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MASH TEST 3-10 OF GUARDRAIL SYSTEM ON 1H:1V SLOPE

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The purpose of this research 1H:1V slope. The structural capacit evaluated with respect to <i>MASH</i> TL criteria, and based on the test result. The 1100C vehicle impacted impact speed of 63.9 mi/h and an in guardrail on 1H:1V slope did not pe	was to develop and evaluate a guardi y and the occupant risk factors of such -3 criteria. A W-beam guardrail syste more stiffness was desired. If the guardrail on 1H:1V slope 31.5 in pact angle of 25.2 degrees. Due to ro erform acceptably for <i>MASH</i> Test 3-10	cail system to be placed with a h proposed guardrail system were om was tested under <i>MASH</i> TL 3-10 nches upstream of post 14 at an ollover of the 1100C vehicle, the 0 for longitudinal barriers.

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gal	gallons	3.785	liters	L	
ft ³	cubic feet	0.028	cubic meters	m ³	
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mm	millimeters	0.039	inches	in	
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m	meters	1.09	vards	vd	
km	kilometers	0.621	miles	mi	
		AREA			
mm ²	square millimeters	0.0016	square inches	in ²	
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N	newtons	0.225	poundforce	lbf	
kPa	kilopascals	0.145	poundforce per square inch	lb/in ²	

*SI is the symbol for the International System of Units

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CHAPTER 1. INTRODUCTION

1.1. PROBLEM STATEMENT

The American Association of State Highway and Transportation Officials (AASHTO) Roadside Design Guide recommends that guardrail be installed with the back edges of the guardrail post being 2 ft from a slope break (1). In many areas with tight environmental controls, this width is difficult to provide. As a result, designers often have to make a trade-off between reduced shoulder width and a less than optimal guardrail placement. The Washington State Department of Transportation (WSDOT) Design Manual provides for the placement of the guardrail post closer to or on slopes as steep as 1H:1V slope (2).





Notes:

- Use Cases 1 and 3 when there is a 2.5-foot or greater shoulder widening from face of guardrail to the breakpoint.
- Use Case 2 when there is a 4.0-foot or greater shoulder widening from the face of the guardrail to the breakpoint.
- Use Cases 4, 5, and 6 when there is less than a 2.5-foot shoulder widening from face of guardrail to the breakpoint.

Figure 1.1. Allowable Post on Slope Installation Cases from WSDOT Design Manual; Beam Guardrail Post Installation — Exhibit 1610-11 (2)

1.2. BACKGROUND

Texas A&M Transportation Institute (TTI) researchers conducted in March 2018 a fullscale crash tests of a 31-inch high guardrail system placed on 2H:1V slope in accordance with AASHTO *MASH* (3, 4). The posts were placed 1 ft from the slope break such that the face of the guardrail was aligned with the slope break, as shown in Figure 1.2.



Figure 1.2. Cross Section of the Guardrail on Slope System Tested by TTI.

The guardrail on slope system was comprised of a 106.25-ft length of need section and a 37.5-ft long ET PLUS terminal on each end. The 12-gauge W-beam was mounted on W6×8.5 steel posts. The guardrail height was 31 inches above the flat terrain. A 2H:1V sloped ditch was excavated behind the rail to represent the slope terrain. An overview of this system installation is shown in Figure 1.3. Standard size 6-inch × 8-inch × 14-inch wood blockouts were used in the length of needed section.



Figure 1.3. Guardrail on Slope System as Tested by TTI.

The researchers conducted two AASHTO Manual for Assessing Safety Hardware (MASH) crash tests (3, 4).

MASH Test 3-11, which involves a 2000 kg (4409-lb) pickup truck impacting the critical impact point (CIP) of the length of need section at a nominal impact speed of 100 km/h (62 mi/h) and a nominal impact angle of 25 degrees.

MASH Test 3-10, which involves an 1100 kg (2420-lb) passenger car impacting the CIP of the length of need section at a nominal impact speed of 100 km/h (62 mi/h) and nominal impact angle of 25 degrees.

The test vehicle was successfully redirected by the guardrail system in each test. The test evaluation metrics were all within the limit of *MASH* test evaluation metrics. Hence, both tests passed *MASH* test evaluation criteria. Sequential images of both tests are shown in Figure 1.4.







Figure 1.4. Sequential Photos of MASH 3-11 and MASH 3-10.

⁽b) Test No. 405160-20-2

1.3. OBJECTIVE

The objective of this study is to crash test a guardrail system with the face of the rail aligned with the break point of a 1H:1V slope. The system is to be tested and evaluated per MASH TL-3 impact conditions and criteria.

1.4. BENEFITS

A guardrail system in which the face of the rail is aligned with the slope break will provide significant savings in terms of reduced shoulder width in mountainous areas as well as other locations that have very restrictive space.

CHAPTER 2. MASH TEST 3-10 (CRASH TEST 609301-01-1)

2.1. TEST ARTICLE DESIGN AND CONSTRUCTION

The test installation consisted of a flexible W-beam guardrail system, with the top edge of the rail 31 inches above the roadway. The length of need portion (W-beam guardrail, supported by 9-ft long, W6×8.5 posts on 75-inch spacings, and offset from the posts with routered timber blockouts, with the rail splices midspan between the posts) was 162.5 ft long. It was anchored on each end with a TxDOT DAT terminal, for a total installation length of 181.25 ft. The ground sloped down and toward the field side at 45 degrees (1:1 slope) in the impact area, beginning approximately at the traffic side face of the guardrail, and extending for 8 ft to the field side and 8 ft deep. Figure 2.1 provides photographs of the installation. Appendix A.1 and A.2 provide further details of the guardrail on 1H:1V slope.



Figure 2.1. Guardrail on 1H:1V Slope prior to Test No. 609301-01-1.

In accordance with Appendix B of *MASH*, soil strength was measured the day of the crash test. During installation of the guardrail on 1H:1V slope for full-scale crash testing, two W6×16 posts were installed in the immediate vicinity of the guardrail on 1H:1V slope utilizing the same fill materials and installation procedures used in the test installation and the standard dynamic test. The minimum post loads required for deflections at 5 inches, 10 inches, and 15 inches, measured at a height of 25 inches, are 3940 lb, 5500 lb, and 6540 lb, respectively (90% of static load for the initial standard installation). On the day of the test, March 9, 2018, loads on the post at deflections of 5 inches, 10 inches, and 15 inches were 8030 lbf, 8030 lbf, and 7272 lbf, respectively. Table A.1 in Appendix A.3 shows the strength of the backfill material in which the guardrail on 1H:1V slope was installed met minimum *MASH* requirements.

2.2. TEST DESIGNATION AND ACTUAL TEST CONDITIONS

MASH Test 3-10 involves an 1100C vehicle weighing 2420 lb \pm 55 lb impacting the CIP of the guardrail at an impact speed of 62 mi/h \pm 2.5 mi/h and an angle of 25 degrees \pm 1.5 degrees. The CIP for *MASH* Test 3-10 on the guardrail on 1H:1V slope was 31 inches \pm 1 ft upstream of post 14.

The 2009 Kia Rio used in the test weighed 2437 lb, and the actual impact speed and angle were 63.9 mi/h and 25.2 degrees, respectively. The actual impact point was 31.5 inches upstream of post 14. Minimum target impact severity (IS) was 51 kip-ft, and actual IS was 60 kip-ft.

2.3. TEST VEHICLE

Figure 2.2 shows the 2009 Kia Rio used for the crash test. The vehicle's test inertia weight was 2437 lb, and its gross static weight was 2602 lb. The height to the lower edge of the vehicle bumper was 7.75 inches, and height to the upper edge of the bumper was 21.5 inches. The vehicle was directed into the installation using the cable reverse tow and guidance system, and was released to be freewheeling and unrestrained just prior to impact. Table A.2 in Appendix A.4 provides measurements of the vehicle.



Figure 2.2. Guardrail on 1H:1V Slope/Test Vehicle Geometrics for Test No. 609301-01-1.

2.4. WEATHER CONDITIONS

MASH Test 3-10 on the guardrail on 1H:1V slope was performed on the morning of March 9, 2018. Weather conditions at the time of testing were as follows: wind speed: 13 mi/h; wind direction: 163 degrees (vehicle was traveling at a heading of 325 degrees); temperature: 68°F; relative humidity: 63 percent.

2.5. TEST DESCRIPTION

Table 2.1 lists times and significant events that occurred during Test No. 609301-01-1. Figures A.1 and A.2 in Appendix A.4 provides sequential photos from the test.

	0
TIME (s)	EVENTS
0.000	Vehicle impacts guardrail
0.010	Post 14 begins to move
0.016	Post 13 begins to move
0.025	Post 15 begins to move
0.044	Vehicle begins to redirect
0.056	Post 16 begins to move
0.087	Rail element begins to tear at joint between posts 14 and 15
0.096	Rail element disconnects from post 15
0.099	Rail element completely disconnected between posts 14 and 15
0.106	Vehicle loses contact with the guardrail while traveling at 57.4 mi/h and 20.8°
0.156	Vehicle hits post 16, to right of middle of front bumper
0.207	Vehicle begins to roll into ditch
0.254	Vehicle hits post 17, right of middle of front bumper
0.689	Vehicle lands on side in ditch (continues rolling)
1.555	Vehicle in ditch facing upstream, slightly to the left (from original direction)

Table 2.1. Events during Test No. 609301-01-1.

For longitudinal barriers, it is desirable that the vehicle redirects and exits the barrier within the exit box criteria (not less than 32.8 ft downstream from impact for cars and pickups). The rail element ruptured at the splice between posts 14 and 15, and the vehicle penetrated the guardrail. After loss of contact with the guardrail, the vehicle came to rest 40 ft downstream of the impact and 10 ft toward the field side.

2.6. TEST ARTICLE/COMPONENT DAMAGE

Figure 2.3 shows the damage to the guardrail on 1H:1V slope. The soil around post 1 and 12 was disturbed. Post 13 deflected 0.4 inch toward the field side, and post 14 deflected 4.0 inches toward the field side. The rail element tore at the splice between posts 14 and 15. The rail element released from posts 15-18, and the blockouts released from the posts 15 and 16. Posts 15-17 were leaning downstream at 35 degrees from vertical, and post 18 was leaning downstream at 68 degrees from vertical and deflected toward the field side 1.0 inch. No movement was noted at other posts.



Figure 2.3. Guardrail on 1H:1V Slope after Test No. 609301-01-1.

2.7. TEST VEHICLE DAMAGE

Due to vehicle rollover, the vehicle sustained damage to all exterior components as shown in Figure 2.4. Figure 2.5 shows the interior of the vehicle.



Figure 2.4. Test Vehicle after Test No. 609301-01-1.



Figure 2.5. Interior of Test Vehicle after Test No. 609301-01-1.

2.8. OCCUPANT RISK FACTORS

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk and are shown in Table 2.2. Figure A.3 in Appendix A.5 shows the vehicle angular displacements, and Figures A.4 through A.6 in Appendix A.6 show accelerations versus time traces.

Occupant Risk Factor	Value	Time
Occupant Impact Velocity (OIV)		
Longitudinal	14.4 ft/s	at 0,1286 s on left side of interior
Lateral	13.8 ft/s	at 0.1280's on left side of interior
Occupant Ridedown Accelerations		
Longitudinal	12.3 g	0.1785 - 0.1885 s
Lateral	12.0 g	0.8958 - 0.9058 s
Theoretical Head Impact Velocity (THIV)	21.6 km/h 6.0 m/s	at 0.1230 s on left side of interior
Post Head Deceleration (PHD)	15.1 g	0.9028 - 0.9128 s
Acceleration Severity Index (ASI)	1.3	0.8995 - 0.9495 s
Maximum 50-ms Moving Average		
Longitudinal	-7.7 g	0.8639 - 0.9139 s
Lateral	-9.3 g	0.8740 - 0.9240 s
Vertical	7.7 g	0.8305 - 0.8805 s
Maximum Roll, Pitch, and Yaw Angles		
Roll	156°	0.9062 s
Pitch	83°	1.2362 s
Yaw	138°	2.2724 s

Table 2.2. Occupant Risk Factors for Test No. 609301-01-1.

CHAPTER 3. SUMMARY AND CONCLUSIONS

The crash test reported herein was performed in accordance with *MASH* Test 3-10, which involves an 1100C vehicle impacting the guardrail at a target impact speed and impact angle of 62 mi/h and 25 degrees, respectively. Figure 2.6 summarizes the data and other pertinent information from the test. An assessment of the test based on the applicable safety evaluation criteria for *MASH* Test 3-10 for longitudinal barriers is provided in Table 2.3.

The 1100C vehicle impacted the guardrail on 1H:1V slope 31.5 inches upstream of post 14 at an impact speed of 63.9 mi/h and an impact angle of 25.2 degrees. Due to rollover of the 1100C vehicle, the guardrail on 1H:1V slope did not perform acceptably for *MASH* Test 3-10 for longitudinal barriers.

A finite element analysis was performed to determine feasible enhancements to be made for the guardrail to perform acceptably. The analysis and results are reported in a separate report (5).



General Information		Impact Conditions	Post-Impact Trajectory	
Test Agency	Texas A&M Transportation Institute (TTI)	Speed 63.9 mi/h	Stopping Distance	40 ft downstream
Test Standard Test No	MASH Test 3-10	Angle		10 ft twd field side
TTI Test No	609301-01-1	Location/Orientation	Vehicle Stability	
Test Date	2018-03-09	upstream of post 14	Maximum Yaw Angle	138°
Test Article		Impact Severity 60 kip-ft	Maximum Pitch Angle	83°
Туре	Longitudinal Barrier – Guardrail	Exit Conditions	Maximum Roll Angle	156°
Name	Guardrail on 1H:1V Slope	Speed 57.4 mi/h	Vehicle Snagging	Yes
Installation Length	181 ft 3 inches	Angle 20.8°	Vehicle Pocketing	No
Material or Key Elements	31-inch W-Beam Guardrail on 9 ft W6x8.5	Occupant Risk Values	Test Article Deflections	
-	steel posts with wood blockouts spaced at	Longitudinal OIV 14.4 ft/s	Dynamic	Rail Ruptured
	75 inches on 1H:1V slope	Lateral OIV 13.8 ft/s	Permanent	Rail Ruptured
Soil Type and Condition	Embedded in AASHTO M147-65(2004),	Longitudinal Ridedown 12.3 g	Working Width	15 ft
	grading B Soil (crushed limestone)	Lateral Ridedown 12.0 g	Height of Working Width	NA
Test Vehicle		THIV	Vehicle Damage	
Type/Designation	1100C	PHD15.1 g	VDS	Rollover
Make and Model	2009 Kia Rio	ASI 1.3	CDC	Rollover
Curb	2338 lb	Max. 0.050-s Average	Max. Exterior Deformation	NA
Test Inertial	2437 lb	Longitudinal7.7 g	OCDI	NA
Dummy	165 lb	Lateral9.3 g	Max. Occupant Compartment	
Gross Static	2602 lb	Vertical7.7 g	Deformation	NA
		Ŭ		

Figure 2.1. Summary of Results for MASH Test 3-10 on Guardrail on 1H:1V Slope.

Table 2.1. Performance Evaluation Summary for MASH Test 3-10 on Guardrail on 1H:1V Slope.

Tes	t Agency: Texas A&M Transportation Institute	Test No.: 609301-01-1	Fest Date: 2018-03-09
	MASH Test 3-10 Evaluation Criteria	Test Results	Assessment
<u>Str</u> A.	nctural Adequacy Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.	The guardrail on 1H:1V slope did not contain or redirect the 1100C vehicle. The 1100C vehicle penetrated guardrail.	Fail
<u>Ос</u> D.	 <u>cupant Risk</u> Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone. Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH. 	Some of the wood blockouts separated from the rail element and posts, and the rail element ruptured. These elements did not penetrate or show potential to penetrate the occupant compartment, or present hazard to others. Due to vehicle rollover, the occupant compartment deformation could not be adequately measured.	Fail
F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	Vehicle roll was 156 degrees, and pitch was 83 degrees.	Fail
Н.	Occupant impact velocities (OIV) should satisfy the following limits: Preferred value of 30 ft/s, or maximum allowable value of 40 ft/s.	Longitudinal OIV was 14.4 ft/s, and lateral OIV was 13.8 ft/s.	Pass
Ι.	The occupant ridedown accelerations should satisfy the following limits: Preferred value of 15.0 g, or maximum allowable value of 20.49 g.	Maximum longitudinal 10-ms occupant ridedown acceleration was 12.3 g, and maximum lateral occupant ridedown acceleration was 12.0 g.	Pass

.

REFERENCES

- 1. AASHTO Roadside Design Guide. American Association of State Highway and Transportation Officials, Washington, DC.
- 2. Washington State Department of Transportation (WSDOT) Design Manual, <u>https://wsdot.wa.gov/Publications/Manuals/M22-01.htm</u>, last accessed 2020-09-27.
- 3. AASHTO *Manual for Assessing Safety Hardware; Second Edition*. American Association of State Highway and Transportation Officials, Washington, DC, 2016.
- 4. Akram Y. Abu-Odeh, Kelly Ha, Ivan Liu, and Wanda L. Menges. *MASH TL-3 Testing and Evaluation of the W-Beam Guardrail on Slope*, Test Report No. 405160-20, Texas A&M Transportation Institute, College Station, Tx, March 2013.
- 5. Sun Hee Park and Akram Y Abu-Odeh. *Finite Element Analysis of Placement of Guardrail System on 1H:1V Slope*. Test Report No. 609301-01-FEA, Texas A&M Transportation Institute, College Station, Tx, October 2020.

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APPENDIX A.









SPECIFICATIONS

The geometry and material specifications for this oval shoulder button-headed bolt and hex nut are found in AASHTO M 180. The bolt shall have 5/8-11 [M16x2] threads as defined in ANSI B1.1 [ANSI B1.13M] for Class 2A [6g] tolerances. Bolt material shall conform to ASTM A307 Grade A [ASTM F 568M Class 4.6], with a tensile strength of 60 ksi [400 MPa] and yield strength of 36 ksi [240 MPa]. Material for corrosion-resistant bolts shall conform to ASTM A325 Type 3 [ASTM F 568M Class 8.8.3], with tensile strength of 120 ksi [830 MPa] and yield strength of 92 ksi [660 MPa]. This bolt material has corrosion resistance comparable to ASTM A588 steels. Metric zinc-coated bolt heads shall be marked as specified in ASTM F 568 Section 9 with the symbol "4.6."

Nuts shall have ANSI B1.1 Class 2B [ANSI B1.13M Class 6h] 5/8-11 [M16x2] threads. The geometry of the nuts, with the exception of the recess shown in the drawing, shall conform to ANSI B18.2.2 [ANSI B18.2.4.1M Style 1] for zinc-coated hex nuts (shown in drawing) and ANSI B18.2.2 [ANSI B18.2.4.6M] for heavy hex corrosion-resistant nuts (not shown in drawing). Material for zinc-coated nuts shall conform to the requirements of AASHTO M 291 (ASTM A 563) Grade A [AASHTO M 291M (ASTM A 563M) Class 5], and material for corrosion-resistant nuts shall conform to the requirements of AASHTO M 291 (ASTM A 563) Grade C3 [AASHTO M 291M (ASTM A 563M) Class 5].

When zinc-coated bolts and nuts are required, the coating shall conform to either AASHTO M 232 (ASTM A 153/A 153M) for Class C or AASHTO M 298 (ASTM B 695) for Class 50. Zinc-coated nuts shall be tapped over-size as specified in AASHTO M 291 (ASTM A 563) [AASHTO M 291M (ASTM A 563M)], except that a diametrical allowance of 0.020 inch [0.510 mm] shall be used instead of 0.016 inches [0.420 mm].

	Stress Area of	Min. Bolt
Designator	Threaded Bolt Shank	Tensile Strength
100	$(in^{2} [mm^{2}])$	(kips [kN])
FBB01-05	0.226 [157.0]	13.6 [62.8]

Dimensional tolerances not shown or implied are intended to be those consistent with the proper functioning of the part, including its appearance and accepted manufacturing practices.

INTENDED USE

These bolts and nuts are used in numerous guardrail and median barrier designs.

GUARDRAIL BOLT AND RECESSED NUT

FBB01-05

SHEET NO.	DATE
2 of 2	6/30/2005



SPECIFICATIONS

Corrugated sheet steel beams shall conform to the current requirements of AASHTO M180. The section shall be manufactured from sheets with a nominal width of 483 mm. Guardrail RWM04a shall conform to AASHTO M180 Class A and RWM04b shall conform to Class B. Corrosion protection may be either Type II (zinc-coated) or Type IV (corrosion resistant steel). Corrosion resistant steel should conform to ASTM A606 for Type IV material and shall not be zinc-coated, painted or otherwise treated. Inertial properties are calculated for the whole cross-section without a reduction for the splice bolt holes.

Designator	Area (10^3 mm^2)	I _x (10 ⁶ mm ⁴)	I _y (10 ⁶ mm⁴)	S_x (10 ³ mm ³)	S _y (10 ³ mm ³)	
RWM04a-b	1.3	1.0		23		

Dimensional tolerances not shown or implied are intended to be those consistent with the proper functioning of the part, including its appearance and accepted manufacturing practices.

INTENDED USE

This corrugated sheet steel beam is used as a rail element in transition systems STB02 and STB03 or when a reduced post spacing is desired in the SGR02, SGR04a-b, SGM02, and SGM04a-b.

4-SPACE W-BEAM GUARDRAIL

RWM04a-b			
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04-01-95			





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A.2.

MATERIAL CERTIFICATION DOCUMENTS

A.3. SOIL PROPERTIES



Table A.1. Test Day Static Soil Strength Documentation for Test No. 609301-01-1.

A.4. VEHICLE PROPERTIES

Table A.2. Vehicle Properties for Test No. 609301-01-1.								
Date: 2018-03-09 Test No.:	609301-01-1	VIN No.:	KNAD	E2236964	61040			
Year:2009 Make:	KIA	Model:	18	RIO				
Tire Inflation Pressure: <u>32 PSI</u>	Odometer: <u>1464</u> 5	57	Tire Size:	185/65R1	4			
Describe any damage to the vehicle pr	ior to test: None							
Denotes accelerometer location. NOTES: None								
Engine Type: <u>4 CYL</u> Engine CID: <u>1.6 L</u> Transmission Type:								
		R						
Dummy Data:Type:50th percentile malMass:165 lbSeat Position:Driver Side		H			ĸ			
Geometry: inches ▲ 66.38 □ 33.00	× 12.25	D	_c	>	15 25			
B 51 50 G	1 25.25	Г <u> </u>	22 50	v —	20.50			
с 165.75 н 35.80	м 57.75	R	15.50	w —	35.80			
D 34.00 I 7.75	N 57.70	s	8.25	x	107.00			
Е 98.75 J 21.50	o 28.25	T	66.20					
Wheel Center Ht Front 11.00	Wheel Center H	It Rear	11.00	W-H	0.00			
RANGE LIMIT: A = 65 ±3 inches; C = 168 ±8 inches; E = M+N/2 = 56	= 98 ±5 inches; F = 35 ±4 inches; G ±2 inches; W-H < 2 inches or use MA	= 39 ±4 inches; O = ⁻ SH Paragraph A4.3	FOP OF RADIATOF 2	R SUPPORT (24 ±4 i	nchos) ;			
GVWR Ratings: Mass: II	o Curb	Test	Inertial	Gross	s Static			
Front 1718 M _{front}	1552	-	1554	2	1639			
Back 1874 M _{rear}	786		883		963			
Total <u>3638</u> M _{Total}	2338		2437		2602			
Macc Distribution:	Allowable TIM =	= 2420 lb ±55 lb Alle	owable GSM = 2585	5 lb ± 55 lb				
lb LF:76	<u>1</u> RF: <u>793</u>	LR:	438	RR:	445			

A.4. SEQUENTIAL PHOTOGRAPHS















Figure A.1. Sequential Photographs for Test No. 609301-01-1 (Overhead and Frontal Views).



















Figure A.1. Sequential Photographs for Test No. 609301-01-1 (Overhead and Frontal Views) (Continued).



0.000 s



0.100 s



0.200 s



0.300 s

Figure A.2. Sequential Photographs for Test No. 609301-01-1 (Rear View).



0.400 s











0.700 s



A.5.

VEHICLE ANGULAR DISPLACEMENTS

Figure A.3. Vehicle Angular Displacements for Test No. 609301-01-1.

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A.6.

VEHICLE ACCELERATIONS





Figure A.5. Vehicle Lateral Accelerometer Trace for Test No. 609301-01-1 (Accelerometer Located at Center of Gravity).

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Figure A.6. Vehicle Vertical Accelerometer Trace for Test No. 609301-01-1 (Accelerometer Located at Center of Gravity).