

Texas A&M Transportation Institute 3135 TAMU College Station, TX 77843-3135

979-845-6375 Fax: 979-845-6107 http://tti.tamu.edu/crashtesting

# **TECHNICAL MEMORANDUM**

Contract No.:	T4541-CN		
Test Report No.:	607911-3		
Project Name:	MASH Testing of Portable Concrete Barrier Pinned on Concrete		
-	Pavement		
Sponsor:	Roadside Safety Pooled Fund		
DATE:	May 16, 2017		
то:	Jeffery K. Petterson, P.E.		
	Washington Department of Transportation		
COPY TO:	Epifania Davila, TTI RDO		
	D. L. Bullard, Jr., Head, TTI Roadside Safety & Physical Security Division Rebecca Heck, TTI Roadside Safety & Physical Security Division		
FROM:	Nauman M. Sheikh, P.E., Associate Research Engineer, TTI Roadside Safety & Physical Security Division		
PREPARED BY:	: Wanda L. Menges, Research Specialist, TTI Proving Ground Darrell L. Kuhn, Research Specialist, TTI Proving Ground		
FOR MORE INFO	DRMATION:		

# Name:Nauman M. SheikhPhone:979-845-8955Email:N-Sheikh@tti.tamu.edu

#### **SUMMARY REPORT:**

#### **DISCLAIMER:**

The contents of this report reflect the views of the authors who are solely responsible for the facts and accuracy of the data, findings and conclusions presented herein. The contents do not necessarily reflect the official views or policies of the Roadside Safety Pooled Fund, Texas A&M University System, or Texas A&M Transportation Institute (TTI). This report does not constitute a standard, specification, or regulation. In addition, the above listed company/agencies assume no liability for its contents or use thereof. The names of specific products or manufacturers listed herein do not imply endorsement of those products or manufacturers. The results reported herein apply only to the article being tested. The test was performed according to TTI Proving Ground quality procedures and according to American Association of State Highway and Transportation Officials (AASHTO) *Manual for Assessing Safety Hardware (MASH) (1)*.

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#### **INTRODUCTION**

The purpose of the testing reported herein was to assess the performance of the Pinned Portable Concrete Barrier (PCB) according to the safety-performance evaluation guidelines included in American Association of State Highway and Transportation Officials (AASHTO), *Manual for Assessing Safety Hardware (MASH) (1).* The crash test was performed in accordance with *MASH* Test 3-11, which involves a 2270P vehicle impacting the pinned PCB at a target impact speed and impact angle of 62 mi/h and 25 degrees, respectively.

This technical memo provides details of the pinned PCB, documentation of the crash test performed, the results, and the assessment of the performance of the pinned PCB according to *MASH* Test 3-11 criteria.

#### TEST ARTICLE DESIGN AND CONSTRUCTION

The overall length of the test installation was 100 ft-7 inches. The installation was comprised of eight 12 ft-6 inch long precast concrete F-shape barrier segments connected end-toend. The F-shape segments were 32 inches tall, 24 inches wide at the base, and  $9\frac{1}{2}$  inches wide at the top. The barrier segments were set on the edge of 8-inch thick unreinforced concrete pavement. Two steel anchor pins were used to secure each of the segments to the pavement. The pins passed through slots cast into the segments near each end (no pin in the middle slot) and into  $1\frac{3}{4}$ -inch diameter holes drilled in the concrete pavement. An 18-inch deep  $\times$  12-inch wide excavation was made on the field side of barrier segments 1 through 7. Details of the segments, including steel reinforcement, can be found in Attachment A.

Adjacent precast barrier segments were connected using a pin and loop type connection. The barrier connection was comprised of two sets of three loops that extended from the ends of adjacent barrier segments. A connecting pin was inserted through the loops to establish the connection. When installed, the distance between the end faces of adjacent barrier segments was about 1 inch. Refer to Sheet 5 of 5 in Attachment A for details of the connection.

The anchor pins were  $1\frac{1}{2}$  inches in diameter  $\times 21\frac{1}{4}$  inches long and had blunt ends. A 4-inch square  $\times \frac{1}{2}$  inch thick plate washer with a  $1\frac{5}{8}$ -inch diameter centered hole was positioned at a 95° angle and welded ( $\frac{1}{4}$ -inch fillet) near the top of the anchor pin. Refer to Sheet 5 of 5 in Attachment A for details. Photographs of the installation are shown in Figures 1 through 3.



Figure 1. Pinned PCB before Test No. 607911-3.



Figure 2. Anchor Pin for Test No. 607911-3.



Figure 3. Connection for Test No. 607911-3.

The minimum compressive strength of the concrete for the precast F-shape barrier segments, provided by Waskey Bridges, Inc., was specified as 5000 psi. Cores were taken from the tops of segments 4 and 8 on Test No. 607911-1. The unconfined compressive strength of the concrete cores was 9150 psi and 4930 psi, respectively. The unconfined compressive strength of the concrete deck was 6975 psi and 7390 psi in front of segments 4 and 5, respectively.

All reinforcing steel was grade 60 material. The loops for the connecting pin were fabricated from ASTM A36 steel. The connecting pin between adjacent barrier segments was fabricated from ASTM A449 steel. The washer on each connecting pin met ASTM A572 grade 50 standards. The anchor pins (including the washers) met ASTM A36 specifications. Certifications for the materials used are on file at TTI Proving Ground.

#### TEST DESIGNATION AND ACTUAL TEST CONDITIONS

*MASH* test 3-11 involves a 2270P vehicle weighing 5000 lb  $\pm$ 100 lb, and impacting the barrier at an impact speed of 62 mi/h  $\pm$ 2.5 mi/h and an angle of 25 degrees  $\pm$ 1.5 degrees. The target impact point was 4.3 ft  $\pm$  1ft upstream of the joint between segments 3 and 4. The 2012 Dodge RAM 1500 pickup truck used in the test weighed 5047 lb and the actual impact speed and angle were 63.5 mi/h and 25.7 degrees, respectively. The actual impact point was 4.2 ft upstream of the joint between segments 3 and 4.

#### **TEST VEHICLE**

A 2012 Dodge RAM 1500 pickup truck was used for the crash test. Test inertia weight of the vehicle was 5047 lb, and its gross static weight was 5047 lb. The height to the lower edge

of the vehicle front bumper was 11.0 inches, and the height to the upper edge of the front bumper was 26.5 inches. The height to the center of gravity was 28.0 inches.

#### SOIL AND/OR WEATHER CONDITIONS

The crash test was performed the morning of March 22, 2017. Weather conditions at the time of testing were: Wind speed: 9 mi/h; wind direction: 190 degrees (vehicle was traveling in a northwesterly direction); temperature: 75°F; relative humidity: 70 percent.

#### **BRIEF TEST DESCRIPTION**

The 2012 Dodge RAM 1500 pickup truck, traveling at an impact speed of 63.5 mi/h, impacted the pinned PCB 4.2 ft upstream of the joint between segments 3 and 4 at an impact angle of 25.7 degrees. At 0.016 s after impact, segment 3 at the joint between segments 3 and 4 began to displace toward the field side, at 0.017 s, the left front tire began to climb the traffic face of segment 3. Segment 4 at the joint between segments 3 and 4 began to displace toward the field side at 0.032 s, and the concrete pavement began to crack under the joint between segments 3 and 4 at 0.034 s. At 0.035 s, the vehicle began to redirect and segment 4 at the joint between segments 4 and 5 began to rotate toward the traffic side. The field side toe on the upstream end of segment 3 began to crack at 0.058 s, and the right side tires were airborne at 0.099 s and 0.163 s, respectively. At 0.208 s, the vehicle was traveling parallel with the barrier, and at 0.263 s, the left rear exterior bed and rear bumper contacted the barrier. The vehicle lost contact with the barrier at 0.550 s, traveling at an exit speed and angle of 54.2 mi/h and 2.7 degrees. Brakes on the vehicle were not applied. The vehicle subsequently rolled 471 degrees counterclockwise, then 111 degrees clockwise, and came to rest upright 167 ft downstream of impact and 27 ft toward traffic lanes. Figure 4 show the barrier and test vehicle after Test No. 607911-3.



Figure 4. Pinned PCB and Test Vehicle after Test No. 607911-3.

#### TEST ARTICLE/COMPONENT DAMAGE

Figure 5 shows damage to the barrier. The upstream field side corner of segment 2, the upstream field side and downstream traffic side corner of segment 3, the downstream traffic side corner of segment 4, and the upstream field side corner of segment 6 were damaged. The anchor pins broke through the concrete pavement at segments 2 through 5, and the pavement was also cracked downstream of the upstream field side pin of segment 6.



Figure 5. Pinned PCB after Test No. 607911-3.

#### **TEST VEHICLE DAMAGE**

Figure 6 shows the damage sustained by the vehicle. The front bumper, hood, radiator and support, left front fender, left front tire and rim, left front door and window glass, left rear door, left rear exterior bed, left rear tire and rim, rear bumper, tailgate, rear springs, right rear exterior bed, right rear tire and rim, right front fender, right front tire and rim, right front ball joint, left frame rail, left upper and lower A-arms, and roof were damaged. Maximum exterior crush to the vehicle was 12.0 inches in the front plane at the left front corner at bumper height. Occupant compartment deformation was 2.0 inches in the kick panel/toe panel area.



Figure 6. Vehicle after Test No. 607911-3.

#### **OCCUPANT RISK VALUES**

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk. In the longitudinal direction, the occupant impact velocity (OIV) was 13.8 ft/s at 0.110 s, the highest 0.010-s occupant ridedown acceleration was 5.6 g from 0.132 to 0.142 s, and the maximum 0.050-s average acceleration was -6.69 g between 0.014 and 0.064 s. In the lateral direction, the OIV was 19.0 ft/s at 0.110 s, the highest 0.010-s occupant ridedown acceleration was 16.3 g from 0.253 to 0.263 s, and the maximum 0.050-s average was 10.5 g between 0.035 and 0.085 s. Theoretical Head Impact Velocity (THIV) was 25.6 km/h or 7.1 m/s at 0.106 s; Post-Impact Head Decelerations (PHD) was 16.5 g between 0.253 and 0.263 s; and Acceleration Severity Index (ASI) was 1.38 between 0.056 and 0.106 s. These data and other pertinent information from the test are summarized in Figure 7.

#### SUMMARY AND CONCLUSIONS

As shown in Table 1, the pinned PCB did not perform acceptably for *MASH* Test 3-11 due to the rollover event.

#### REFERENCES

1. AASHTO. *Manual for Assessing Roadside Safety Hardware, Second Edition.* 2016, American Association of State Highway and Transportation Officials: Washington, D.C.



Test Standard Test No	MASH Test 3-11	Angle
TTI Test No	607911-3	Location/Orientat
Date	2017-03-22	
Test Article		Impact Severity
Туре	Pinned Portable Concrete Barrier	Exit Conditions
Name	Pinned PCB	Speed
Installation Length	100 ft-7 inches	Angle
Material or Key Elements	Eight 12 ft-6 inch long precast concrete F-	Occupant Risk Va
-	shape barrier segments, 32 inches tall,	Longitudinal OIV.
	24 inches wide at base, and 9½ inches	Lateral OIV
	wide at top, pinned to concrete pavement	Longitudinal Ride
Soil Type and Condition	Concrete deck, damp	Lateral Ridedown
Test Vehicle		THIV
Type/Designation	2270P	PHD
Make and Model	2012 Dodge RAM 1500	ASI
Curb	4850 lb	Max. 0.050-s Avera
Test Inertial	5047 lb	Longitudinal
Dummy	No dummy	Lateral
Gross Static	5047 lb	Vertical

0 -	
Location/Orientation	4.2 ft upstrean
	of joint 3-4
npact Severity	128 kip-ft
xit Conditions	•
Speed	54.2 mi/h
Angle	2.7 degrees
ccupant Risk Values	0
Longitudinal OIV	13.8 ft/s
Lateral OIV	19.0 ft/s
Longitudinal Ridedown	5.6 g
Lateral Ridedown	16.3 g
THIV	
PHD	16.5 g
ASI	1.38
lax. 0.050-s Average	
Longitudinal	−6.9 q
Lateral	10.5 g
Vertical	−5.6 g
	3

Vehicle Stability	
Maximum Yaw Angle	. 195 degrees
Maximum Pitch Angle	. 22 degrees
Maximum Roll Angle	. 472 degrees
Vehicle Snagging	. No
Vehicle Pocketing	. No
Test Article Deflections	
Dynamic	. 31.4 inches
Permanent	. 31.0 inches
Working Width	. 59.3 inches
Vehicle Damage	
VDS	. Rollover
CDC	. Rollover
Max. Exterior Deformation	. 12.0 inches
OCDI	LF0000000
Max. Occupant Compartment	
Deformation	. 2.0 inches

Figure 7. Summary of Results for MASH Test 3-11 on the Pinned PCB.

### Table 1. Performance Evaluation Summary for MASH Test 3-11 on the Pinned PCB.

Tes	t Agency: Texas A&M Transportation Institute	Test No.: 607911-3 Te	est Date: 2017-03-22
	MASH Test 3-11 Evaluation Criteria	Test Results	Assessment
Structural Adequacy			
Α.	Test article should contain and redirect the vehicle or	The pinned PCB contained and redirected the	
	bring the vehicle to a controlled stop; the vehicle	2270P vehicle. The vehicle did not penetrate,	
	should not penetrate, underride, or override the	underride, or override the installation. Maximum	Pass
	installation although controlled lateral deflection of	dynamic deflection during the test was	
	the test article is acceptable	31.4 inches.	
<u>Occ</u>	upant Risk		
<i>D</i> .	Detached elements, fragments, or other debris from	The concrete pavement broke around several	
	the test article should not penetrate or show potential	anchor pins in the impact area, however, there	
	for penetrating the occupant compartment, or present	was not penetration or potential for penetration	Pass
	an undue hazard to other traffic, pedestrians, or	of the occupant compartment.	
	personnel in a work zone.		
	Deformations of, or intrusions into, the occupant	Occupant compartment deformation was	
	compartment should not exceed limits set forth in	2.0 inches in the kick panel/toe panel area.	Pass
	Section 5.3 and Appendix E of MASH.		
<i>F</i> .	The vehicle should remain upright during and after	The 2270P vehicle rolled 472 degrees counter-	
	collision. The maximum roll and pitch angles are not	clockwise and then 111 degrees clockwise and	Fail
	to exceed 75 degrees.	came to rest upright.	
Н.	Longitudinal and lateral occupant impact velocities	Longitudinal OIV was 13.8 ft/s, and lateral OIV	
	should fall below the preferred value of 30 ft/s, or at	was 19.0 ft/s.	Pass
	<i>least below the maximum allowable value of 40 ft/s.</i>		
<i>I</i> .	Longitudinal and lateral occupant ridedown	Maximum longitudinal occupant ridedown	
	accelerations should fall below the preferred value of	acceleration was 5.6 g, and maximum lateral	Pass
	15.0 g, or at least below the maximum allowable value	occupant ridedown acceleration was 16.3 g.	1 455
	of 20.49 g.		

## ATTACHMENT A: TEST ARTICLE DETAILS





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