Vertical-2.5 G

Post-Impact Trajectory

Post-impact majectory	
Stopping Distance	195 ft dnstrm
	21 ft twd traffic
Vehicle Stability	
Maximum Yaw Angle	60 degrees
Maximum Pitch Angle	8 degrees
Maximum Roll Angle	25 degrees
Vehicle Snagging	No
Vehicle Pocketing	No
Test Article Deflections	
Dynamic	0.9 inch
Permanent	Nil
Working Width	10.7 inches
Vehicle Damage	
VDS	01RFQ4
CDC	01FREW3
Max. Exterior Deformation	11.0 inches
OCDI	RF0030000
Max. Occupant Compartment	
Deformation	3.0 inches

2012-10-25

Figure 5.7. Summary of Results for MASH Test 3-10 on the TxDOT Picket Rail.

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5.8 ASSESSMENT OF TEST RESULTS

An assessment of the test based on the applicable *MASH* safety evaluation criteria is provided below.

5.8.1 Structural Adequacy

- A. Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.
- Results: The TxDOT Picket Rail contained and redirected the 1100C vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection of the horizontal metal rail elements was 0.9 inch. (PASS)

5.8.2 Occupant Risk

D. Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.

Deformation of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH. (roof ≤ 4.0 inches; windshield = ≤ 3.0 inches; side windows = no shattering by test article structural member; wheel/foot well/toe pan ≤ 9.0 inches; forward of A-pillar ≤ 12.0 inches; front side door area above seat ≤ 9.0 inches; front side door below seat ≤ 12.0 inches; floor pan/transmission tunnel area ≤ 12.0 inches).

- Results: No detached elements, fragments, or other debris was present to penetrate or show potential for penetrating the occupant compartment, or present undue hazard to others. (PASS) Maximum occupant compartment deformation was 3.0 inches in the right floor pan area. (PASS)
- *F.* The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.
- <u>Results</u>: The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 25 degrees and 8 degrees, respectively. (PASS)
- H. Occupant impact velocities should satisfy the following: Longitudinal and Lateral Occupant Impact Velocity <u>Preferred</u> <u>30 ft/s</u> <u>40 ft/s</u>

- <u>Results</u>: Longitudinal occupant impact velocity was 22.0 ft/s, and lateral occupant impact velocity was 33.5 ft/s. (PASS)
- I. Occupant ridedown accelerations should satisfy the following: <u>Longitudinal and Lateral Occupant Ridedown Accelerations</u> <u>Preferred</u> <u>15.0 Gs</u> <u>20.49 Gs</u>
- <u>Results</u>: Maximum longitudinal ridedown acceleration was 5.7 Gs, and maximum lateral ridedown acceleration was 12.2 Gs. (PASS)

5.8.3 Vehicle Trajectory

For redirective devices, the vehicle shall exit the barrier within the exit box (not less than 32.8 ft).

<u>Result</u>: The 1100C vehicle crossed the exit box 60 ft downstream of loss of contact with the bridge rail. (PASS)

CHAPTER 6. MASH TEST 3-11 CRASH TEST RESULTS

6.1 **TEST DESIGNATION AND ACTUAL IMPACT CONDITIONS**

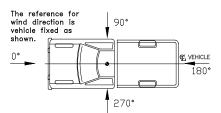
MASH Test 3-11 involves a 2270P vehicle weighing 5000 lb \pm 110 lb impacting the test article at an impact speed of 62.2 mi/h \pm 2.5 mi/h and an angle of 25 degrees \pm 1.5 degrees. The target impact point was 4.3 ft upstream of post 4. The 2006 Dodge Ram 1500 pickup truck used in the test weighed 5018 lb and the actual impact speed and angle were 61.6 mi/h and 24.2 degrees, respectively. The actual impact point was 5.0 ft upstream of post 4. Target impact severity (IS) was 115.6 kip-ft, and actual IS was 107.0 kip-ft, which was 7.4 percent less than the target IS.

6.2 **TEST VEHICLE**

A 2006 Dodge Ram 1500 pickup truck, shown in Figures 6.1 and 6.2, was used for the crash test. Test inertia weight of the vehicle was 5018 lb, and its gross static weight was 2018 lb. The height to the lower edge of the vehicle bumper was 13.75 inches, and it was 25.38 inches to the upper edge of the bumper. The height to the center of gravity was 28.25 inches. Tables D1 and D2 in Appendix D give additional dimensions and information on the vehicle. The vehicle was directed into the installation using the cable reverse tow and guidance system, and was released to be free-wheeling and unrestrained just prior to impact.

6.3 WEATHER CONDITIONS

The test was performed on the morning of April 10, 2012. Weather conditions at the time of testing were as follows: wind speed: 6 mi/h; wind direction: 195 degrees with respect to the vehicle (vehicle was traveling in a southwesterly direction); temperature: 77°F, relative humidity: 62 percent.



6.4 **TEST DESCRIPTION**

The test vehicle, traveling at an impact speed of 61.6 mi/h, impacted the Picket Rail 5.0 ft upstream of post 4 at an impact angle of 24.2 degrees. At approximately 0.024 s after impact, the right front tire blew out, and at 0.039 s, the vehicle began to redirect. The top of the front passenger door and rear passenger door separated from the frame of the cab at 0.046 s and 0.061 s, respectively. Stress cracks in the windshield appeared at 0.074 s, and the rear of the vehicle impacted the bridge rail at 0.155 s. The vehicle began traveling parallel with the bridge rail at 0.166 s. At 0.295 s, the vehicle lost contact with the bridge rail while traveling at an exit speed and angle of 57.6 mi/h and 19.6 degrees. Brakes on the vehicle were applied at 1.308 s, and the vehicle subsequently came to rest 240 ft downstream of impact and 35 ft toward traffic lanes. Figures D1 and D2 in Appendix D show sequential photographs of the test period.



Figure 6.1. Vehicle/Installation Geometrics for Test No. 490022-3.



Figure 6.2. Vehicle before Test No. 490022-3.

6.5 DAMAGE TO TEST INSTALLATION

Figures 6.3 and 6.4 show damage to the TxDOT picket rail. A crack in the concrete curb radiated toward the field side from the rear anchor bolt on the impact side of post 3. Cracks in the concrete curb radiated toward the field side from the front and rear anchor bolts on both sides of post 4, and extended into the concrete deck where each radiated downward and outward on each side of the post. Working width was 10.4 inches. Maximum dynamic deflection of the top rail was 2.8 inches. Maximum permanent deformation of the rail elements was 0.8 inch on the top rail, 0.7 inch on the middle rail, and 0.9 inch on the bottom rail.

6.6 VEHICLE DAMAGE

Figure 6.5 shows damage to the 2270P vehicle. The right front frame rail and right front upper and lower A-arms were deformed. Also damaged were the front bumper, hood, right front tire and wheel rim, right front fender, right front and rear doors, right exterior bed, right rear tire and wheel rim and the rear bumper. The windshield sustained stress cracks in each lower corner near the hood. Maximum exterior crush to the vehicle was 11.0 inches in both the front and side planes at the right front corner at bumper height. Maximum occupant compartment deformation was 2.75 inches in the lateral area across the cab at the passenger side kickpanel. Figure 6.6 shows the interior of the vehicle, while Tables D3 and D4 in Appendix D show the exterior vehicle crush and occupant compartment measurements.

6.7 OCCUPANT RISK FACTORS

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk. In the longitudinal direction, the occupant impact velocity was 10.8 ft/s at 0.091 s, the highest 0.010-s occupant ridedown acceleration was 4.6 Gs from 0.182 to 0.192 s, and the maximum 0.050-s average acceleration was -6.5 Gs between 0.028 and 0.078 s. In the lateral direction, the occupant impact velocity was 28.5 ft/s at 0.091 s, the highest 0.010-s occupant ridedown acceleration was 15.2 Gs from 0.201 to 0.211 s, and the maximum 0.050-s average was -15.7 Gs between 0.035 and 0.085 s. Theoretical Head Impact Velocity (THIV) was 34.1 km/h or 9.5 m/s at 0.090 s; Post-Impact Head Decelerations (PHD) was 15.5 Gs between 0.201 and 0.211 s; and Acceleration Severity Index (ASI) was 1.83 between 0.029 and 0.079 s. Figure 5.7 summarizes these data and other pertinent information from the test. In Appendix D, Figures D3 through D9 present the Vehicle angular displacements and accelerations versus time traces.



Figure 6.3. Installation/Vehicle after Impact for Test No. 490022-3.



Figure 6.4. Installation after Test No. 490022-3.



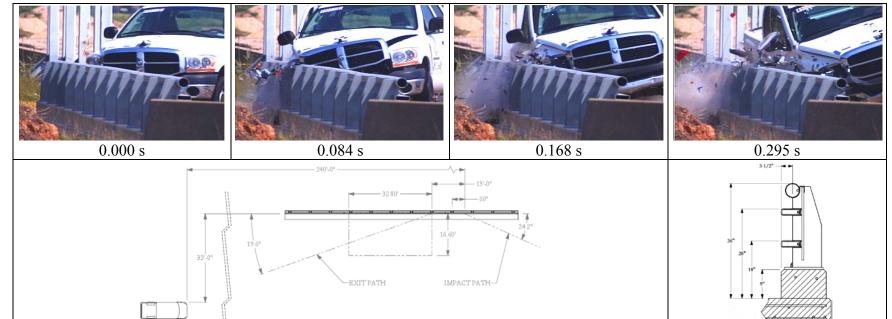
Figure 6.5. Vehicle after Test No. 490022-3.





Figure 6.6. Interior of Vehicle for Test No. 490022-3.

After Test



General Information		Impact Conditions
Test Agency	Texas A&M Transportation Institute (TTI)	Speed
Test Standard Test No		Angle
TTI Test No.	490022-3	Location/Orientatio
Test Date		Exit Conditions
Test Article		Speed
Туре	Bridge Rail	Angle
Name		Occupant Risk Valu
Installation Length	92.0 ft	Impact Velocity
Material or Key Elements	Three tubular steel rail elements with	Longitudinal
	vertical pickets mounted on steel plate	Lateral
	posts anchored on concrete deck and curb	Ridedown Accelera
Soil Type and Condition	Concrete bridge deck and curb, dry	Longitudinal
Test Vehicle	6	Lateral
Type/Designation	2270P	THIV
	2006 Dodge Ram 1500 Pickup	PHD
Curb	5018 lb	ASI
Test Inertial	5018 lb	Max. 0.050-s Averag
Dummy	No dummy	Longitudinal
Gross Static	5018 lb	Lateral
		Vertical

Speed	61.6 mi/h
Angle	24.2 degrees
Location/Orientation	
Exit Conditions	of post 4
Speed	
Angle	19.6 dearees
Occupant Risk Values	
Impact Velocity	
Longitudinal	10.8 ft/s
Lateral	
Ridedown Accelerations	
Longitudinal	4.6 a
Lateral	
THIV	34.1 km/h
PHD	15.5 G
ASI	1.83
Max. 0.050-s Average	
Longitudinal	-6.5 G
Lateral	
Vertical	

Post-Impact Trajectory

Stopping Distance	240 ft dwnstrm
	35 ft twd traffic
Vehicle Stability	
Maximum Yaw Angle	35 degrees
Maximum Pitch Angle	5 degrees
Maximum Roll Angle	23 degrees
Vehicle Snagging	No
Vehicle Pocketing	No
Test Article Deflections	
Dynamic	2.8 inches
Permanent	0.9 inch
Working Width	10.4 inches
Vehicle Damage	
VDS	01RFQ5
CDC	01FREW4
Max. Exterior Deformation	11.0 inches
OCDI	RF0000000
Max. Occupant Compartment	
Deformation	2.75 inches

Figure 6.7. Summary of Results for MASH Test 3-11 on the TxDOT Picket Rail.

6.8 ASSESSMENT OF TEST RESULTS

An assessment of the test based on the applicable *MASH* safety evaluation criteria is provided below.

6.8.1 Structural Adequacy

- A. Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.
- <u>Results</u>: The TxDOT Picket Rail contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 2.8 inches. (PASS)

6.8.2 Occupant Risk

D. Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.

Deformation of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH. (roof ≤ 4.0 inches; windshield = ≤ 3.0 inches; side windows = no shattering by test article structural member; wheel/foot well/toe pan ≤ 9.0 inches; forward of A-pillar ≤ 12.0 inches; front side door area above seat ≤ 9.0 inches; front side door below seat ≤ 12.0 inches; floor pan/transmission tunnel area ≤ 12.0 inches).

- <u>Results</u>: No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or present undue hazard to others. (PASS) Maximum occupant compartment deformation was 2.75 inches in the lateral area across the cab at the front passenger kick panel. (PASS)
- *F.* The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.
- <u>Results</u>: The 2270P vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 23 degrees and 5 degrees, respectively. (PASS)
- I. Occupant impact velocities should satisfy the following: Longitudinal and Lateral Occupant Impact Velocity <u>Preferred</u> 9.0 m/s (30 ft/s) <u>Maximum</u> 12.2 m/s (40 ft/s)

- <u>Results</u>: Longitudinal occupant impact velocity was 10.8 ft/s, and lateral occupant impact velocity was 28.5 ft/s. (PASS)
- I. Occupant ridedown accelerations should satisfy the following: <u>Longitudinal and Lateral Occupant Ridedown Accelerations</u> <u>Preferred</u> <u>15.0 Gs</u> <u>20.49 Gs</u>
- <u>Results</u>: Maximum longitudinal ridedown acceleration was 4.6 G, and maximum lateral ridedown acceleration was 15.2 G. (PASS)

6.8.3 Vehicle Trajectory

For redirective devices, the vehicle shall exit the barrier within the exit box (not less than 32.8 ft).

<u>Result</u>: The 2270P vehicle crossed the exit box 105 ft downstream of loss of contact with the bridge rail. (PASS)

CHAPTER 7. SUMMARY AND CONCLUSIONS

7.1 SUMMARY OF RESULTS

7.1.1 MASH Test 3-10 (Test No. 490022-2)

The TxDOT Picket Rail contained and redirected the 1100C vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection of the horizontal metal rail elements was 0.9 inch. No detached elements, fragments, or other debris was present to penetrate or show potential for penetrating the occupant compartment, or present undue hazard to others. Maximum occupant compartment deformation was 3.0 inches in the right floor pan area. The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 25 degrees and 8 degrees, respectively. Occupant compartment risk factors were within the limits specified in *MASH*. The 1100C vehicle crossed the exit box 60 ft downstream of loss of contact with the bridge rail.

7.1.2 *MASH* Test 3-11 (Test No. 490022-3)

The TxDOT Picket Rail contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 2.8 inches. No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or present undue hazard to others. Maximum occupant compartment deformation was 2.75 inches in the lateral area across the cab at the front passenger kick panel. The 2270P vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 23 degrees and 5 degrees, respectively. Occupant compartment risk factors were within the limits specified in *MASH*. The 2270P vehicle crossed the exit box 105 ft downstream of loss of contact with the bridge rail.

7.2 CONCLUSIONS

The TxDOT Picket Rail performed acceptably for MASH TL-3 (see Tables 7.1 and 7.2).

Table 7.1. Performance Evaluation Summary for MASH Test 3-10 on the TxDOT Picket Rail.

5	Test Agency: Texas A&M Transportation Institute		Test Date: 2012-04-09
`	MASH Test 3-10 Evaluation Criteria	Test Results	Assessment
0 1000 10 0	 Structural Adequacy A. Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable. 	The TxDOT Picket Rail contained and redirected the 1100C vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection of the horizontal metal rail elements was 0.9 inch.	Pass
	Occupant Risk		
	D. Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	No detached elements, fragments, or other debris was present to penetrate or show potential for penetrating the occupant compartment, or present undue hazard to others.	Pass
20	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH.	Maximum occupant compartment deformation was 3.0 inches in the right floor pan area.	Pass
	<i>F.</i> The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 25 degrees and 8 degrees, respectively.	Pass
	H. Longitudinal and lateral occupant impact velocities should fall below the preferred value of 9.1 m/s (30 ft/s), or at least below the maximum allowable value of 12.2 m/s (40 ft/s).	The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 25 degrees and 8 degrees, respectively.	Pass
	I. Longitudinal and lateral occupant ridedown accelerations should fall below the preferred value of 15.0 Gs, or at least below the maximum allowable value of 20.49 Gs.	Maximum longitudinal ridedown acceleration was 5.7 Gs, and maximum lateral ridedown acceleration was 12.2 Gs.	¹ Pass
	Vehicle Trajectory For redirective devices, the vehicle shall exit the barrier within the exit box (not less than 32.8 ft).	The 1100C vehicle crossed the exit box 60 ft downstream of loss of contact with the bridge rail.	Pass

Table 7.2. Performance Evaluation Summary for MASH Test 3-11 on the TxDOT Picket Rail.

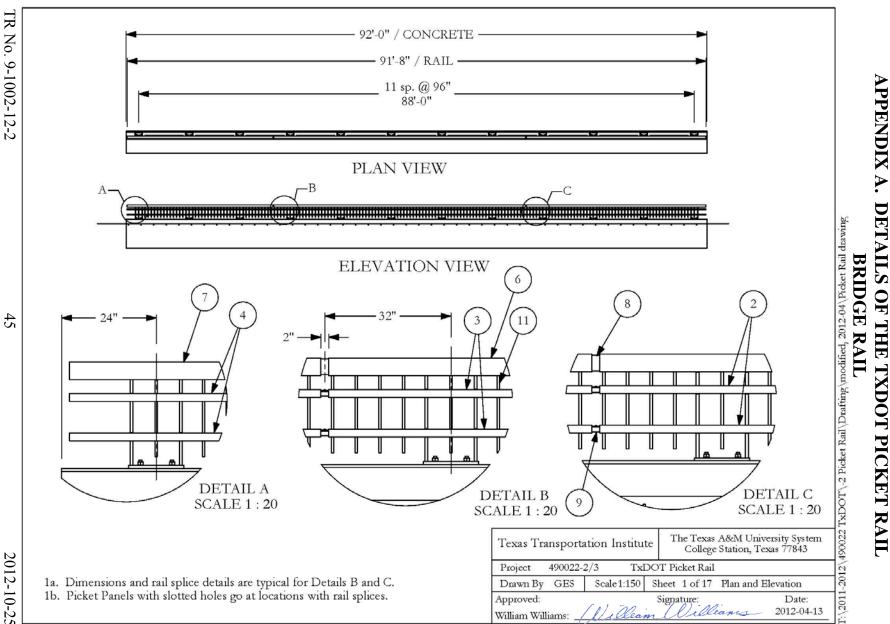
: 	Test Agency: Texas A&M Transportation Institute		Test Date: 2012-04-10
	MASH Test 3-11 Evaluation Criteria	Test Results	Assessment
0 1000 10 0	 Structural Adequacy A. Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable. 	The TxDOT Picket Rail contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 2.8 inches.	Pass
	Occupant Risk		
	D. Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	No detached elements, fragments, or other debris were present to penetrate or show potential for penetrating the occupant compartment, or present undue hazard to others.	Pass
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH.	Maximum occupant compartment deformation was 2.75 inches in the lateral area across the cab at the front passenger kick panel.	Pass
	<i>F.</i> The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 2270P vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 23 degrees and 5 degrees, respectively.	Pass
	H. Longitudinal and lateral occupant impact velocities should fall below the preferred value of 9.1 m/s (30 ft/s), or at least below the maximum allowable value of 12.2 m/s (40 ft/s).	Longitudinal occupant impact velocity was 10.8 ft/s, and lateral occupant impact velocity was 28.5 ft/s.	Pass
	I. Longitudinal and lateral occupant ridedown accelerations should fall below the preferred value of 15.0 Gs, or at least below the maximum allowable value of 20.49 Gs.	Maximum longitudinal ridedown acceleration was 4.6 G, and maximum lateral ridedown acceleration was 15.2 G.	Pass
	Vehicle Trajectory		
	For redirective devices, the vehicle shall exit the barrier within the exit box (not less than 32.8 ft).	The 2270P vehicle crossed the exit box 105 ft downstream of loss of contact with the bridge rail.	Pass

CHAPTER 8. IMPLEMENTATION STATEMENT

The purpose of this project was to develop and evaluate a new aesthetic bridge rail with steel pickets that meets the current *MASH* safety performance criteria for TL-3. The TxDOT Picket Rail tested under this project met all the safety performance criteria for *MASH* TL-3 and is suitable for implementation on new bridge construction.

REFERENCES

- 1. AASHTO, *Manual for Assessing Safety Hardware*, American Association of State Highway and Transportation Officials, Washington, D.C., 2009.
- H. E. Ross, Jr., D. L. Sicking, R. A. Zimmer, and J. D. Michie. *Recommended Procedures for the Safety Performance Evaluation of Highway Features*, National Cooperative Highway Research Program Report 350, Transportation Research Board, National Research Council, Washington, D.C., 1993.
- 3. K. K. Mak, D. L. Bullard, Jr., and W. L. Menges. Testing and Evaluation of the Wyoming 740WYBRAIL Bridge Railing System, TTI Project No. 472610-4, Texas Transportation Institute, The Texas A&M University System, May 1996.

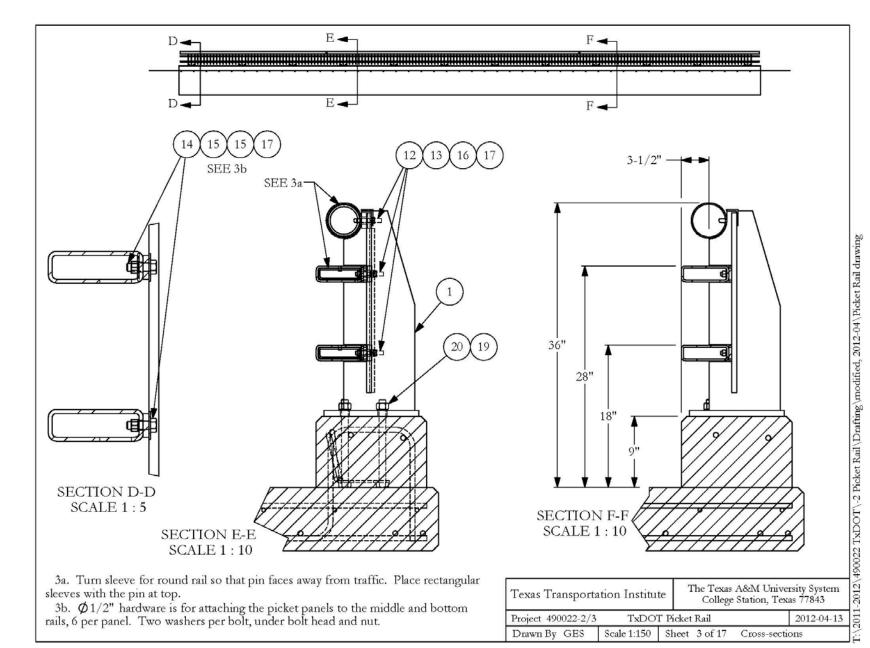


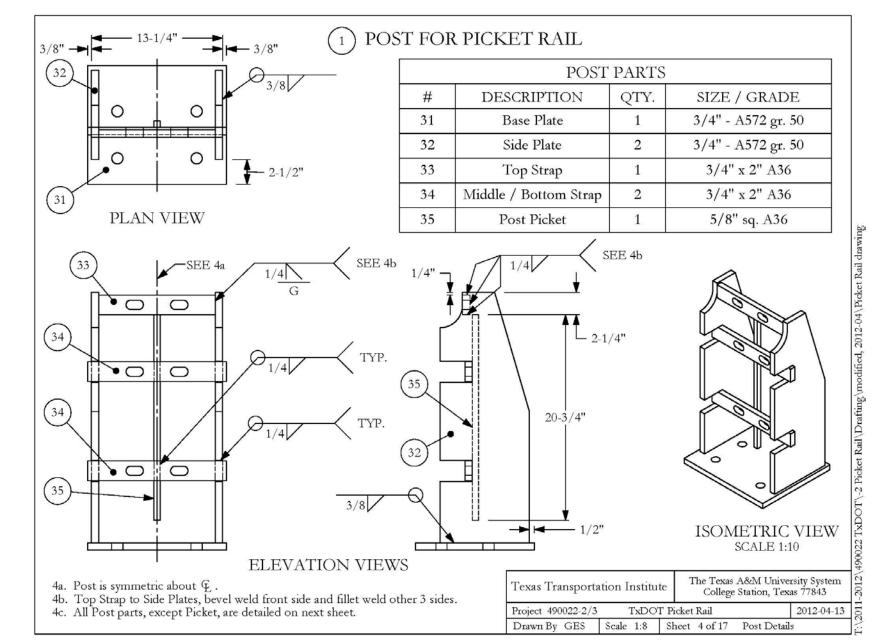
DETAILS OF THE TXDOT PICKET RAIL

RAIL PARTS					RAIL PARTS				
#	PART NAME	QTY.	SHT/GRD	#	#	PART NAME	QTY.	SHT/GRI	
1	Post for Picket Rail	12	sheet 4 - 5	1	.4	Bolt, 1/2 x 1-1/2 hex	66	A325	
2	HSS6x2x1/4 Left	2	sheet 6 - 7	1	5	Washer, 1" flat hardened	132		
3	HSS6x2x1/4 Center	2	sheet 8 - 9	1	6	Washer, 1/2 lock	72		
4	HSS6x2x1/4 Right	2	sheet 10	1	.7	Nut, 1/2 hex	138	A563	
5	HSS Round 4-1/2 x 3/16 Left	1	sheet 11	1	.8	Bolt, 7/8 x 10-1/2 hex	48	see 2b	
6	HSS Round 4-1/2 x 3/16 Center	1	sheet 11	1	.9	Washer, 7/8 hardened	48		
7	HSS Round 4-1/2 x 3/16 Right	1	sheet 12	2	20	Nut, 7/8 hex	48	Heavy Hex	
8	Splice Sleeve for HSS Round Rail	2	sheet 12	2	21	Anchor Plate for Picket Rail	12	sheet 14	
9	Splice Sleeve for HSS Rect. Rail	4	sheet 14	2	22	Rebar, Z	24	sheet 17	
10	Picket Panel	9	sheet 13	2	23	Rebar, transverse bottom	62	sheet 17	
11	Picket Panel at Rail Splice	2	sheet 13	2	24	Rebar, transverse top	184	sheet 17	
12	U-bolt for Picket Rail	36	sheet 14	2	25	Rebar, wall tie	46	sheet 17	
13	Plate Washer for Picket Rail	72	sheet 14	2	26	Rebar, curb stirrup	184	sheet 17	

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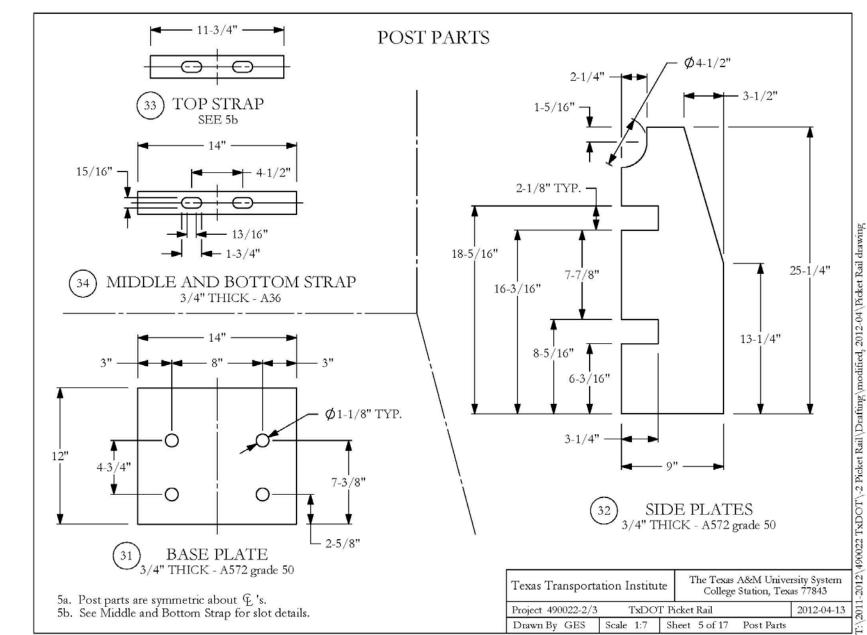
2a. All HSS Rails and HSS Round Splice Sleeve for this test are ASTM - A500 grade B. Do not substitute grade C.			
substituted, with additional 7/8 neavy nex nut tack-weided hush at bottom.	Texas Transportation Institu	ersity System kas 77843	
2c. A449 or A325T hardware is acceptable alternative to A325. 2d. Tolerances on steel parts is $\pm 1/8$ " unless otherwise indicated.	Project 490022-2/3 TxDO	2012-04-13	
2d. Tolerances on steel parts is $\pm 1/6$ unless otherwise indicated.	Drawn By GES Scale 1:150	Sheet 2 of 17 BOM	





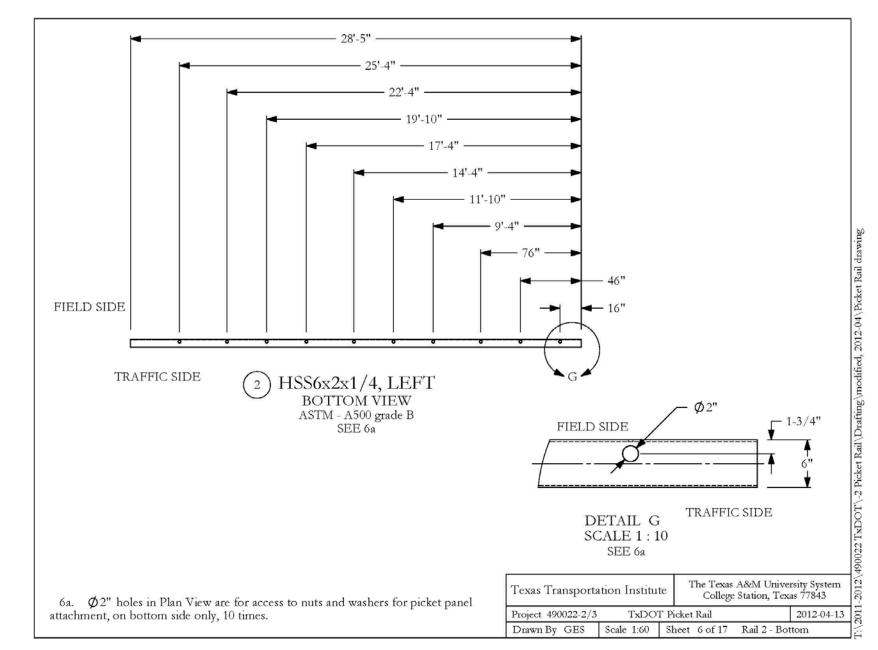
TR No. 9-1002-12-2

48



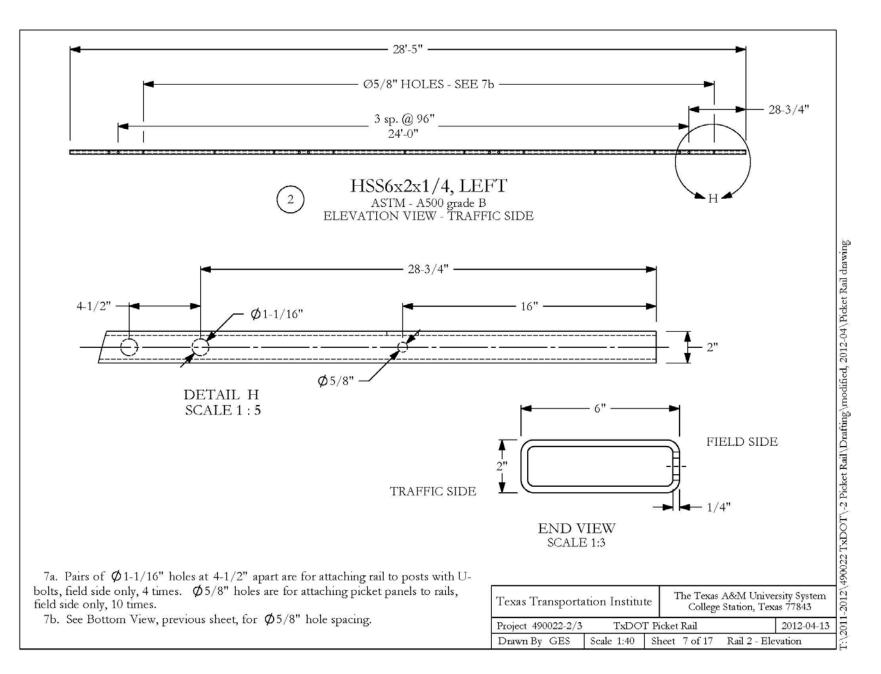
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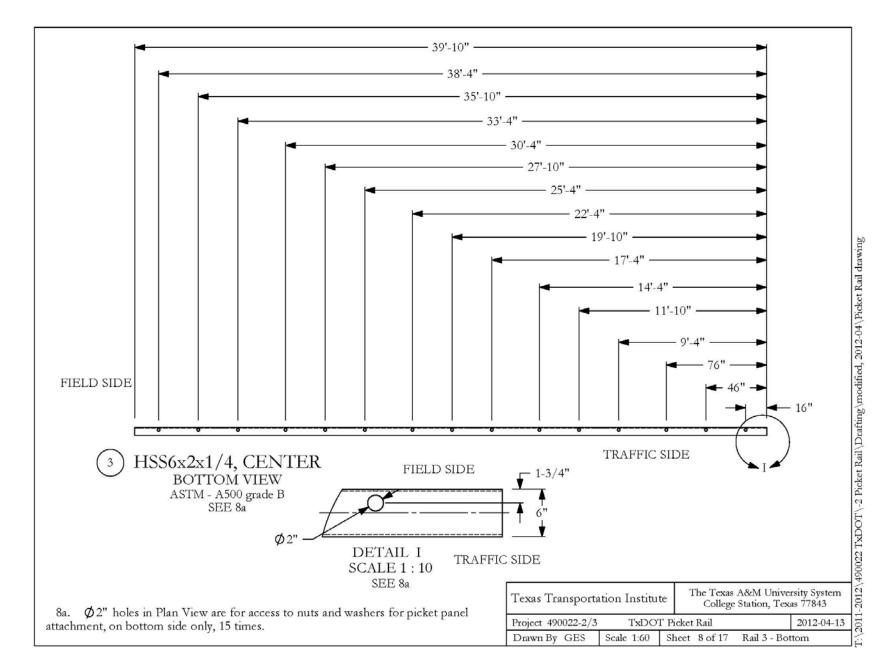
49



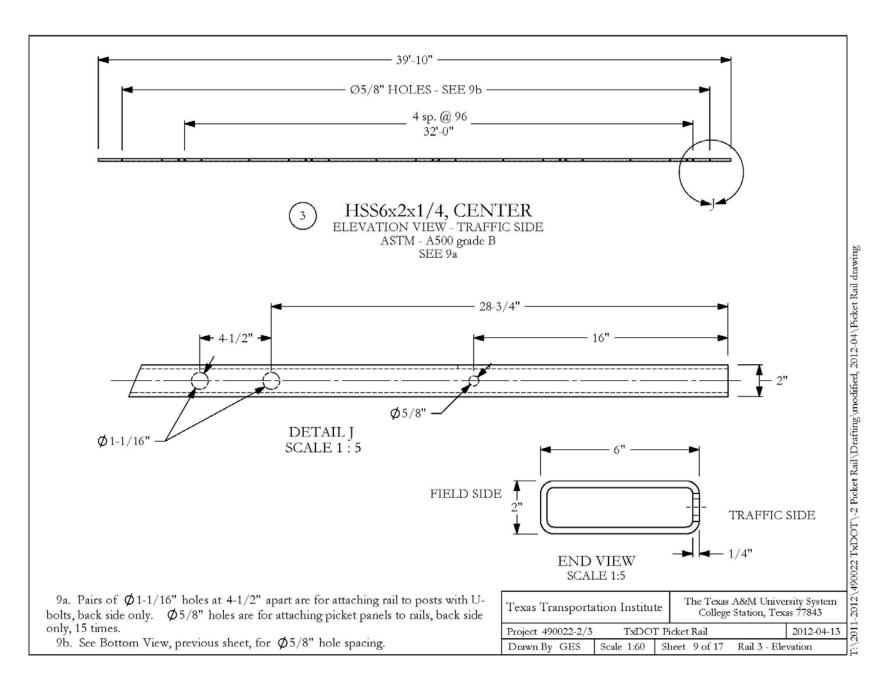


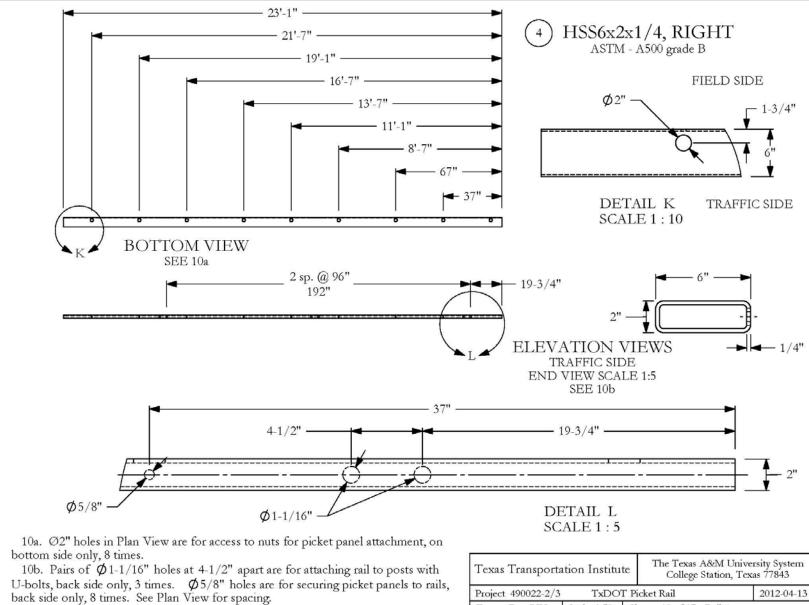
51











Drawn By GES

Scale 1:50

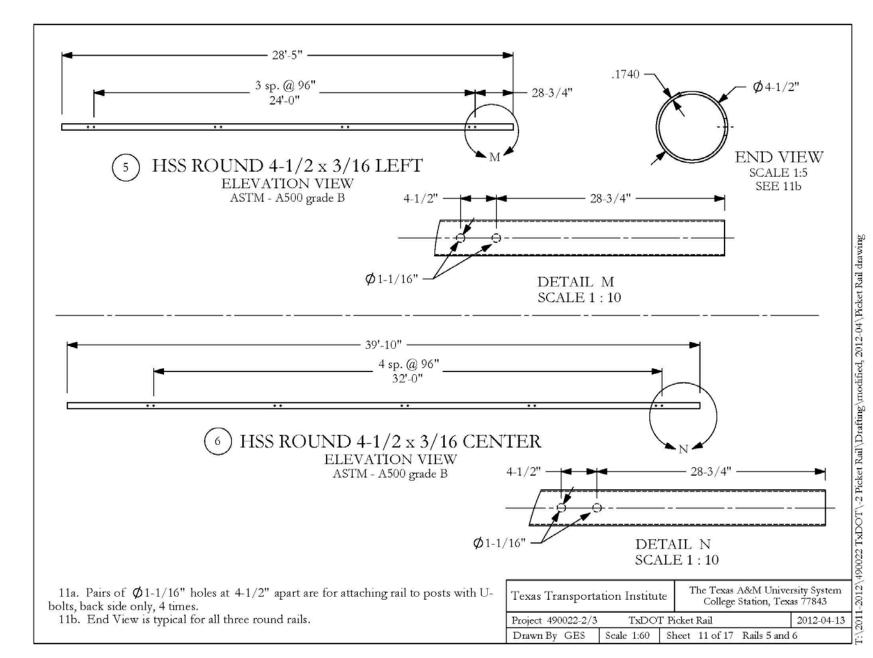
Sheet 10 of 17 Rail 4

-2012/490022 TxDOT/-2 Picket Rail/Drafting/modified, 2012-04/Picket Rail drawing

2011-

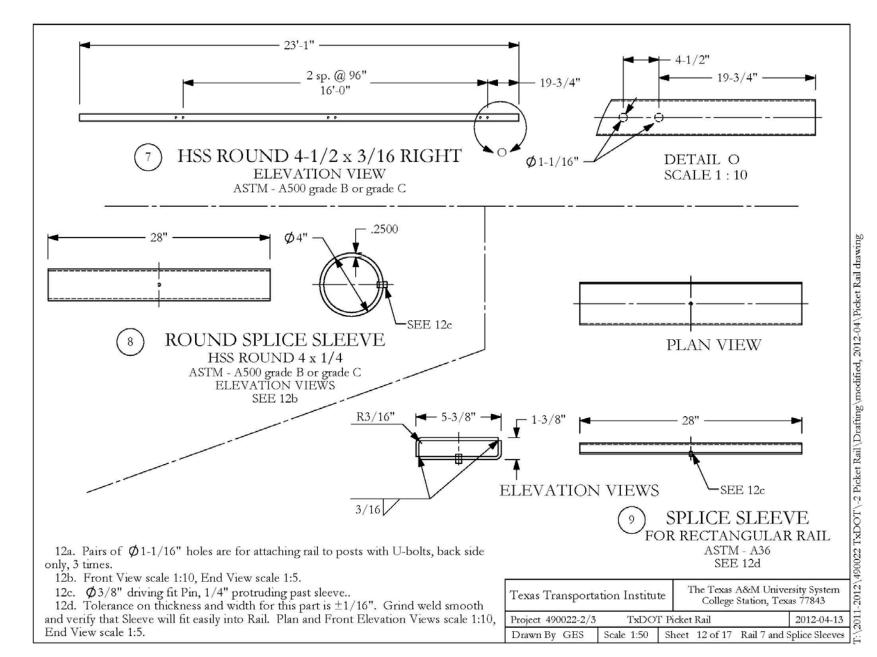
54

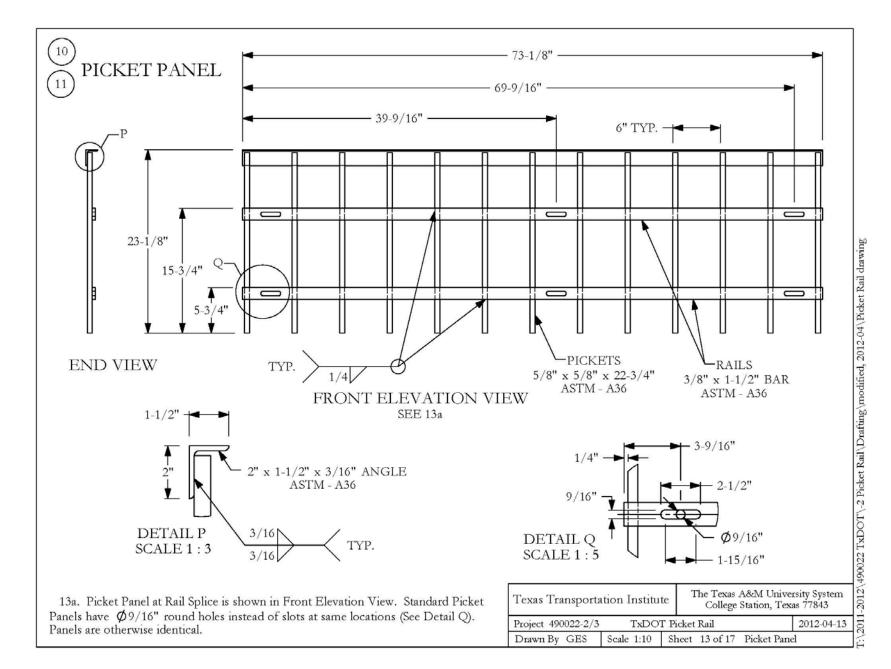
TR No. 9-1002-12-2



TR No. 9-1002-12-2

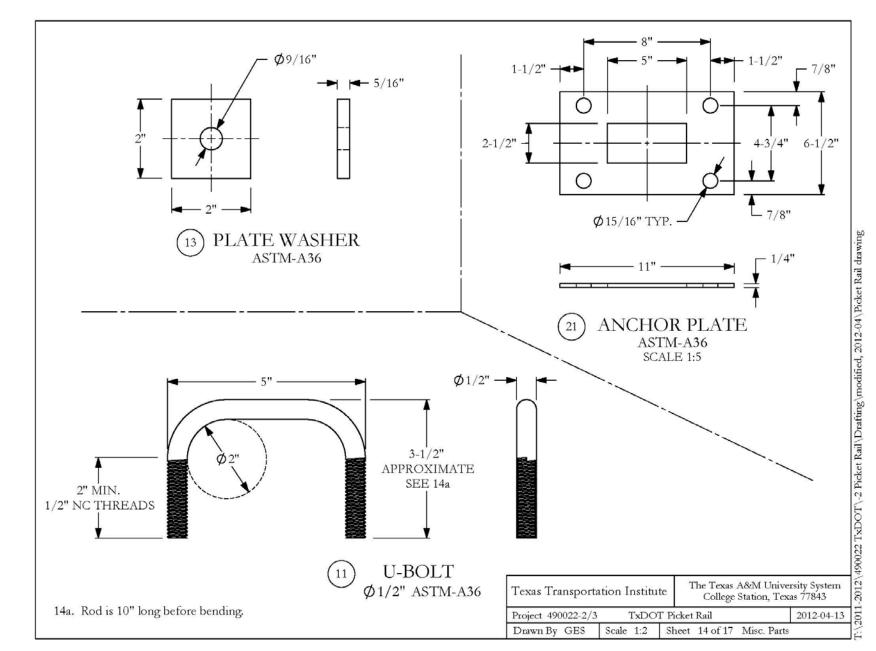
55



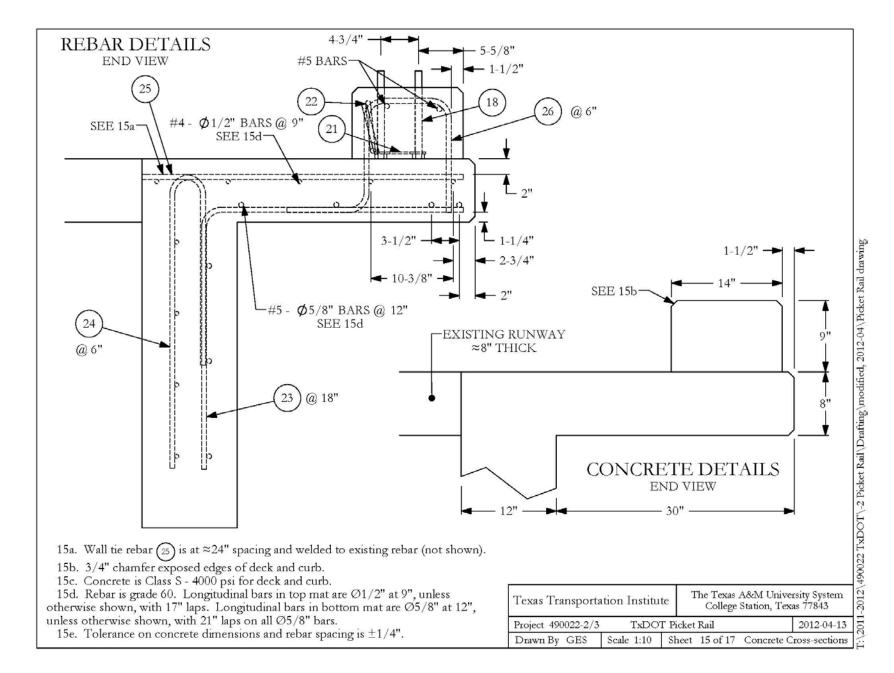


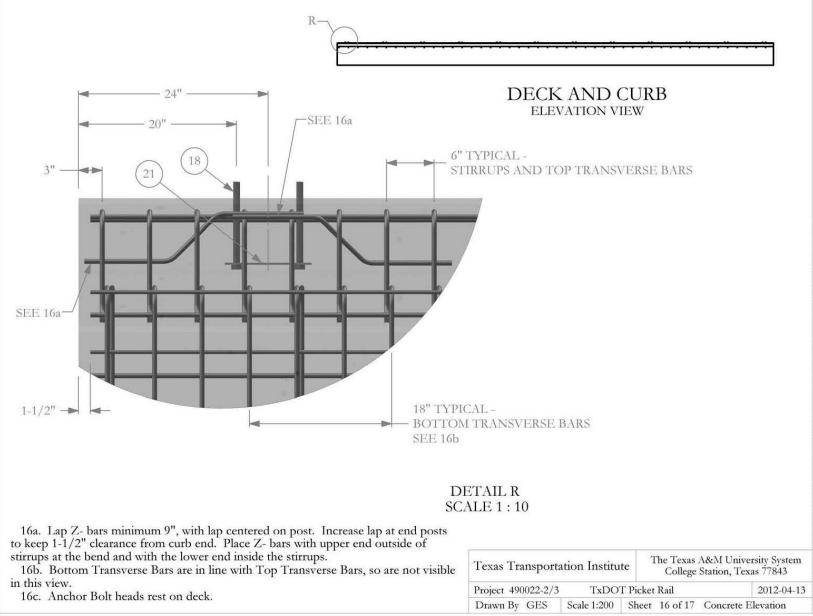
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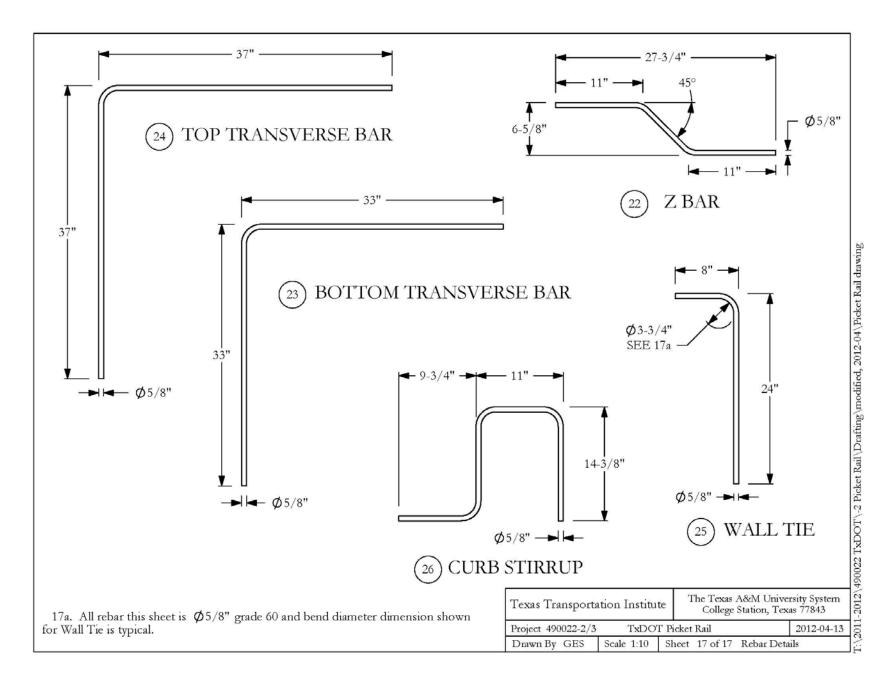
57



85







APPENDIX B. CERTIFICATION DOCUMENTATION

MATERIAL USED

TEST NUMBER 490

TEST NAME TxDOT Picket Rail

DATE 2012-04-09/10

DATE RECEIVED	ITEM NUMBER	DESCRIPTION	SUPPLIER	HEAT #
2012-03-19	Parts-18	Picket Rail Parts	Brazos Industries	see file
2012-02-23	Rebar 04-26	1/2'' x 20' gr 60	CMC-Sheplers	3029770
2012-02-23	Rebar 05-15	5/8'' x 20' grd 60	CMC-Sheplers	3028494

03/18/2012	21:25	281-371-5204

TUBULAR STEEL, TX

PAGE 01

09/28/2011 10:56 3148519338

TUBULAR STEEL INC

PAGE 01

Independenc	e Tube	6226 W, 74th St Chicago, IL 60638 708-496-0380 Fax: 708-563-1950				Itctube.com CHI 818292
Sold By: INDEPENDENCE TI 6226 W. 74th St. Chicago, IL 60638 Tei: 708-496-0380 Fax: 708-563-1950	UBE CORPORATION	Purchase Order No: po Sales Order No: CHI 19 Bill of Lading No: CHI 1 Invoice No:	91963 - 1	Shipp Invoic	ed: 9/22/20 ed:	11
Sold To: 2025 - TUBULAR S 1031 EXECUTIVE P ST. LOUIS, MO 631	KWY DRIVE	Ship To: 84 - TUBULAR STEEL 1700 TUBULAR STEEL STAUNTON, IL 62088	L ROAD		•	
CERTIFICATE Customer Part No:	of ANALYSIS and TE	STS	Ce	rtificate No; Test Date:		2
ROUND A500 GRA 4.000"OD X .250"	DE B(Ç)			Total Piece	es Total 30	Weight 7,215
Heat Number:	C56944					
Bundle Tag Yield, 557474 YLD=6 557475 YLD=6	C56944 Tensile Strength, Elongation, I 34158/TEN=79907/ELG=27.46 34158/TEN=79907/ELG=27.46 34158/TEN=79907/ELG=27.46	3	Y/T Ratio 0.8029 0.8029 0.8029 0.8029	Pieces 10 10 10	Weight 2,405 2,405 2,405	,
Bundle Tag Yield, 557474 YLD=6 557475 YLD=6	Tensile Strength, Elongation, I 34158/TEN=79907/ELG=27.46 34158/TEN=79907/ELG=27.46 34158/TEN=79907/ELG=27.46 **** Chemical Analysis *	3 3 5 P=0.0070 S=0.0040 Si=0.0300	0.8029 0.8029 0.8029	10 10 10	2,405 2,405	

Certification:

I certify that the above results are a true and correct copy of records prepared and maintained by independence Tube Corporation, Sworn this day, 9/15/2011

a 8

.

Annette Gorz, Test Report Clerk

WE PROUDLY MANUFACTURE ALL OF OUR HSS IN THE USA. INDEPENDENCE TUBE PRODUCT IS MANUFACTURED, TESTED, AND INSPECTED IN ACCORDANCE WITH ASTM STANDARDS.

CURRENT STANDARDS:

Page - 1

CN FASTENER MANUFACTURING, CO.

QUALITY CERTIFICATE

Date: Dec. 03, 2010 Product: B7 STUDDING Size: 7/8 x 12' (48 Pcs. 7/8-9 x 10-1/2) Production No: 00241364 Lot#: 315010042 Surface Coating: PLN QTY: 12015 pcs.

CHEMICAL COMPOSITION

	C	Si	Mn	P	S	Cu	NI	G .	Mo	B	
MILL HEAT #:	0.40	0.27	0.83	0.015	0.007	0.04	0.02	0.97	0.18		
0103002											

MECHANICAL PROPERTIES

LTR	Tempering Temperature
REQUIRED	<< OBSERVATIONS >>
HEC Max 35 C	HRC 30.0 ~ 33.0
860 min	966 ~ 967 N/mm²
725 min	889 - 890 N/mm ²
6 min	21.4-21.5
\$0 min	60.3 - 60.4
	and the second se
·	
	REQUIRED HEC Max 35 C 860 min 725 min 16 min

The information on chemical composition is based on the test certificated received from the steel mill or material supplier described in this document has been inspected under the parameters setforth and found to be in conformance with the physical requirement we certify the above product meets specified requirement of:



#1822 P. 001/001

1 22:10 2102/21/80

	.032804	Part#:		******.DII	ghtonBest.c			14 (14 (Jacob	Constant of the	
		CER	TIFIE	D MA	TERIA	I. TES	ST RE	PORT		
	FOR	an Shanay	Sheet Street			Santa Barley	1947 (A) C 1948 (A) A	Y HEX	NUTS	
	TORF		A174/E			ADL	414 11 7	I IILA	ne i s	
FACTORY: ADDRESS:	The state of second states	HAIXIN ANG,LUC	A REAL PROPERTY AND A REAL	L. STSPATER SPECIES	LTD. IEJIANG 3	15205	MFG LOT	DATE:	OCT.12.2	and a start
CUSTOMER: QNTY SHIPP SAMPLE SIZ SIZE & DESC	ED: E:	64.800M	P <u>CS</u> D_ASME	Sec. 1	and the second	<u>n) INC</u>	PO	NUMBER: PART NO:		
STEEL PROP STEEL GRAI	DE:	SWRCH4	45K	SLZE	: <u>34mm</u>			HEAT NO:	331	105356
CHEMIST	C%	Mn %	P %	S%	Si %	Cr %	Ni %	Cu %	Mo %	OTHERS
SPE:	MIN	MAX	MAX	MAX	MAX	和法律的	and the second s	and the second	Steer States	in ficato
TECT	0.40	1.00	0.04	0.05	0.40			a name a state		and officer of
TEST:	0.45	0.76	0.011	0.003	0.21	ANG COLORED	18 8 6 1 A 81.	A Starting		
DIMENSION	AL INSPE	CTIONS	ALC: NOT		SPECIE	CATION	ASME/AN	ISL B18.2	2 . 87(R)	(000)
HARACTE	RISTICS	CHOND	TEST M	A PERSONAL PROPERTY AND A PERSON AND A PERS	2.2.3.2.2.5.5.5.5.	IFIED		RESULT	ACC.	REJ.
APPEARANC	CE		ASTM	F812-02		a Bhalannai Gertainn an Stat	PAS	SSED	100	0
WIDTH A/F			1.394"	-1.438"	Start Contract		1.409	'-1.424"	32	0
WIDTH A/C	1			-1.660"				-1.638"	32	0
THREAD		民族建	013771076585777	B1.1-02			A CONTRACTOR	SSED	8	0
HEIGHT MARK	(Jakebride)		C	-0.885" LM	Contraction of the	s-state and	11 Carl 10	"-0.860" SSED	32 100	0
MARK	Contraction of the		in	Trial	and and a	の言語を発	FA.	3360	100	0
MECHANIC	AL PROPE	RTIES:	TO 1-1/2	?" in		SPECIF	ICATION:	ASTM AI	94-10a	
CHARACTE	RISTICS		TEST MI	ETHOD	SPEC	IFIED	ACTUAL	RESULT	ACC.	REJ.
HARDNESS				E18-05	24-35	Contract The second second	and the second se	29-30	5	0
PROOF LOA			Section States	F606-07	808	501bf		Solbf	5.	0
DECARBUR HARDNESS		HAT 540		J121 A 194 M	IN 89 HRB	C Station		SSED B 92-94	1 5	0 0
	TEMPER		2010 11 11 11					D(520 ^O C)	Section of the	Para district
			ASTM E	381	\$1/R1/C1	~\$4/R4/C4		12/C2	5	0
MACROETC		12222-232203000-04		THE STOCK			CA-COLLEGE COLLEGE	CONTRACTOR OF A LAND	MARKED BACK BACK STOLEN	

http://www.brightonbest.com/mtrcenter/getmtr.asp

STAMPING THE FUTURE VROUGHT WASHER MFG., INC.



January 16, 2009

Certification of Compliance

012476 ALBRITTON & GROVES - HOUSTON 3605 WILLOWBEND BLVD. #550 HOUSTON, IX 77054

Wrought Washer Ordr/Lot Number 230425 HT 228734

		Chemic	al Anal	sis	
Heat Number 284276	C 0 350	Ma 0.640	0 008 I	S 0.001	Si 0.213
204270	0.000	0.040	0.000	0.001	0.210

Purchase		Date	Quantity
Order Namber	Part Description	Shipped	Shipped
HARDENFD	7/8 S MARK HT	01/15/2009	30.000

We hereby certify that the subject parts conform to the requirements of the applicable specification indicated for the subject parts and are in complete conformance to F436-04. We hereby certify that the subject parts were hardened to RC 38-45.

We hereby certify that all statutory requirements as to American Production and Labor Standards and all conditions of purchase applicable to the transaction have been complied with and that the subject parts were melied and manufactured in the U.S.A.

I'mly yours. Wrought Washer Mfg., Inc. 124.SI

Paul Schnefer Q.C. Manager

Sugan M. Daoust

Sworn and subscribed before me on January 16, 2009 My commission expires June 21, 2009



(0.9) SMARK, ITE 1436 WW INTERNAL USE (53628901/016/017308/38521

1901 CHICORY RD. • MOUNT PLEASANT, WI 53403 • PHONE (262) 554-9550 • FAX (262) 554-9584 VISIT OUR WEBSITE: www.wroughtwasher.com

(1 STE	STEEL TEXAS EL MILL DRIVE N TX 78155-7510	CERTIFIED MILL TE For additional co 830-372-8	opies call	accurate and confo	fy that the test results form to the reported grad Actual for Achaeck Daniel J. Schacht Jailty Assurance Manager	de specification
HEAT NO.:3011321 SECTION: ROUND 1/2 x 20'0" A36/52950 GRADE: ASTM A36-08/A529-0 ROLL DATE: 08/15/2009 MELT DATE: 08/14/2009	S Madden Bolt Cor O L 13420 Hempste 5 Gr 50 D Houston TX US 77040-5813 T 7139399999 O 7139397200	ad Rd	S Madden Bolt Corp H 1 I 13420 Hempstead Rd P Houston TX US 77040-5813 T 7139399999 O 7139397200		Delivery#: 80199515 BOL#: 70063367 CUST PO#: PE33988 CUST P/N: DLVRY LBS / HEAT: 4 DLVRY PCS / HEAT: 5	562.000 LB
Characteristi	c Value	Charact	eristic Value		Characteristic	Value
	P 0.008% S 0.039% Si 0.19% U 0.15% Cr 0.16% Vi 0.09% 0 0.033% V 0.008% tb 0.001% I 0.002% 9 0.36% 1 51.6ksi 1 77.5ksi 1 29%	A A			4	

THIS MATERIAL IS FULLY KILLED, 100% MELTED AND MANUFACTURED IN THE USA, WITH NO WELD REPAIR OR MERCURY CONTAMINATION IN THE PROCESS. REMARKS :

89

2012-10-25

10/02/2009 20:07:59 Page 1 OF 1

BLR466	TANK - A CONTRACT OF A CONTRACT	STE 500	XO CORP ONIAL CENTER PKWY .L, GA 30076-	NUCOR CORPORATION NUCOR STEEL TEXAS	CERTIFIED MILL TEST REPO Ship from: Nucor Steel - Texas	RT Page: 2
	Server	SHIP NAMASC TO: SOUTH L BUDA, TX	.00P 4		5812 Hwy 79 W JEWETT, TX 75846 800-527-6445	Date: 14-Oct-201 B.L. Number: 585706 Load Number: 196747
	Fax	Meterial Safety Dat	a Sheets are available et www.nucorba	ar.com or by contacting your inside sates represent PHYSICAL TESTS		NEWCAL TESTS
6501		HEAT NUM. *	DESCRIPTION	MELO TEMPLE CLOWD	END WTS DEF C No Min Cr Mo	S V SI CL CU Sn
BL - 3674880 Heat - JW1110866501 Order-Line - 6970700 / 6	8:28:59 AM PAGE 4/004	P0# ⇒ JW1110866601 P0# ⇒ JW1110866601	6389968 Nucor Steel - Texas 3/4x10" Fist 20' A529 GISS ASTM A529/A52914-05 GR 55	58.900 76,500 21.0% 406MPa 527MPa 58,200 76,000 19.0% 401MPa 524MPa 9 PARB 3.1B & EN 10204-3.1 58.900 76.500 21.0% 406MPa 527MPa 58,200 76,000 19.0% 401MPa 524MPa 9 PARB 3.1E & EN 10204-3.1	.11 1.06 .018 .12 .17 .034 CBV CEA529 MN 0.040 0.40 09.6 .11 1.06 .018 .12 .17 .034 CBV CEA529 MN 0.040 0.40 09.6	a .003 .032 MC 54 3 .039 .20 .38 4 .003 .032 MC
Load - 1110207	10/17/2011					
11-21-2011 04:12 Brazos Industries Inc Cust. PO -	Nucor Steel					Martes

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2012-10-25

	1																											
		D: \$270471 Page 5 of 31	CHARLOTTE STEEL MI 6601 LAKEVIEW FOAD CHARLOTTE NC 26266 (704) 596-0361	ŁL	A											Physics D STAT		rt Rep	ort									ugo 7 of 563085
			SHEP TO NAMASCO CORP SOUTH LOOP 4, EXIT 2 512-472-5533 BUDA, TX 78610	17						NAM ***A 500	CCT	S PAY	ABLE"		WY S-5(00				01/1: CUS		COUNT	NO					
63			PRODUCED IN: CHAP																									
C017163 1/5			SHAPE + SIZE 55/8		GRADE			ICATION 36-08 AAS	ME SA	156-08	A8 A	STM A7	09-07										00133-00			IST P.O.		ĸ
Heat - C01 7140964 / 5			HEATI.D. C		Man	P	\$	51 0	1	Ně	Cr	Ma	V	PR)		CENN		1	<u> </u>	[[1	1					
23			C0317163 .1			.012	.038	.19 .4	S	12	.08	.020				.37		1]	Presson of	I	1]			· ·		
Heat -		8	Mechanical Test: Yield Customer Provisionis CA		G: STRA			ensile: 725	us (*3),	, 499.9	MPA	-%EI;	23.008	1, 2380	ZDUAIM	Hed H	04											
rder-Lin		PR Office Prr 14																										
Order-Line		Nen E Gerdau - Tanpa Office Pre 14																										
Order-Lin		News Geodes - Tange Office Pr. 14	Customer Notes NO WELD REPARMENT Dris meterial, including the bil States of Amorica Amarcha	lets,	अवक मार्स	Necl and Lithu	menudaa skar Yala iity Direu	stureod in sta ernanchili			янγ.			146 PON	MANENT	FIGURES RECOR	DS OF	COMP	NY.	MK AL I	Metalh	uryicad S	TEST R	an nakher	6 AS C	XIAN	ëd in Th	E

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2012-10-25

02-14-2012 12:03 Load - 1168331 BL - 3681309 **BLR466** Heat - A60808 Brazos Industries Inc Cust. PO -Order-Line - 7140964 / 3 P. 004/005 JAN-18-2012(WED) 16:39 RTLAS TUBE 888 Tube Bate: 80460814 Customer: 980 Atles Tube Inc. 5039N County Road 1015 Blythavilla, Arkansas, USA 72310 Tel: 870-838-2000 Fax: 870-752-6630 **DDD** JMC STEEL GROUP MATERIAL TEST REPORT Sold to Shipped to NAMASCO CORPORATION Steel Warehousing Corporati 500 COLONIAL CENTER PR ROSWELL GA 30076 USA NAMASCO SOUTH WEST SOUTH LOOP 4, P.O. BOX BUDA TX 78715-0367 Material: 5.0x3.0x250x40'0'0(4x3). Material No: 500302504000 Made In: USA Motted In: USA Sales order: 675809 Purchase Order: 6392958 Cust Material #: T5314RECTA5000480 Al Cu Cb Ni Cr V Ti Heat No C P SI Mo B Nin S 0.218 0.790 0.009 0.009 0.009 0.009 0.041 0.030 0.000 0.000 0.010 0.040 0.000 0.001 0.000 0.000 35461D PCs Yield Ein.Zin . Bundle No Tenslia Certification CE: 0.35 M400040721 12 061160 Psi 071150 Psi 31 % ASTM ASOD-10A GRADE B&C 1 Meterial Note: Seles Or.Note: Material: 6,0x2.0x250x40'0'0(3x4). Material No: 600202504000 Made In: USA Molted In: USA Sales orden: 070803 Purchase Orden: 6392958 Guat Material #: T6214RECTA5000490 71 Heat No. ĉ AI Cu Cb N Gr v в Ma P 5 Si Mo N A60808 0.220 0.810 0.012 0.003 0.030 0.023 0.100 0.000 0.020 0.050 0.060 0.001 0.001 0.000 0.000 Bundlo No PCs Yield Tensile En.2h Certification CE: 0.39 M400040785 12 065300 Psi 078930 Psi 29 % ASTM ASCO-10A GRADE B&C Material Note: Sales Or Note: Material: 6.0x2.0x260x40'0"0(3x4). Material No: 500202804000 Made in: USA Molted In: USA Salas order: 676809 Purchase Order: 6392958 Cust Material #: T6214RECTA5000480 Al Cu Cb Cr v ті в C Ρ Si Ni Heat No. Mn S Mo N 0.030 0.023 0.100 0.000 0.020 0.050 0.060 0.001 0.001 0.000 0.000 A50808 0.810 0.012 0.003 0,220 Bundle No PCs Yield Termus Ein,2In M400040786 12 066300 Psi 078930 Psi 29 % Certification CE: 0.39 ASTM ASOD-104 GRADE B&C ų, Meterial Note: Salas Or.Note: Al Obel Authorized by Quality Assurance: The results reported on this report represent the astual attributes of the material furnished and indicate full compliance with all applicable specification and contract requirements. In the state of the material furnished and indicate full compliance with all applicable specification and contract requirements. In the state of the material furnished and indicate full compliance with all applicable the state of the material furnished and indicate full compliance with all applicable the state of the material function of the state of the material furnished and indicate full compliance with all applicable applicable for the state of the state of the material furnished and indicate full compliance with all applicable applicable for the state of the state of the material furnished and indicate full compliance with all applicable applicable for the state of the state of the state of the material furnished and indicate full compliance with all applicable applicable for the state of 🐼 Metals Service Center Institute institute Page : 2 Of 3

Namasco

Namascu

-14-2012 12:03 azos Industries Inc	oad - 1168	331	BL - 3	681309 Heat - 51	5678			BLR46
st. PO -			Order-Line	- 7140964 / 2	2	a a a di Mani Real ang a di Mana ana ang di Mana ang di Sang di	5. - 1 M	
S Sol		The contract of the second sec		3.	525 Rich	ard Arrington, Ju Birmingham, Phone (205 Lab Fax (205 Lab@Southlan	AL 35234) 251-1884) 421-4561	
*****		TES	T REP	ORT				
Customer Name: Customer PO No:		CORPORATIO	IN LTD					
Heat No.: Description: Size/Length:	515678 CARBON S 2" X 6" 1/4"	TEEL TUBINC 'Wall 40'	;	Spee/Grad Print Date Wall Thic	:	A500-10/B/C 2/9/2012 0.2500		
Carbon (C); Manganese (Mn): Phosphorus (P); Sulphur (S): Silicon (Si); Copper (Cu):	0.2000 0.4300 0.0100 0.0110 0.0120 0.0380	Tin (Sn): Nickel (Ni): Chromium (Molybdenu Aluminum Nitrogen (N	(Cr): m (Mo): (Al);	0.0020 0.0150 0.0430 0.0060 0.0360 0.0037	Coli Tita Bor Cale	adium (V): umbium (Cb): nium (Ti): on (B): cium (Ca): bon Equiv, (CE)	0.0010 0.0000 0.0010 0.0001 0.0000 : 0.2852	
Sample Number		Sample Date	Tens (psi		Yield (psi)	Êlong (%		
SL31866	2/6/2012 6		68.40	58,400 56,200		0 26.00		

We hereby certify that the above figures are correct as contained in the records of this company. Tensile testing (if applicable) is performed according to ASTM A370 and ASTM E8 (Yield Strength determined using 0.2% offset method).

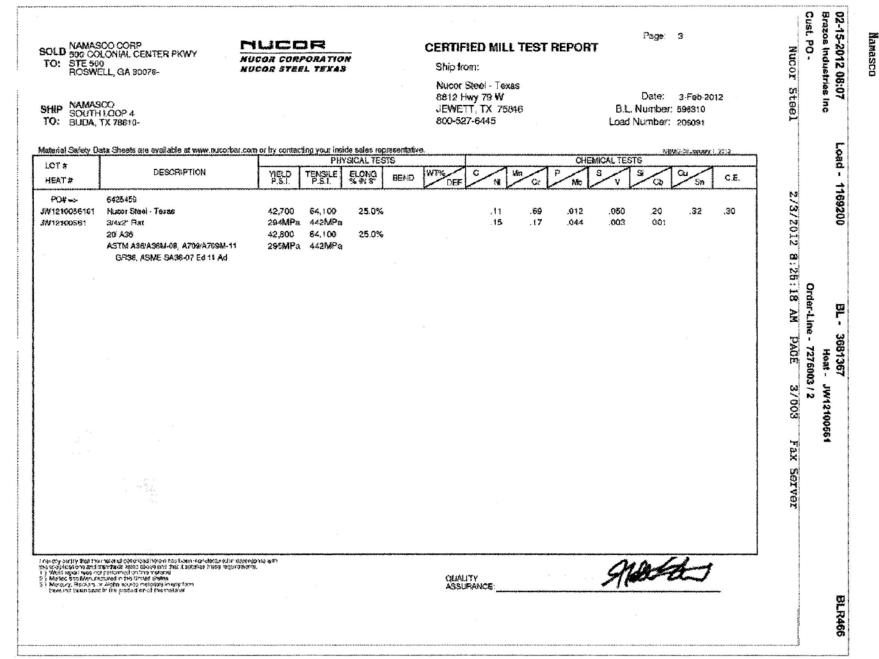
Computer Generated Document

Melted & Manufactured in the U.S.A.

Quality Assurance

STI Pickup No: 021.3081 STI Order No: 264127

STI Item No: 2.0X6.025040



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2012-10-25

O: 500 (STE ROS	ASCO CORP COLONIAL CENTER PKWY 500 WELL, GA 30076- ASCO TH LOOP 4 A, TX 78610-	NUCOR C NUCOR S	ORF	ORATIO	-		Ship from: Nucor Ste 8812 Hwy	el - Texas 79 W TX 75846	test re			mber: 5	7-Feb-2012 96570	2	Cust. PO -	02-15-2012 08:07 Brazos Industries Inc
daterial Sale	ly Data Sheets are available at www.nuccrbar	com or by cont	acting	your inside	sales repre	sentative.						ra:	MG-08 Jar vary '	1,2912		Load -
LOT #	DECODINTION				SICAL TES	75	1			And the second second	AL TESTS		- 7			а ,
HEAT #	DESCRIPTION	YIE P.S	1.	TENSILE P.S.J.	ELONG %IN 8	BEND	WT% DEF	C N N	n cr p	MOS	V	3	CU En	G.E.		1169200
																392
PO# =>	6425459 9701 Nucor Steel - Texas	48.3	00	68,000	25.0%			.15	.70	.017	.030	.21	.32	.35		8
JW111103				469MPa				.*0	.22	.050	.004	.002	-32	.30		
	20' A35	48,5		68,000	26.0%			.70			.004	.046				
PO#>	ASTM A36/A36M-08, A709/A709/ GR36, ASME SA36-07 Ed 11 A 6425459		MPa	469MPa											0	
W1210041	-	48.4	00	65.200	26.0%			.12	.63	.016	.030	.20	.36	.29	rde	
JW1210041				450MPa				.11	.14	.036	.002	.002			17	
204	20" A36 ASTM A36/A36M-08, A709/A709/ GR36, ASME SA36-07 Ed 11 A 6425459	4-11 341	00 MPa	66,300 457MPa	27.0%										Order-Line - 7276003 / 1	36
PO# => JW1210060		50.1	00	68.300	25.0%			.11	.70	.008	.030	.21	.33	.31	60	31367 Heat -
JW1210060				471MPa				.19	.17	.054	.002	.003			8	
	20' A36	50,6		68,400	25.0%										1	¥.
PO#=>	ASTM A36/A36M-08, A709/A709/ GR35, ASME SA36-07 Ed 11 # 6425459		MPa	472MPa												JW11110387
JW1210078		53.5	00	71,300	24.0%			.11	.86	.007	.035	.22	.32			87
JW121007				492MPa				.17	.13	.044			.012			ł
	20" A36'A529 G/50	54,7		72,400	27.0%			AL								
	ASTM A36-08, A529-05, A709-09 R 36, ASME SA36-07 Ed 11 Ac		MPa	499MPa				0.000	0.32	0.36	0.001					
haraby onti be specificat i Neltice i Neltice ki Nescurg, kive act	(b) short the destorial factor rate be- tions one standards listed between the tit. at we not performed as this statement. At the protection of the destored the statement and the statement of the destored the statement backs used in the graduenties of this natural.	n vernfammeri razisfiss chase s	16 03 29%-1	an Aard wit retaint,	£.		QUALITY Assoran	:R: Natin	an Stewart	5	M	H	£	· .		BLR466

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2012-10-25

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PAGE 01

Atlas Tube Canada ULC 200 Clark St. Harrow, Ontario, Canada			
NOR 1G0 Tel: 519-738-3541 Fax: 519-738-3537	۰.		
		ŕ	MAT
Caldia			



Ref.B/L: 80426715 Date: 04.18.2011 Customer: 193

ERIAL TEST REPORT

Sold	to									*	Sh	ipped to	2		
USA	, ,		Kwa	Ϋ́.	: 		•			•	US	a		ad	ŗ
Material: 4.500 Sales order: 6		2'0"0(19x1)	CSA				٦,	01884200	CSA				: Canad n: Canad	_	•
Heat No	с	Mn	P	\$	Si	Al	Cu	СЬ	Мо	Ni	Cr	V	Π	в	N
758508 Bundle No	0.190 PCs	0.790 Yield	0.017 Ter	800.0	0.010 Ein.2in	0.000	0.044	0.005 (0.005 rtificatio	0.016	0.055	0.002	0.000 CE: 0.34	0.000	0.000
M100997855 Material Note: Sales Or.Note	19	058520 Ps	066	240 Psi	30.0 %	·				1-04 50W	CLASS				
Material: 4.500 Sales order: 6 Heat No		2'0"0(19x1) Mn	CSA P	s	,			01884200 D-022403 Cb	-CSA	NI	Ст		: Canad in: Canad 11	-	N
758508 - Bundle No	0,190 PCs	0.790 Yield	0.017 Ter	0.008 naile	0.010 Ein.2in	0.000	0.044	0.005 (Ce	0.005 Intificatio	0.016 on	0.055	0.002	0.000 CE: 0.34		0.000
M100997853 Material Note: Sales Or.Note	19 Meets	058520 Pel		240 Pal	30.0 %			CS	A G40.2	1-04 50W	CLASS			`~	
Material: 10.0	00x250x	48'0"0(2x1).			M	aterial No	: R1600	02504800					in: Canad		
Sales order:	630305				PL	irchase (Order: P	0-022558					•		
Heat No	C	Mn	P	\$	Si	A	Cu	Cb	Mo	Ni	Cr	¥.	TI	В	N
759207	0.180	0.770	0.009	0.008	0.015	0.038	0.047	0.006	0.004	0.013	0.046	0.002	0.000	0.000	0.000
Bundle No	PCs	Yield	Ter	nsile	Ein.2in			Ce	rtificatio	on			CE: 0.33		
M200738165	2	050900 Psi	07	220 Psi	35.0 %			AS	TM A50	0-07 GRA	DE B&C		,		

Material Note: Sales Or.Note:

Authorized by Quality Assurance: The results reported on this report represent the actual attributes of the material furnished and indicate full compliance with all applicable specification and contract requirements. Steel Tube: 10.1 method.



Page: 1 Of 2

Metals Service Center institute



CMC STEEL TEXAS 1 STEEL MILL DRIVE SEGUIN TX 78155-7510 CERTIFIED MILL TEST REPORT For additional copies call 830-372-8771 We hereby certify that the test results presented here are accurate and conform to the reported grade specification

Daniel J. Schacht

Quality Assurance Manager

76

HEAT NO.:3028494	s	CMC Construction Svcs College Stati	S	CMC Construction Svcs College Stati	Delivery#: 80669347
SECTION: REBAR 16MM (#5) 20'0"	0		н		BOL#: 70236513
420/60	L	10650 State Hwy 30	1	10650 State Hwy 30	CUST PO#: 5434V
GRADE: ASTM A615-09b Gr 420/60	D	College Station TX	P	College Station TX	CUST P/N:
ROLL DATE: 11/18/2011		US 77845-7950		US 77845-7950	DLVRY LBS / HEAT: 45990.000 LB
MELT DATE: 11/14/2011	Т	979 774 5900	Т	979 774 5900	DLVRY PCS / HEAT: 2205 EA
	0		0		

Characteristic	Value	Characteristic Value	Characteristic Value
C	0.38%		
Mn	1.00%		
Р	0.015%		
S	0.030%		
Si	0.22%		
Cu	0.33%		
Cr	0.21%		
Ni	0.19%	,	
Mo	0.088%		
v	0.003%		
Cb	0.001%		
Sn	0.013%		
AI	0.002%		
Yield Strength test 1	68.3ksi		
Tensile Strength test 1	108.1ksi		
Elongation test 1	15%		
Elongation Gage Lgth test 1	8IN		
Bend Test Diameter	2.188IN		
Bend Test 1	Passed		

THIS MATERIAL IS FULLY KILLED, 100% MELTED AND MANUFACTURED IN THE USA, WITH NO WELD REPAIR OR MERCURY CONTAMINATION IN THE PROCESS. REMARKS :

s.,

01/17/2012 21:56:23 Page 1 OF 1



CMC STEEL TEXAS 1 STEEL MILL DRIVE SEGUIN TX 78155-7510 CERTIFIED MILL TEST REPORT For additional copies call 830-372-8771 We hereby certify that the test results presented here are accurate and conform to the reported grade specification

> Aerief J. Achaeter Daniel J. Schacht

Quality Assurance Manager

TR No. 9-1002-12-2

HEAT NO.:3029770	S	CMC Construction Svcs College Stati	S	CMC Construction Svcs College Stati	Delivery#: 80681077
SECTION: REBAR 13MM (#4) 20'0"	0		н		BOL#: 70240462
420/60	L	10650 State Hwy 30	1	10650 State Hwy 30	CUST PO#: 53534v
GRADE: ASTM A615-09b Gr 420/60	D	College Station TX	Ρ	College Station TX	CUST P/N:
ROLL DATE: 01/22/2012		US 77845-7950		US 77845-7950	DLVRY LBS / HEAT: 43820.000 LB
MELT DATE: 01/15/2012	Т	979 774 5900	т	979 774 5900	DLVRY PCS / HEAT: 3280 EA
	0		0		

Characteristic	Value	Characteristic	Value		Characteristic	Value
с	0.45%					
Mn	0.83%					
P	0.009%					
S	0.034%					
Si	0.18%					
Cu	0.41%					
Cr	0.15%					
Ni	0.22%		Υ.			
Mo	0.070%					
v	0.002%			- x		
Cb	0.002%					
Sn	0.014%					
AI	0.002%					
Yield Strength test 1	65.7ksi					
Tensile Strength test 1	102.8ksi					
Elongation test 1	12%					
Elongation Gage Lgth test 1	8IN					
Bend Test Diameter	1.750IN					
Bend Test 1	Passed					
Dona Tost T	1 43354					

THIS MATERIAL IS FULLY KILLED, 100% MELTED AND MANUFACTURED IN THE USA, WITH NO WELD REPAIR OR MERCURY CONTAMINATION IN THE PROCESS. REMARKS :

1. 1.

02/02/2012 23:04:38 Page 1 OF 1

APPENDIX C. RESULTS FOR MASH TEST 3-10 (TEST NO. 490022-2).

C1. TEST VEHICLE PROPERTIES AND INFORMATION

		Tabl	e C1. Veh	icle Prop	erties for I	Test No. 4	90022-2.		
Date:	2012-04-	09	Test No.:	490022-	2	VIN No.:	KNADC12	258563649 ⁻	18
Year:	2005		Make:	Kia		Model:	Rio		
Tire Infla	ation Press	sure: <u>30</u>	psi	Odomet	er: <u>133137</u>		Tire Size:	175/65R14	4
Describe	e any dam	age to the	vehicle prio	r to test:					
• Deno	tes accele	rometer lo	cation.				A	CCELEROMETERS	
NOTES	:								WHEEL N T
Engine Engine	CID:	4 cylinder							
<u>x</u> / <u>x</u> /		or RWD	_ Manual 4WD						
	– – osition:	166 lb Front pass	entile male senger			W			
Geome	-	_	20.00	IZ.	40.00	P	 0.05		 4 E E O
A B	62.50 56.12	. F G	32.00	_ K_ _	12.00 24.25	 	3.25 22.50	_ U V	<u>15.50</u> 21.50
	164.25	. <u>с</u> _	35.38	_ L _ M	56.50	 	15.50	- v	35.00
D	37.00	· ·· _	8.50	-	57.00		8.62	-	104.50
E	95.25	<u> </u>	22.75	0	28.00	. в _ Т	63.00		101100
	Center Ht F	· -	10.75		enter Ht Rea		1.125		
GVWR	Ratings:		Mass: Ib	<u>C</u>	<u>urb</u>	Test	Inertial	Gros	s Static
Front		1691	M _{front}		1521		1528		1610
Back		1559	M _{rear}		852		903		987
Total		3250	M _{Total}		2373		2431		2597
					Allowable TI	M = 2420 lb ±	55 lb Allowab	le GSM = 258	5 lb ± 55 lb
Mass D Ib	istributio	n: LF:	790	RF:	738	LR:	458	RR:4	45

Date:	2012-04-09	Test No.:	490022-2	VIN No.:	KNADC125856364918	
Year:	2005	Make:	Kia	Model:	Rio	

Table C2. Exterior Crush Measurements for Test No. 490022-2.

VEHICLE CRUSH ME	ASUREMENT SHEET ¹
Complete Whe	en Applicable
End Damage	Side Damage
Undeformed end width	Bowing: B1 X1
Corner shift: A1	B2 X2
A2	
End shift at frame (CDC)	Bowing constant
(check one)	X1+X2 _
< 4 inches	2
\geq 4 inches	

Note: Measure C_1 to C_6 from Driver to Passenger side in Front or Rear Impacts – Rear to Front in Side Impacts.

a : c		Direct I	Damage								
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	C ₁	C ₂	C ₃	C ₄	C ₅	C ₆	±D
1	Front plane at bumper ht	19.0	10.0	24	0	4.0	5.5	6.5	7.5	10.0	-14
2	Side plane at bumper ht	19.0	11.0	36	0	1.25	4.0	6.0	8.0	11.0	
	Measurements recorded										
	in inches										

¹Table taken from National Accident Sampling System (NASS).

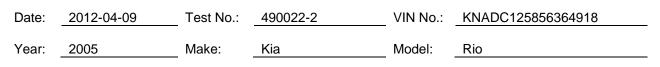
*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

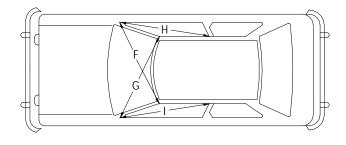
**Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

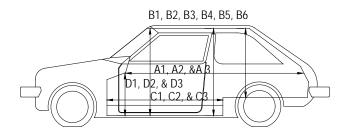
***Measure and document on the vehicle diagram the location of the maximum crush.

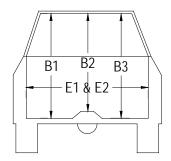
Note: Use as many lines/columns as necessary to describe each damage profile.











OCCUPANT COMPARTMENT DEFORMATION MEASUREMENT

	Before (inches)	After
	(<i>,</i>	(inches)
A1	67.25	67.25
A2	65.00	65.00
A3	37.25	66.75
B1	39.25	39.25
B2	35.50	35.50
B3	39.25	40.25
B4	34.75	34.75
B5	35.00	35.00
B6	34.75	34.75
C1	26.75	26.75
C2		
C3	26.50	23.50
D1	10.75	10.75
D2		
D3	8.75	8.25
E1	49.00	49.25
E2	50.50	53.50
F	49.25	49.50
G	49.25	47.75
Н	36.50	36.50
I	36.50	36.50
J*	50.25	49.00

*Lateral area across the cab from

driver's side kickpanel to passenger's side kickpanel.









0.149s

0.186 s

0.223 s



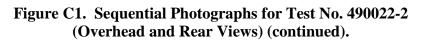












0.260 s



0.000 s



0.038 s



0.076 s



0.112 s 0.260 s Figure C2. Sequential Photographs for Test No. 490022-2 (Rear of Bridge Rail View).



0.149 s



0.186 s



0.223 s



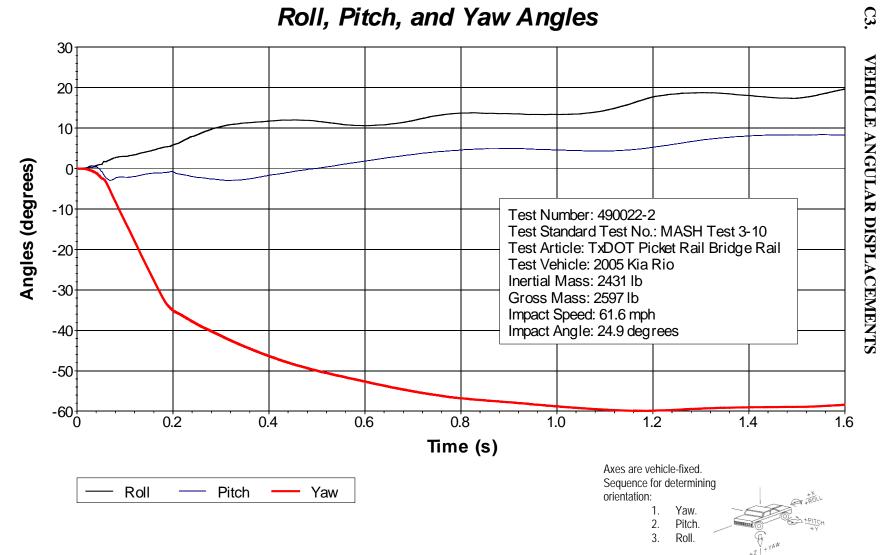


Figure C3. Vehicle Angular Displacements for Test No. 490022-2.

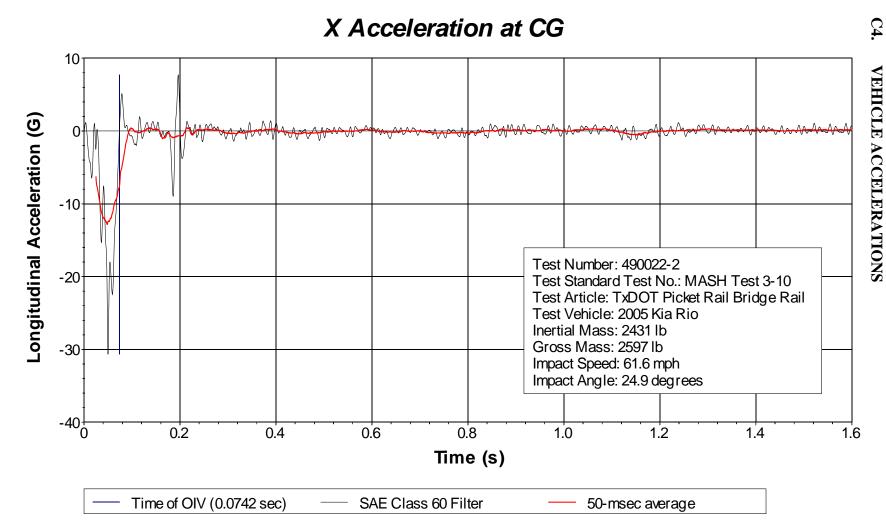


Figure C4. Vehicle Longitudinal Accelerometer Trace for Test No. 490022-2 (Accelerometer Located at Center of Gravity).

98

2012-10-25

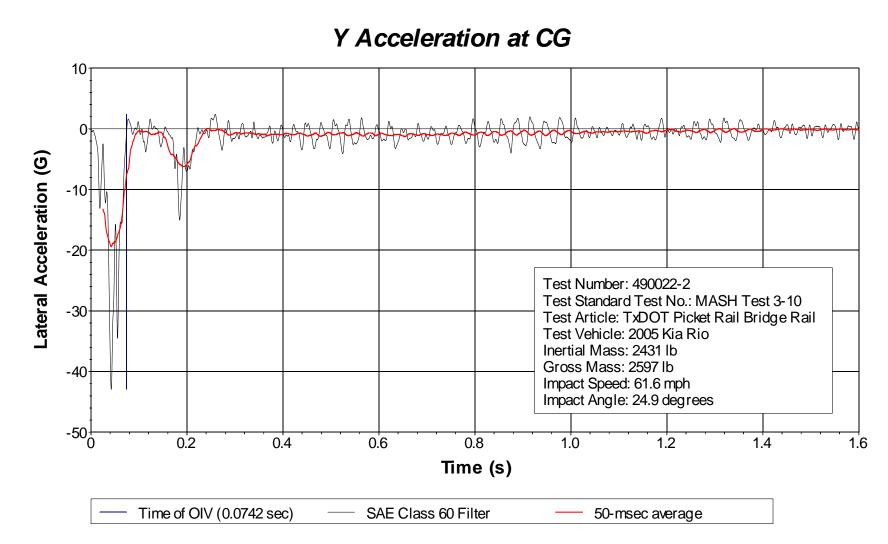


Figure C5. Vehicle Lateral Accelerometer Trace for Test No. 490022-2 (Accelerometer Located at Center of Gravity).



Z Acceleration at CG

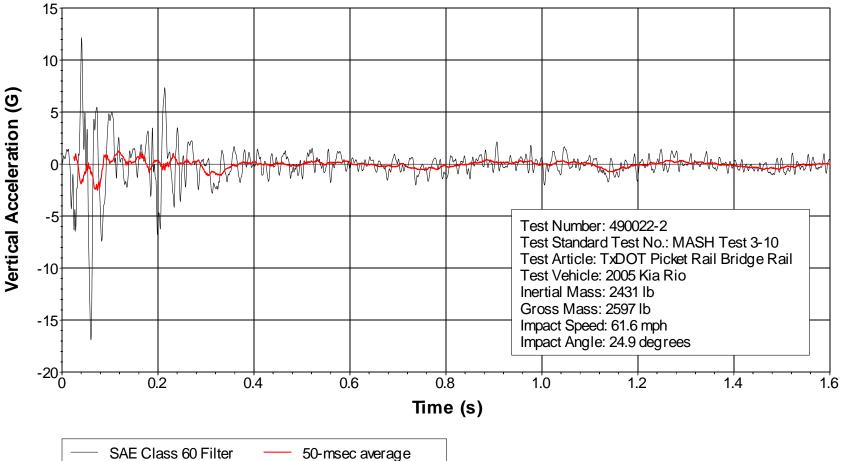


Figure C6. Vehicle Vertical Accelerometer Trace for Test No. 490022-2 (Accelerometer Located at Center of Gravity).

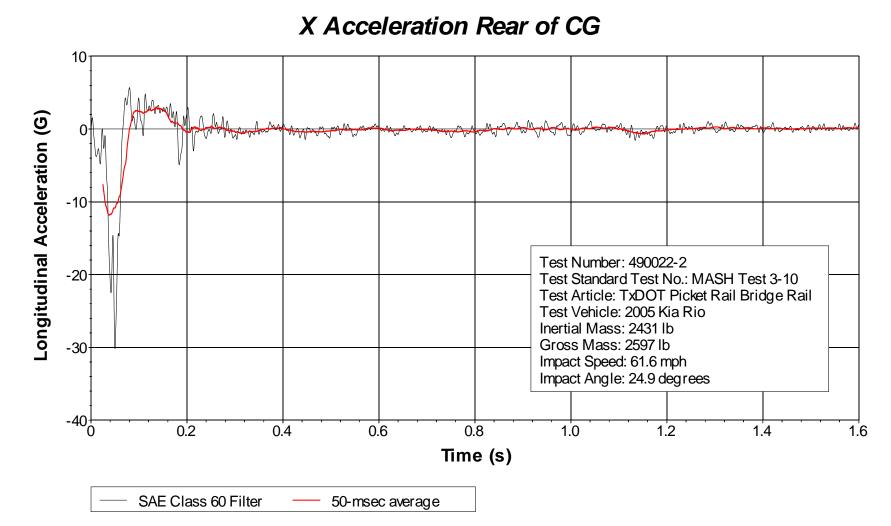


Figure C7. Vehicle Longitudinal Accelerometer Trace for Test No. 490022-2 (Accelerometer Located Rear of Center of Gravity).

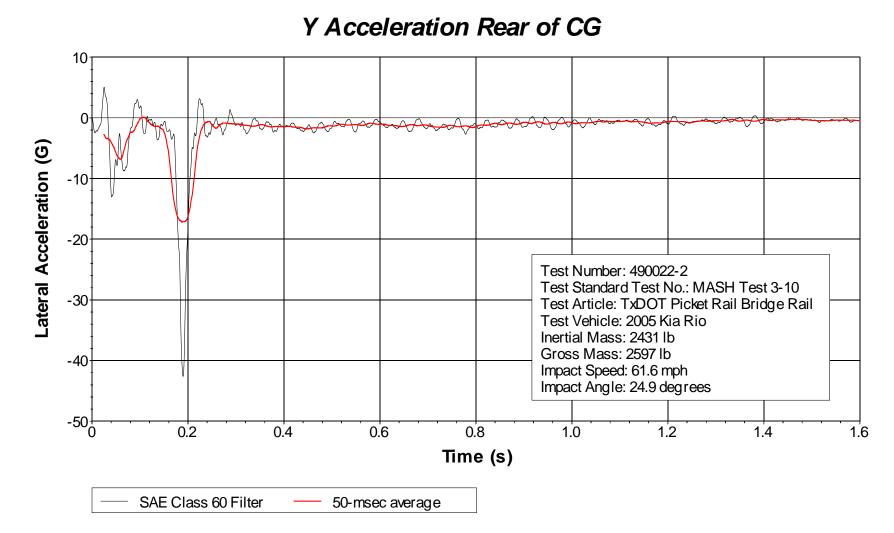


Figure C8. Vehicle Lateral Accelerometer Trace for Test No. 490022-2 (Accelerometer Located Rear of Center of Gravity).

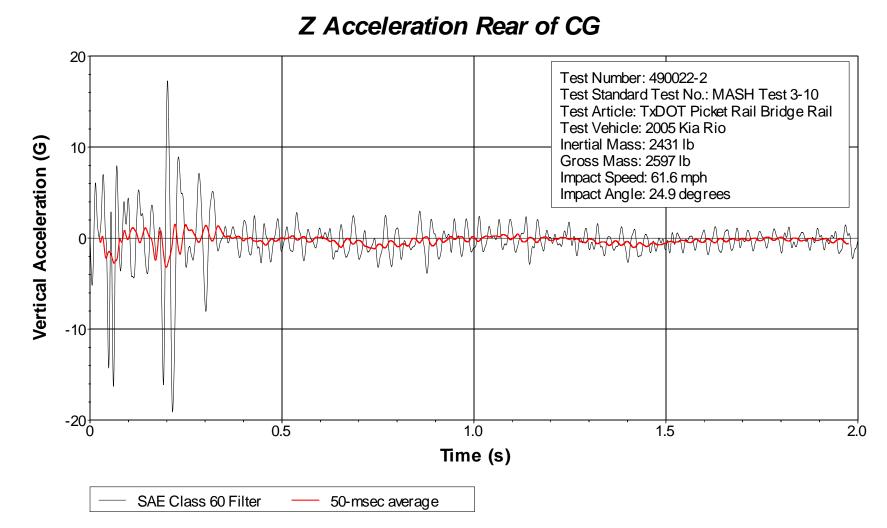


Figure C9. Vehicle Vertical Accelerometer Trace for Test No. 490022-2 (Accelerometer Located Rear of Center of Gravity).

APPENDIX D. RESULTS FOR MASH TEST 3-11 (TEST NO. 490022-3).

D1. TEST VEHICLE PROPERTIES AND INFORMATION

Table D1. Vehicle Properties for Test No. 490022-3.											
Date:	te: 2012-04-10		Test No.:	490022-3		VIN No.:	1D7HA18X65708197				
Year:	2006			Make:	Dodge		Model:	Ram	1500		
Tire Siz	e: <u>2</u>	265/70F	R17			Tire I	nflation Pre	ssure:	35 psi		
Tread T	ype: I	Highwa	у				Odo	meter:	129282		
Note an	y damag	ge to th	e veł	nicle prior to t	est:						
 Deno 	tes acce	elerome	ter lo	ocation.		-	— W —	_ X			
NOTES	:				. 1						
Engine Engine	• •				A 			•			
x	ission Ty Auto FWD	or	ND.	_ Manual 4WD	1	- Q -				> TEST INE	ERTIAL C.M.
	l Equipn			1112							
Dummy Type:	Data:	No d	umm	ıy					G A	\bigcirc	
Mass: Seat P	osition:				- ' 	- F	— H - ont	——• E —	I	M _{re}	ear - D
Geome	-	nches			-			- C -			
Α	78.25		F _	36.00	K	20.50	P _	2.88		U	28.50
В	75.00		G _	28.25	_ L	29.12	Q _	31.25		V	29.50
	223.75		Η	61.51	M	68.50		18.38		W	60.50
D	47.25		<u>ا</u> _	13.75	<u> </u>	68.00		12.00		X	78.00
Whe	140.50 eel Center eight Front		J_	25.38 14.75 Cle	O Wheel Wel arance (Front		T) n Frame it - Front		17.12
Whe	eel Center				Wheel Wel earance (Rear)		10.25	Botton	n Frame nt - Rear		24.75
									_	0	
	Rating			Mass: Ib	<u>C</u>	urb 0050	lest	Inertial		Gros	s Static
Front		3700	-	M _{front}		2852		2821	_		
Back		3900	-	M _{rear}		2166		2197	_		
Total		6700	-	M _{Total}		<u>5018</u> (Allowa	ble Range for	5018 TIM and (0 lb ±110) lb)
Mass D Ib	istributi	ion:	LF:	1430	RF:	1391	LR:	1058	RR		139

Table D2. Vehicle Parameters for Test No. 490022-3.

Date: 2012-04	<u>-10</u> Te	st No.: 4	90022-3	<u></u> ۱	/IN: <u>1D</u>	7HA18X6	570819	97	
Year: 2006		Make: D	odge		Model:	Ram 150			
Body Style: _Q	uad-Cab			Mileage: <u>129282</u>					
Engine: Transmission: Automatic									
Fuel Level: Er	mpty	Balla	st: <u>100</u>	b at front	of bed			(440 lb	max)
Tire Pressure: I	Front: <u>3</u>	5 psi	Rear	35	osi S	ize: 265	/70R17	7	
Measured Vehicle Weights: (lb)									
LF:	1430		RF:	1391		Front	t Axle:	2821	
LR:	1058		RR:	1139		Rear	· Axle:	2197	
Left:	2488		Right:	2530			Total:	5018	
							5000 ±11	0 lb allow ed	
Wh	eel Base:	140.5	inches	Track: F:	68.	5 inches	R:	68	inches
148 ±12 inches allow ed				Track = (F-	+R)/2 = 67 ±1	.5 inches	s allow ed		
Center of Gravity, SAE J874 Suspension Method									
X:	61.51	in	Rear of F	ront Axle	(63 ±4 incł	nes allow ed)			
Y:	0.29	in	Left -	Right +	of Vehic	le Center	line		
Z:	28.25	in	Above Gr	ound	(minumum	28.0 inches a	allow ed)		
Hood Heigh		44.50 thes allowed	inches	Front B	umper H	eight:	2	5.375 inc	hes
Front Overhang:36.0		36.00	inches	Rear Bumper Height: 29.125 inche			hes		
	39 ±3 inc	hes allowed							
Overall Length	า:	223.78	inches						
	237 ±13	inches allowed	b						

Table D3. Exterior Crush Measurements for Test No. 490022-3.

Date:	2012-04-10	Test No.:	490022-3	VIN No.:	1D7HA18X65708197			
Year:	2006	Make:	Dodge	Model:	Ram 1500			

VEHICLE CRUSH MEASUREMENT SHEET¹

Complete Wh	en Applicable					
End Damage	Side Damage					
Undeformed end width	Bowing: B1 X1					
Corner shift: A1	B2 X2					
A2						
End shift at frame (CDC)	Bowing constant					
(check one)	X1+X2 _					
< 4 inches						
\geq 4 inches						

Note: Measure C_1 to C_6 from Driver to Passenger side in Front or Rear Impacts – Rear to Front in Side Impacts.

a : a		Direct Damage									
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	C1	C ₂	C ₃	C4	C5	C ₆	±D
1	Front plane at bumper ht	17.0	11.0	30	0	1	2.5	11	9	11	+15
2	Side plane at bumper ht	17.0	11.0	10	1					11	+68
	Measurements recorded										
	in inches										

¹Table taken from National Accident Sampling System (NASS).

*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

**Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

***Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

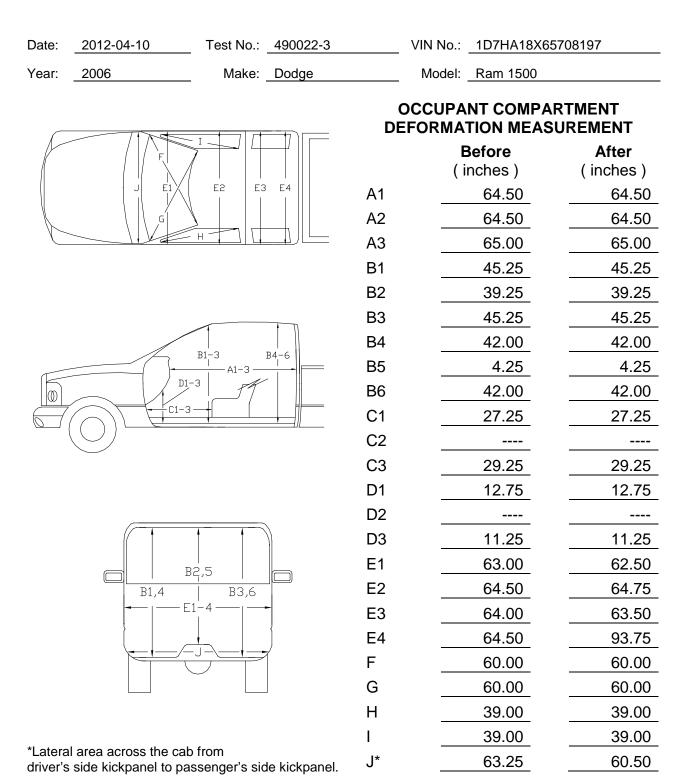


Table D4. Occupant Compartment Measurements for Test No. 490022-3.

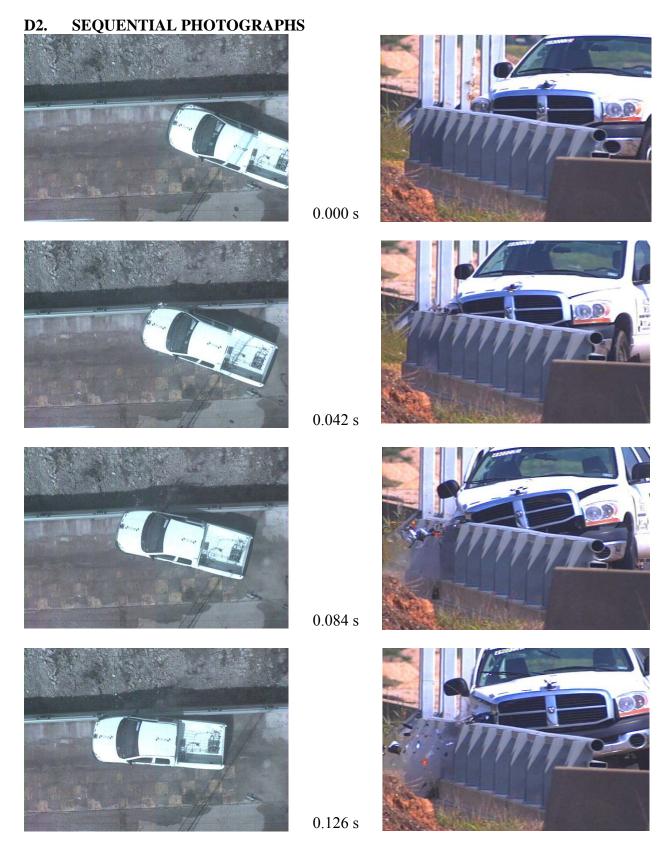


Figure D1. Sequential Photographs for Test No. 490022-3 (Overhead and Frontal Views).











0.168 s

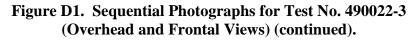
0.210 s

0.252 s









0.295 s



0.000 s



0.042 s



0.084 s





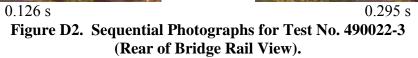


0.210 s



0.252 s





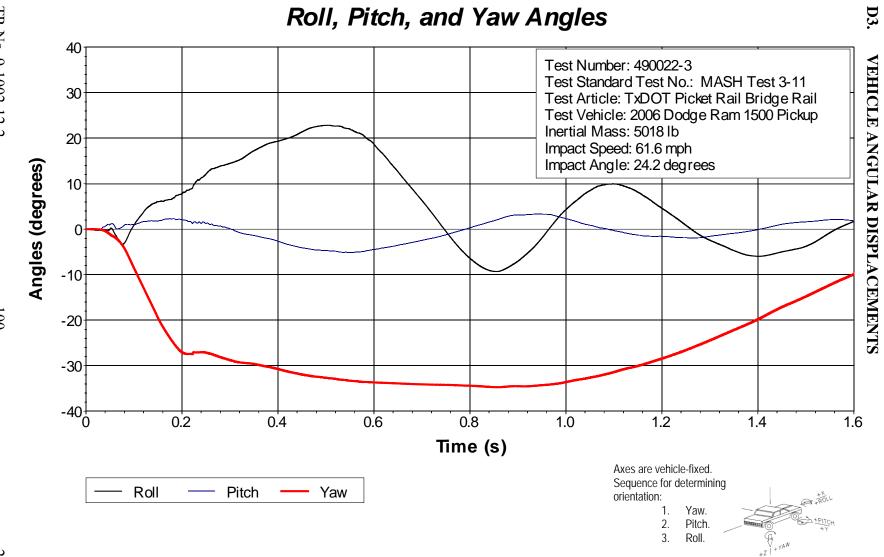


Figure D3. Vehicle Angular Displacements for Test No. 490022-3.

TR No. 9-1002-12-2

100

2012-10-25

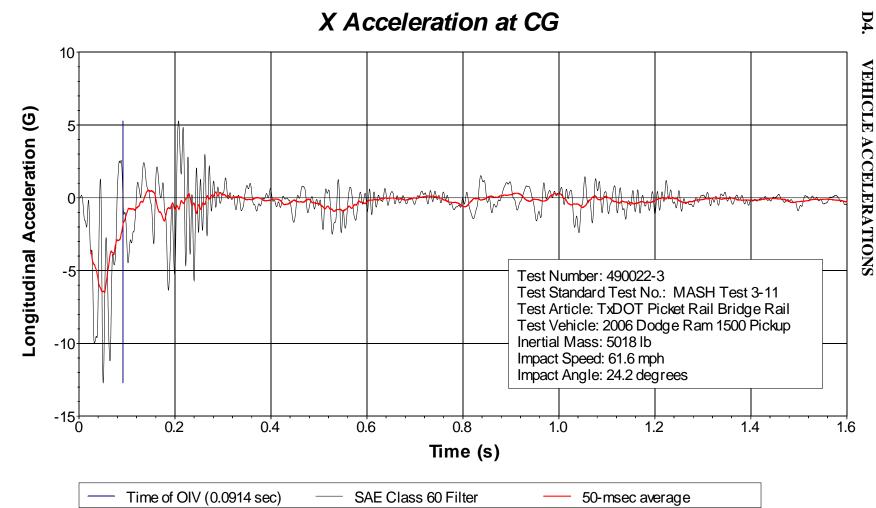
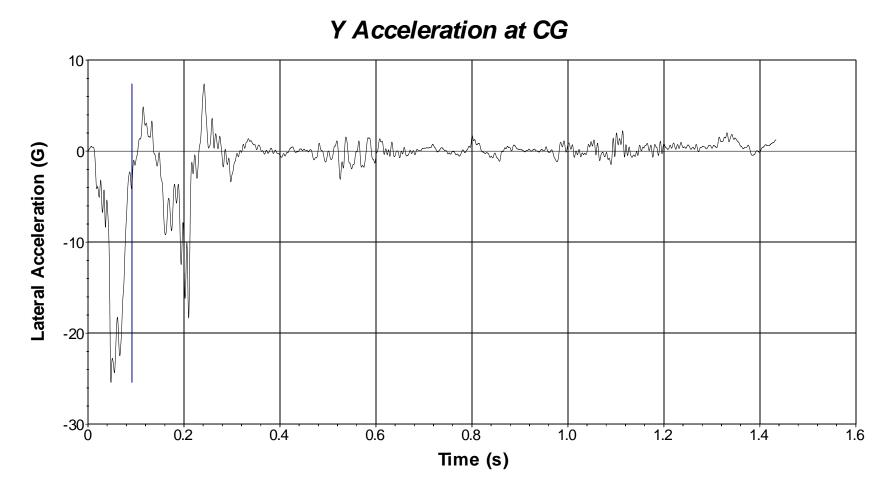


Figure D4. Vehicle Longitudinal Accelerometer Trace for Test No. 490022-3 (Accelerometer Located at Center of Gravity).

101



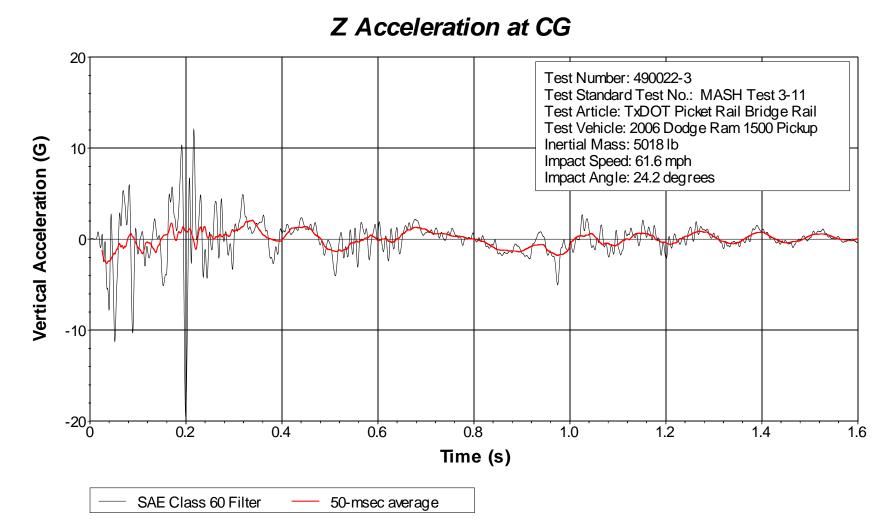


Figure D6. Vehicle Vertical Accelerometer Trace for Test No. 490022-3 (Accelerometer Located at Center of Gravity).

103

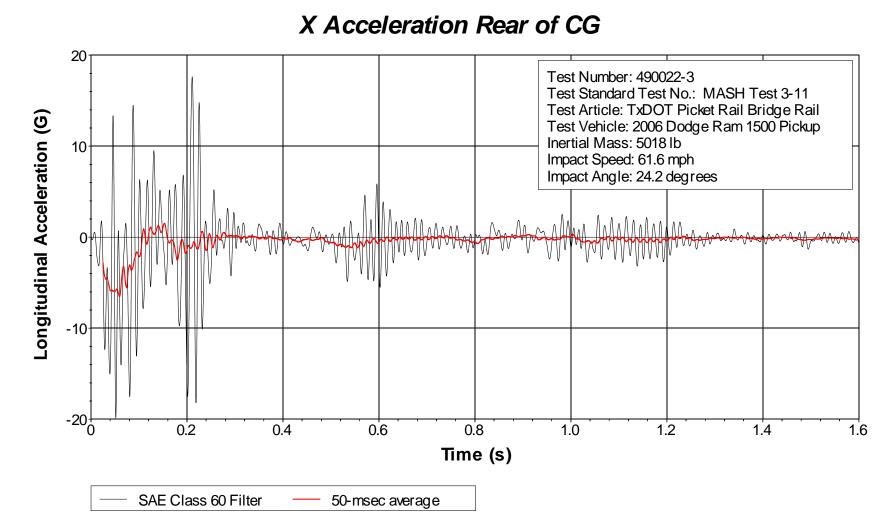


Figure D7. Vehicle Longitudinal Accelerometer Trace for Test No. 490022-3 (Accelerometer Located Rear of Center of Gravity).

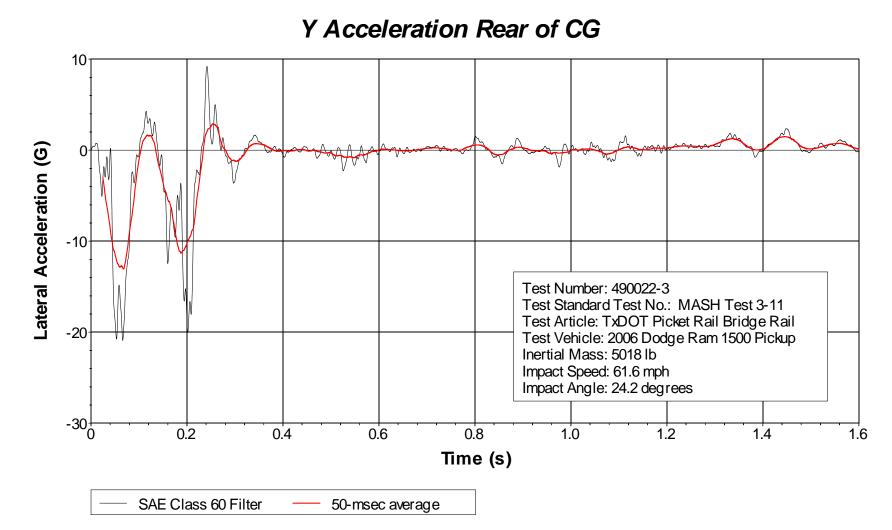


Figure D8. Vehicle Lateral Accelerometer Trace for Test No. 490022-3 (Accelerometer Located Rear of Center of Gravity).

105

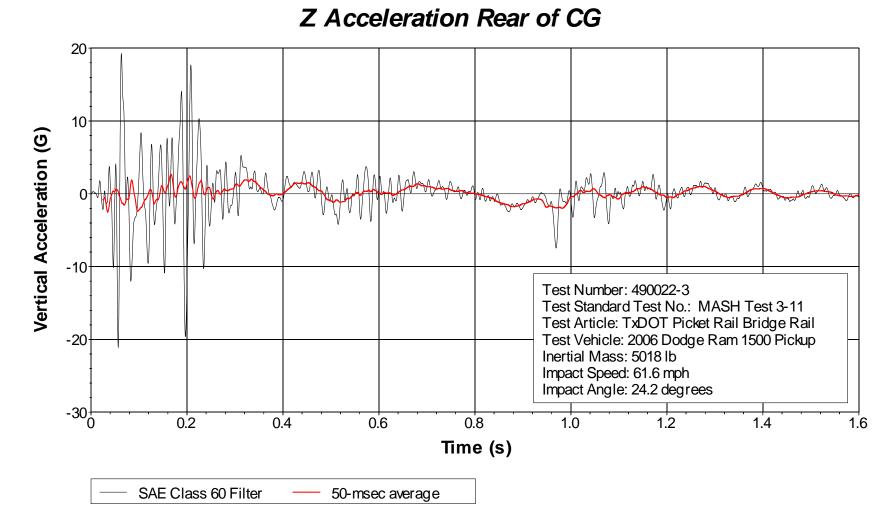


Figure D9. Vehicle Vertical Accelerometer Trace for Test No. 490022-3 (Accelerometer Located Rear of Center of Gravity).