

Test Report No. 617231-01-1&2



MASH TL-3 EVALUATION OF LONG-SPAN W-BEAM GUARDRAIL IN FRONT OF FALL-PROTECTION FENCE

Sponsored by Washington State Department of Transportation

TEXAS A&M TRANSPORTATION INSTITUTE PROVING GROUND

Roadside Safety & Physical Security Texas A&M University System RELLIS Campus Building 7091 1254 Avenue A Bryan, TX 77807



		Technical Report Documentation Page			
1. Report No.	2. Government Accession No.	3. Recipient's Catalog No.			
4. Title and Subtitle		5. Report Date			
MASH TL-3 Evaluation of Long-Spa	an W-Beam Guardrail in Front of	August 2023			
Fall-Protection Fence		6. Performing Organization Code			
7. Author(s)		8. Performing Organization Report No.			
Nauman M. Sheikh, Sun Hee Pa	rk, William J. L. Schroeder, and	Report 617231-01-1&2			
Darrell L. Kuhn					
9. Performing Organization Name and Address		10. Work Unit No. (TRAIS)			
Texas A&M Transportation Instit	ute Proving Ground				
3135 TAMU		11. Contract or Grant No.			
College Station, Texas 77843-31	Project T 4541				
12. Sponsoring Agency Name and Address		13. Type of Report and Period Covered			
Washington State Department of	Technical Report:				
Research Office MS 47372 Transpo	February 2023 - August 2023				
Olympia, WA 98504-7372	· · · · · · · · · · · · · · · · · · ·				
		14. Sponsoring Agency Code			
15. Supplementary Notes	15. Supplementary Notes				
Name of Contacting Representation	tive [.] Tim Moeckel				

16. Abstract

This research report presents the evaluation of the Long-Span Guardrail system installed in front of a fall-protection fence. The design was evaluated through finite element modeling and simulation, followed by full-scale crash testing. Details of the simulation and crash testing evaluation are presented in this report.

The crash tests were performed to assess the performance of the Long-Span Guardrail installed in front of the fall-protection fence according to the safety-performance evaluation guidelines included in the second edition of the American Association of State Highway and Transportation Officials (AASHTO) Manual for Assessing Safety Hardware (MASH) (1). The crash tests were performed in accordance with MASH Test Level 3 (TL-3), which involves performing the following tests:

- 1. MASH Test 3-10: An 1100C vehicle weighing 2420 lb impacting the longitudinal barrier while travelling at 62 mi/h and 25 degrees.
- 2. MASH Test 3-11: A 2270P vehicle weighing 5000 lb impacting the longitudinal barrier while traveling at 62 mi/h and 25 degrees.

The Long-Span Guardrail installed in front of the fall-protection fence met the performance criteria for MASH TL-3 for longitudinal barrier.

17. Key Words		18. Distribution Statement			
Guardrail. Longitudinal Barriers.	No restrictions. This document is available to				
Fall Protection MASH Long-span Fence		the public through NTIS.			
	an, r erree,				
Handrail		National Technical Information Service			
		Alexandria, Virginia 22312			
		nttp://www.ntis.	gov		
19. Security Classification. (of this report) 20. Security Classificati		on. (of this page)	21. No. of Pages	22. Price	
Unclassified Unclassified			88		

Form DOT F 1700.7 (8-72) Reproduction of completed page authorized.

MASH TL-3 Evaluation of Long-Span W-Beam Guardrail in Front of Fall-Protection Fence

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> Report 617231-01-1&2 Contract No.: T 4541

Sponsored by the

Roadside Safety Pooled Fund and the Washington State Department of Transportation

August 2023

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The results reported herein apply only to the article tested. The full-scale crash tests were performed according to TTI Proving Ground quality procedures and American Association of State Highway and Transportation Officials (AASHTO) Manual for Assessing Safety Hardware, Second Edition (*MASH*) guidelines and standards.

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ACKNOWLEDGEMENTS

This research project was performed under a pooled fund program between the following States and Agencies. The authors acknowledge and appreciate their guidance and assistance.

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SI* (MODERN METRIC) CONVERSION FACTORS					
APPROXIMATE CONVERSIONS TO SI UNITS					
Symbol	When You Know	Multiply By	To Find	Symbol	
-	•	LENGTH	•		
in	inches	25.4	millimeters	mm	
ft	feet	0.305	meters	m	
yd	yards	0.914	meters	m	
mi	miles	1.61	kilometers	km	
		AREA		0	
In ²	square inches	645.2	square millimeters	mm²	
Π^2	square feet	0.093	square meters	m²	
yd-	square yards	0.830	square meters	m-	
ac mi ²	square miles	2 50	square kilometers	km ²	
	square miles		square kilometers	NIII	
floz	fluid ounces	29.57	milliliters	ml	
gal	gallons	3,785	liters	1	
ft ³	cubic feet	0.028	cubic meters	m ³	
yd ³	cubic yards	0.765	cubic meters	m ³	
5	NOTE: volumes g	greater than 1000L	shall be shown in m ³		
		MASS			
oz	ounces	28.35	grams	g	
lb	pounds	0.454	kilograms	kg	
Т	short tons (2000 lb)	0.907	megagrams (or metric ton")	Mg (or "t")	
~-	ТЕМРЕ	ERATURE (exac	t degrees)		
۳F	Fahrenheit	5(F-32)/9	Celsius	°C	
	FOROF	or (F-32)/1.8			
11-5	FURCE		or SIRESS	NI	
IDI Ibf/ip2	poundiorce	4.40	kilopascals	IN kPo	
				KI d	
Symbol	When You Know	Multiply By	To Find	Symbol	
- Cymie Ci		LENGTH		- Cjinzei	
mm	millimeters	0.039	inches	in	
m	meters	3.28	feet	ft	
m	meters	1.09	yards	yd	
km	kilometers	0.621	miles	mi	
		AREA			
mm ²	square millimeters	0.0016	square inches	in ²	
m ²	square meters	10.764	square feet	ft ²	
m ²	square meters	1.195	square yards	yd²	
ha	hectares	2.47	acres	ac	
KM ²	Square kilometers	0.386	square miles	mi ^	
ml	milliliters		fluid ounces	07	
1	litere	0.004	allons	al 20	
m ³	cubic meters	35 314	cubic feet	ft ³	
m ³	cubic meters	1.307	cubic vards	vd ³	
		MASS	,	,	
g	grams	0.035	ounces	oz	
kg	kilograms	2.202	pounds	lb	
Mg (or "t")	megagrams (or "metric ton")	1.103	short tons (2000lb)	Т	
	TEMPE	ERATURE (exac	t degrees)		
°C	Celsius	1.8C+32	Fahrenheit	°F	
FORCE and PRESSURE or STRESS					
N	newtons	0.225	poundforce	lbf	
l kPa	kilopascals	0.145	poundforce per square inch	lb/in ²	

*SI is the symbol for the International System of Units

Chapter 1. INTRODUCTION

Washington State Department of Transportation (WSDOT) has fish passages crossing state highways that use concrete culverts underneath the roadways. WSDOT commonly uses the Long-span W-beam guardrail system as the roadside barrier over the span of these culverts (WSDOT Standard Plan C-20.40-07). This system allows the guardrail to be installed across the width of the culvert without having to install the posts in soil while spanning the concrete culvert.

Maintenance workers and pedestrians may need to work or walk behind the guardrail system. Since this can be a fall hazard, WSDOT wants to install a fall-protection fence behind the Long-Span Guardrail system. The posts of the fence would be installed in the concrete culvert's headwall. The fence may be installed with some offset from the Long-Span Guardrail, or it may be installed with no offset from the back of the guardrail posts to the inner face of the culvert headwall.

WSDOT was concerned that the installation of a fall-protection fence behind the guardrail may interfere with the performance of the Long-Span Guardrail system, or there may be other hazards to an impacting vehicle that might lead to unsuccessful performance of the guardrail with the fence according to the safety-performance evaluation guidelines included in the American Association of State Highway and Transportation Officials (AASHTO) *Manual for Assessing Safety Hardware (MASH*), Second Edition (1).

In this project, the TTI research team evaluated the installation of a fall-protection fence behind the Long-Span Guardrail system using the *MASH* TL-3 evaluation criteria. The research team developed a finite element (FE) simulation model of the Long-Span Guardrail system with the fence installed with no offset from the back of the guardrail posts to the inner face of the culvert headwall. The research team then performed vehicle impact simulations with the guardrail and fence system using *MASH* TL-3 impact conditions and made recommendations for full-scale crash testing (as discussed in Chapter 2).

Full-scale crash testing was performed to assess the performance of the Long-Span Guardrail system installed in front of the fall-protection fence in accordance with *MASH* Test Level 3 (TL-3) (as discussed in Chapter 4).

Chapter 2. DESIGN AND SIMULATION

This chapter presents the details of the simulation analysis performed to assess the performance of the Long-Span Guardrail system with the fall-protection fence. The simulations were performed using the finite element (FE) method. LS-DYNA, which is a commercially available FE software was used for all simulations.

2.1. LONG-SPAN GUARDRAIL SYSTEM MODELING

The Long-Span Guardrail system was crash tested by Midwest Roadside Safety Facility (MwRSF) under MASH Test 3-11 criteria with a 5,000-lb pickup truck (2). This successful test led to acceptance of the Long-Span Guardrail system as a MASH TL-3 compliant system. The design was adopted by WSDOT in its standard plan C-20.40-07.

Key design details of the Long-Span Guardrail system test by MwRSF are shown in Figure 2.1. The test installation was comprised of 181.25 ft of standard W-beam guardrail supported by W6x9 steel posts. The guardrail spanned a 25-ft wide concrete culvert without any posts. Three adjacent posts on each side of the unsupported Wbeam guardrail span were timber CRT posts. The height to the top of the W-beam rail was 31.0 inches. A surrogate concrete culvert was used in the crash testing. It was comprised of 9.0-inch thick x 48.0-inch tall reinforced concrete wall that was installed flush with the back of the CRT posts. Some photos of MwRSF test installation are shown in Figure 2.2.



PLAN VIEW



Figure 2.1. Details of Long-Span Guardrail Test 3-11 (MwRSF Test LSC-2).



Figure 2.2. Long-Span Guardrail Test Installation Photos (MwRSF Test LSC-2).

2.1.1. FE Model Development and Validation

Since the fall-protection fence was to be installed behind the Long-Span Guardrail system described above, the researchers first developed a full-scale FE model of the guardrail system. To validate the guardrail system model, the researchers performed impact simulation with the model using the impact conditions of MASH Test 3-11 that was performed by MwRSF. The researchers then compared the simulation results with Test 3-11 results to establish that the guardrail model was reasonably valid for further use in assessing the guardrail with the fall-protection fence installed behind it.

The full-scale model of the Long-Span Guardrail system is shown in Figure 2.3. The model captured the test installation design used in Test 3-11. The model incorporated elastic-plastic material representation for the guardrail parts, which included the W-beam rail, steel posts, guardrail bolts, etc. The soil was incorporated into the model as a continuum surrounding each post. The culvert wall and the ground surface were modeled with rigid material representation since no movement or deflection of these parts was expected. The timber CRT posts were also included in the model. Their material properties incorporated failure of the wood, which is a key performance factor in the functioning of the CRT posts and the Long-Span Guardrail.





The researchers performed an impact simulation of the Long-span Guardrail System with a MASH pickup truck model using the impact conditions of the Test 3-11 performed by MwRSF. Figure 2.4 and Figure 2.5 show the sequential images comparing the results of the crash test and the simulation model. It can be observed that the simulation results closely matched the test results. Furthermore, the maximum dynamic rail deflection in the crash test was 73.1 inches at 74.7 inches downstream of post 13. In the simulation, the maximum dynamic deflection was 77.5 inches at 75.0 inches downstream of post 13. This implies that the simulation model closely matches the maximum dynamic deflection of the guardrail and the location of the dynamic deflection observed in the crash test.

Based on the above-mentioned comparisons of simulation and test results, the researchers concluded that the FE model of the Long-Span Guardrail System reasonably matched the test results and was therefore considered validated for further use in the assessment of a fall-protection fence behind the guardrail.



0.000 sec





0.094 sec



0.182 sec







0.422 sec





0.710 sec

Figure 2.4. Sequential Images Comparing Test and Simulation Results (Gut View).



0.992 sec

Figure 2.5. Sequential Images Comparing Test and Simulation Results (Top View).

2.2. GUARDRAIL WITH FALL-PROTECTION FENCE

WSDOT did not have a state standard for the fall-protection fence. However, for the purposes of this project, WSDOT provided drawings of an existing installation that uses such a fall-protection fence (Figure 2.6). The researchers used the details of this system to develop the preliminary fall-protection fence model for evaluation through simulation and crash testing. The fall-protection fence was comprised of posts and cross members of a typical industrial-grade chain-link fence hardware. The vertical posts were typical 2-inch NPS pipes, and the horizontal cross-members were 1-3/8-inch NPS pipes. Both were Schedule 40 pipes of ASTM A53 Grade A material. The posts were inserted into the concrete wall that had holes cast into them for embedding the posts. Cross members were attached to the posts at two locations along the height of the posts. The embedment of the posts in the concrete wall was 12 inches, and the

height of the fence to the center of the top cross members was 42 inches. Standard fencing hardware was used to attach the post to the cross members. In the simulation analysis and subsequent full-scale crash testing, the researchers used a surrogate concrete culvert wall that was only comprised of a section of the vertical wall. The model of the fall-protection fence incorporated into the long span guardrail system model is shown in Figure 2.7.



Figure 2.6. Fence System Drawings of a Current WSDOT Installation.



(a) Plan View



(b) Isometric View of Full Model

Figure 2.7. FE Model of Fall-Protection Fence with Long-Span Guardrail System.

After developing the model of the fall-protection fence and the Long-Span Guardrail system, the researchers performed MASH Test 3-11 and Test 3-10 impact simulations. These involved impacting the guardrail system with a 5,000-lb pickup truck (Test 3-11) and a 2,420-lb small car (Test 3-10) at an impact speed and angle of 62 mi/h and 25 degrees, respectively. The pickup truck and the small car models used in the simulations were developed by Center for Collision Safety and Analysis and were improved over the course of various projects by TTI researchers to achieve better validations and robustness. Details of the simulations are presented next.

2.2.1. MASH Test 3-11 Simulation Analysis

In this simulation, the pickup truck model impacted the Long-span Guardrail system 41 ft-3 inches upstream of the first downstream post after the long unsupported span of the guardrail. This impact point was similar to the one selected in the full-scale crash testing of the Long-Span Guardrail system performed by MwRSF. Results of the simulation are presented in Figure 2.8 and Table 2.1. The vehicle was successfully

contained and redirected in a stable manner. The occupant risk numbers were within MASH thresholds. The maximum dynamic and permanent deflections of the guardrail were about 55 inches and 49 inches, respectively. Based on the results of the simulation, the system was expected to pass MASH Test 3-11.





Occurrent Impact Valacity (ft/c)	Longitudinal	11.48
	Lateral	-11.81
Didedown Acceleration (a)	Longitudinal	-7.3
Ridedown Acceleration (g)	Lateral	6.4
	Roll	-7.4
Max. Angles (degrees)	Pitch	2.5
	Yaw	36.3

Table 2.1 Occupant Risk Factors for MASH Test Level 3-11 Simulations.

2.2.2. MASH Test 3-10 Simulation Analysis

For MASH Test 3-10 impact condition, the researchers evaluated the design at two impact locations with the goal of selecting the more critical of the two for full-scale crash testing. One of the impact locations was upstream on the CRT posts and the other was at the midpoint of the unsupported long-span of the W-beam rail.

Figure 2.9 and Figure 2.10 show the results of the simulation at the impact point upstream of the CRT posts and at the midpoint of the long-span guardrail section, respectively. The MASH occupant risk factors are presented in Table 2.2

In both simulations, the vehicle was successfully contained and redirected. The occupant risk numbers were within MASH thresholds. The maximum dynamic and permanent deflections of the guardrail were about 57 inches and 27 inches, respectively for the impact upstream of the CRT posts. The maximum dynamic and permanent deflections of the guardrail were about 55 inches and 32 inches, respectively for the impact at the midpoint of the long-span of the W-beam guardrail.

While the two impact points performed very similar to each other, the research team recommended crash testing with the impact point upstream of the CRT posts as the vehicle encountered greater number of fence posts and had more opportunity to drop into the culvert compared to the impact at midpoint between the long-span rail section.







0.0 s



0.10 s



0.8 s

Figure 2.10. MASH Test 3-10 Impact Simulation Sequential Images for Impact at Midpoint of the Long-Span.

Impact Point	Midpoint of Long-Span	Between CRT Posts	
Occupant Impact Velocity	Longitudinal.	27.56	20.01
(ft/s)	Lateral	16.40	14.11
Ridedown Acceleration	Longitudinal.	-12.7	-14.0
(g)	Lateral	-7.8	12.4
	Roll	8.7	10.2
Max. Angles (degrees)	Pitch	4.3	3.7
	Yaw	53.2	34.7

Table 2.2 Occupant Risk Factors for MASH Test Level 3-10 Simulations.

Based on the successful results of the simulations for Test 3-11 and Test 3-10 impact conditions, the researchers recommended performing full-scale crash testing of the Long-Span Guardrail System with the fall-protection fence installed behind it, while having no offset from back of post to inner face of headwall. The details of the crash tested system are presented in the following chapter.

Chapter 3. SYSTEM DETAILS

3.1. TEST ARTICLE AND INSTALLATION DETAILS

The installation consisted of a Long-Span Guardrail system with a fall-protection fence installed behind it. The Long-Span Guardrail system was comprised of a W-beam guardrail that was 181 feet 3 inches long, with 13 posts on the upstream end spaced at 75 inches, then a span of 25 feet where no posts were present, and then 14 posts spaced at 75 inches. Posts 3 through 10 and 17 through 25 were 72-inch-long standard wide flange guardrail posts, with 12-inch timber blockouts that held the W-beam guardrail 31 inches above grade to the top of the rail. Posts 11 through 16 were CRT timber posts with 12-inch wood blockouts. The ends of the installation were terminated with a steel rail terminal.

Centered between posts 13 and 14, and beginning at 20 inches from the field side of the W-beam rail element, was an embedded 24-inch tall and 14 inches wide concrete wall mounted on an 8 inch thick slab. The slab spanned 23 feet in length and 96 inches wide, with the vertical wall set parallel with the length of the slab. A 71-inch section of 24-inch tall wall on either end of the slab extended out past the slab towards the field side at a 45 degree angle. Mounted on top of the parapet was a fall-protection handrail with posts spaced at 54 inches parallel to the guardrail and at 62 inches on the wings at each end, with two cross members between each handrail post.

Figure 3.1 presents the overall information on the Long-Span Guardrail with the fall-protection fence, and Figure 3.2 thru Figure 3.7 provide photographs of the installation. Appendix A provides further details on the test installation. Drawings were provided by the Texas A&M Transportation Institute (TTI) Proving Ground, and construction was performed by TTI Proving Ground Personnel.

3.2. DESIGN MODIFICATIONS DURING TESTS

No modifications were made to the installation during the testing phase.



Figure 3.1. Details of Long-Span Guardrail System with Fall-Protection Fence.



Figure 3.2. An Overall View of the Test Installation.



Figure 3.3. Upstream In-Line View of the Test Installation.


Figure 3.4. Test Installation at Impact Point Prior to Testing.



Figure 3.5. Downstream In-line View of the Test Installation Prior to Testing.



Figure 3.6. Field Side View of the Test Installation Prior to Testing.



Figure 3.7. Test Installation's Upstream End Terminal Prior to Testing.

3.3. MATERIAL SPECIFICATIONS

Appendix B provides material certification documents for the materials used to install/construct the Long-Span Guardrail with the fall-protection fence. Table 3.1 shows the average compressive strengths of the concrete on the day of the test 2023-02-13.

Location	Design Strength (psi)	Average Strength (psi)	Age (days)	Detailed Location
Moment Slab	4500	4540	23	100% of slab
Deck	4500	4683	14	100% of deck

Table 3.1. Concrete Strength.

3.4. SOIL CONDITIONS

The test installation was installed in standard soil meeting Type 1 Grade D of AASHTO standard specification M147-17 "Materials for Aggregate and Soil Aggregate Subbase, Base, and Surface Courses."

In accordance with Appendix B of *MASH*, soil strength was measured the day of the crash test. During installation of the guardrail for full-scale crash testing, two 6-ft long W6×16 posts were installed in the immediate vicinity of the test installation using the same fill materials and installation procedures used in the test installation and the standard dynamic test.

On the day of Test 3-10, 2023-02-13, loads on the post at deflections were as follows: the backfill material in which the test installation was installed met the minimum *MASH* requirements for soil strength.

Displacement (in)	Minimum Load (lb)	Actual Load (lb)	
5	4420	8757	
10	4981	8969	
15	5282	8242	

Table 3.2. Soil Strength for Test 617231-01-1.

On the day of Test 3-11, 2023-02-23, loads on the post at deflections were as follows: the backfill material in which the Long-Span Guardrail was installed met the minimum *MASH* requirements for soil strength.

Table 3.3. Soil Strength for Test 617231-01-2.

Displacement (in)	Minimum Load (lb)	Actual Load (Ib)
5	4420	8454
10	4981	9818
15	5282	10787

Chapter 4. TEST REQUIREMENTS AND EVALUATION CRITERIA

4.1. CRASH TEST PERFORMED/MATRIX

Table 4.1 shows the test conditions and evaluation criteria for *MASH* TL-3 for Longitudinal Barriers. The target critical impact points (CIPs) for each test were determined using the information provided in Chapter 2. Figure 4.1 shows the target CIP for *MASH* TL-3 tests on the Long-Span Guardrail with fall-protection fence.

Table 4.1. Test Conditions and Evaluation Criteria Specified for MASH TL-3 for
Longitudinal Barriers.

	De	Te sig	est nat	tion	l	Те	st '	Veh	icle	lr os	npact Speed	Impac Angle	ct e	Evaluation Criteria	
		3-	10			1100C		6	2 mi/h	25°		A, D, F, H, I			
		3-	11			2270P			6	2 mi/h	25°		A, D, F, H, I		
2	6 	24	ň	22 ă	ň	20 4	ň	18	16 # #	A	14 8		1		
											L		act P	Path, 3-10 and 3-11	

Figure 4.1. Target CIP for MASH TL-3 Tests on the Test Installation.

The crash tests and data analysis procedures were in accordance with guidelines presented in *MASH*. Chapter 4 presents brief descriptions of these procedures.

4.2. EVALUATION CRITERIA

The appropriate safety evaluation criteria from Tables 2.2 and 5.1 of *MASH* were used to evaluate the crash tests reported herein. Table 4.1 lists the test conditions and evaluation criteria required for *MASH* TL-3, and Table 4.2 provides detailed information on the evaluation criteria.

Evaluation Factors	Evaluation Criteria
A.	Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.
D.	Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present undue hazard to other traffic, pedestrians, or personnel in a work zone. Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of <i>MASH</i> .
F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.
H.	Occupant impact velocities (OIV) should satisfy the following limits: Preferred value of 30 ft/s, or maximum allowable value of 40 ft/s. Occupant impact velocities (OIV) should satisfy the following limits: Preferred value of 10 ft/s, or maximum allowable value of 16 ft/s.
Ι.	The occupant ridedown accelerations should satisfy the following: Preferred value of 15.0 g, or maximum allowable value of 20.49 g.

 Table 4.2. Evaluation Criteria Required for MASH Testing.

Chapter 5. TEST CONDITIONS

5.1. TEST FACILITY

The full-scale crash tests reported herein were performed at the TTI Proving Ground, an International Standards Organization (ISO)/International Electrotechnical Commission (IEC) 17025-accredited laboratory with American Association for Laboratory Accreditation (A2LA) Mechanical Testing Certificate 2821.01. The full-scale crash tests were performed according to TTI Proving Ground quality procedures, as well as *MASH* guidelines and standards.

The test facilities of the TTI Proving Ground are located on The Texas A&M University System RELLIS Campus, which consists of a 2000-acre complex of research and training facilities situated 10 mi northwest of the flagship campus of Texas A&M University. The site, formerly a United States Army Air Corps base, has large expanses of concrete runways and parking aprons well suited for experimental research and testing in the areas of vehicle performance and handling, vehicle-roadway interaction, highway pavement durability and efficacy, and roadside safety hardware and perimeter protective device evaluation. The sites selected for construction and testing are along the edge of an out-of-service apron/runway. The apron/runway consists of an unreinforced jointed-concrete pavement in 12.5-ft × 15-ft blocks nominally 6 inches deep. The aprons were built in 1942, and the joints have some displacement but are otherwise flat and level.

5.2. VEHICLE TOW AND GUIDANCE SYSTEM

For the testing utilizing the 1100C and 2270P vehicles, each was towed into the test installation using a steel cable guidance and reverse tow system. A steel cable for guiding the test vehicle was tensioned along the path, anchored at each end, and threaded through an attachment to the front wheel of the test vehicle. An additional steel cable was connected to the test vehicle, passed around a pulley near the impact point and through a pulley on the tow vehicle, and then anchored to the ground such that the tow vehicle moved away from the test site. A 2:1 speed ratio between the test and tow vehicle existed with this system. Just prior to impact with the installation, the test vehicle was released and ran unrestrained. The vehicle remained freewheeling (i.e., no steering or braking inputs) until it cleared the immediate area of the test site.

5.3. DATA ACQUISITION SYSTEMS

5.3.1. Vehicle Instrumentation and Data Processing

Each test vehicle was instrumented with a self-contained onboard data acquisition system. The signal conditioning and acquisition system is a multi-channel data acquisition system (DAS) produced by Diversified Technical Systems Inc. The accelerometers, which measure the x, y, and z axis of vehicle acceleration, are strain gauge type with linear millivolt output proportional to acceleration. Angular rate sensors,

measuring vehicle roll, pitch, and yaw rates, are ultra-small, solid-state units designed for crash test service. The data acquisition hardware and software conform to the latest SAE J211, Instrumentation for Impact Test. Each of the channels is capable of providing precision amplification, scaling, and filtering based on transducer specifications and calibrations. During the test, data are recorded from each channel at a rate of 10,000 samples per second with a resolution of one part in 65,536. Once data are recorded, internal batteries back these up inside the unit in case the primary battery cable is severed. Initial contact of the pressure switch on the vehicle bumper provides a time zero mark and initiates the recording process. After each test, the data are downloaded from the DAS unit into a laptop computer at the test site. The Test Risk Assessment Program (TRAP) software then processes the raw data to produce detailed reports of the test results.

Each DAS is returned to the factory annually for complete recalibration and to ensure that all instrumentation used in the vehicle conforms to the specifications outlined by SAE J211. All accelerometers are calibrated annually by means of an ENDEVCO® 2901 precision primary vibration standard. This standard and its support instruments are checked annually and receive a National Institute of Standards Technology (NIST) traceable calibration. The rate transducers used in the data acquisition system receive calibration via a Genisco Rate-of-Turn table. The subsystems of each data channel are also evaluated annually, using instruments with current NIST traceability, and the results are factored into the accuracy of the total data channel per SAE J211. Calibrations and evaluations are also made anytime data are suspect. Acceleration data are measured with an expanded uncertainty of ± 1.7 percent at a confidence factor of 95 percent (k = 2).

TRAP uses the DAS-captured data to compute the occupant/compartment impact velocities, time of occupant/compartment impact after vehicle impact, and highest 10-millisecond (ms) average ridedown acceleration. TRAP calculates change in vehicle velocity at the end of a given impulse period. In addition, maximum average accelerations over 50-ms intervals in each of the three directions are computed. For reporting purposes, the data from the vehicle-mounted accelerometers are filtered with an SAE Class 180-Hz low-pass digital filter, and acceleration versus time curves for the longitudinal, lateral, and vertical directions are plotted using TRAP.

TRAP uses the data from the yaw, pitch, and roll rate transducers to compute angular displacement in degrees at 0.0001-s intervals, and then plots yaw, pitch, and roll versus time. These displacements are in reference to the vehicle-fixed coordinate system with the initial position and orientation being initial impact. Rate of rotation data is measured with an expanded uncertainty of ± 0.7 percent at a confidence factor of 95 percent (k = 2).

5.3.2. Anthropomorphic Dummy Instrumentation

An Alderson Research Laboratories Hybrid II, 50th percentile male anthropomorphic dummy, restrained with lap and shoulder belts, was placed in the front seat on the impact side of impact of the 1100C vehicle. The dummy was not instrumented. According to *MASH*, use of a dummy in the 2270P vehicle is optional, and no dummy was used in the test.

5.3.3. Photographic Instrumentation Data Processing

Photographic coverage of each test included three digital high-speed cameras:

- One located overhead with a field of view perpendicular to the ground and directly over the impact point.
- One placed upstream from the installation at an angle to have a field of view of the interaction of the rear of the vehicle with the installation.
- A third placed with a field of view parallel to and aligned with the installation at the downstream end.

A flashbulb on the impacting vehicle was activated by a pressure-sensitive tape switch to indicate the instant of contact with the Long-Span Guardrail. The flashbulb was visible from each camera. The video files from these digital high-speed cameras were analyzed to observe phenomena occurring during the collision and to obtain timeevent, displacement, and angular data. A digital camera recorded and documented conditions of each test vehicle and the installation before and after the test.

Chapter 6. MASH TEST 3-10 (CRASH TEST 617231-01-1)

6.1. TEST DESIGNATION AND ACTUAL IMPACT CONDITIONS

See Table 6.1 for details of *MASH* impact conditions for this test and Table 6.2 for the exit parameters. Figure 6.1 and Figure 6.2 depict the target impact setup.

Test Parameter	Specification	Tolerance	Measured
Impact Speed (mi/h)	62	±2.5 mi/h	62.7
Impact Angle (deg)	25	±1.5°	24.8
Impact Severity (kip-ft)	51	≥51 kip-ft	56.2
Impact Location	45 inches upstream from the centerline of post 11	± 12 inches	44 inches upstream from the centerline of post 11

Table 6.1. Impact Conditions for MASH TEST 3-10, Crash Test 617231-01-1.

Table 6.2. Exit Parameters for MASH TEST 3-10, Crash Test 617231-01-1.

Exit Parameter	Measured
Speed (mi/h)	Not Measurable
Trajectory (deg)	Not Measurable
Heading (deg)	Not Measurable
Brakes applied post impact (s)	>5
Vehicle at rest position	72 ft downstream of impact point 58 ft to the traffic side 80° left
Comments:	Vehicle remained upright and stable. Vehicle crossed the exit box ^a 14 ft downstream from loss of contact.

^a Not less than 32.8 ft downstream from loss of contact for cars and pickups is optimal.



Figure 6.1. Test Installation/Test Vehicle Geometrics for Test 617231-01-1.



Figure 6.2. Test Installation/Test Vehicle Impact Location for Test 617231-01-1.

6.2. WEATHER CONDITIONS

Table 6.3 provides the weather conditions for Test 617231-01-1.

Date of Test	2023-02-13 AM
Wind Speed (mi/h)	6
Wind Direction (deg)	184
Temperature (°F)	59
Relative Humidity (%)	83
Vehicle Traveling (deg)	195

 Table 6.3. Weather Conditions for Test 617231-01-1.

6.3. TEST VEHICLE

Figure 6.3 and Figure 6.4 show the 2019 Nissan Versa used for the crash test. Table 6.4 shows the vehicle measurements. Figure C.1 in Appendix C.1 gives additional dimensions and information on the vehicle.



Figure 6.3. Impact Side of Test Vehicle before Test 617231-01-1.



Figure 6.4. (Opposite Im	pact Side of	Test Vehicle	before Te	st 617231-01-1.

Test Parameter	Specification	Tolerance	Measured
Dummy (if applicable)ª (lb)	165	N/A	165
Inertial Weight (lb)	2420	±55	2430
Gross Static ^a (lb)	2585	±25	2595
Wheelbase (inches)	98	±5	102.4
Front Overhang (inches)	35	±4	32.5
Overall Length (inches)	169	±8	175.4
Overall Width (inches)	65	±3	66.7
Hood Height (inches)	28	±4	30.5
Track Width ^b (inches)	59	±2	58.4
CG aft of Front Axle ^c (inches)	39	±4	41.7
CG above Ground ^{c,d} (inches)	N/A	N/A	N/A

Table 6.4. Vehicle Measurements for Test 617231-01-1.

Note: N/A = not applicable; CG = center of gravity. ^a If a dummy is used, the gross static vehicle mass should be increased by the mass of the dummy.

^b Average of front and rear axles.

^c For test inertial mass.

^d 2270P vehicle must meet minimum CG height requirement.

6.4. TEST DESCRIPTION

Table 6.5 lists events that occurred during Test 617231-01-1. Figures C.4, C.5, and C.6 in Appendix C.2 present sequential photographs during the test.

Time (s)	Events
0.0000	Vehicle impacted the installation
0.0130	Post 11 began to lean toward field side
0.0320	Vehicle began to redirect
0.0330	Post 12 began to lean toward field side
0.0620	Post 10 began to twist clockwise
0.1740	W-beam rail contacted handrail post #2
0.2360	Handrail post #2 contacted by right front tire and sheared off at grade
0.2420	Vehicle was parallel with installation
0.3180	Handrail post #3 contacted by right front tire, and bent over
0.6750	Vehicle lost contact with guardrail

Table 6.5. Events during Test 617231-01-1.

6.5. DAMAGE TO TEST INSTALLATION

There was some soil disturbance at post 9. Post 10 had a 0.5-inch soil gap on the traffic and field sides of the post and was leaning back 1 degree from vertical. Posts 11 through 13 were broken off at grade. Post 14 had a 0.5-inch gap in the soil on the traffic side of the post and was leaning 1 degree back from vertical. The fall-protection fence was also damaged, with post 2 broken off at grade, post 3 leaning downstream, and post 4 leaning towards the field side and downstream. The rail cross members released from posts 1 through the upstream side of post 4. One cross member travelled 111 feet towards the traffic side and 322 feet downstream.

Table 6.6 presents the deflection and working width of the Long-Span Guardrail. Figure 6.5 and Figure 6.6 show the damage to the test installation.

Table 6.6. Deflection and Working Width of the Long-Span Guardrail forTest 617231-01-1.

Test Parameter	Measured
Permanent Deflection/Location	18.9 inches toward field side, at the centerline of post 12
Dynamic Deflection	38.2 inches toward field side between posts 12 and 13
Working Width ^a and Height	46.2 inches, at a height of 16 inches at the front impact side tire

^a Per *MASH*, "The working width is the maximum dynamic lateral position of any major part of the system or vehicle. These measurements are all relative to the pre-impact traffic face of the test article." In other words, working width is the total barrier width plus the maximum dynamic intrusion of any portion of the barrier or test vehicle past the field side edge of the barrier.



Figure 6.5. Test Installation from the Field Side at Impact Location after Test 617231-01-1.



Figure 6.6. Test Installation from the Field Side at Impact Location after Test 617231-01-1.

6.6. DAMAGE TO TEST VEHICLE

Figure 6.7 and Figure 6.8 show the damage sustained by the vehicle. Figure 6.9 and Figure 6.10 show the interior of the test vehicle. Table 6.7 and Table 6.8 provide details on the occupant compartment deformation and exterior vehicle damage. Figures C.2 and C.3 in Appendix C.1 provide exterior crush and occupant compartment measurements.



Figure 6.7. Front Impact Side of Test Vehicle after Test 617231-01-1.



Figure 6.8. Rear Impact Side of Test Vehicle after Test 617231-01-1.



Figure 6.9. Overall Interior of Test Vehicle after Test 617231-01-1.



Figure 6.10. Interior of Test Vehicle on Impact Side after Test 617231-01-1.

Test Parameter	Specification	Measured
Roof	≤4.0 inches	0 inches
Windshield	≤3.0 inches	0 inches
A and B Pillars	≤5.0 overall/≤3.0 inches lateral	0 inches
Foot Well/Toe Pan	≤9.0 inches	0 inches
Floor Pan/Transmission Tunnel	≤12.0 inches	1.5 inches
Side Front Panel	≤12.0 inches	1 inch
Front Door (above Seat)	≤9.0 inches	1.5 inches
Front Door (below Seat)	≤12.0 inches	0 inches

 Table 6.7. Occupant Compartment Deformation in Test 617231-01-1.

Table 6.8. Exterior Vehicle Damage in Test 617231-01-1.

Side Windows	The side windows remained intact
Maximum Exterior Deformation	10 inches in the front plane at the right front corner at bumper height
VDS	01RFQ3
CDC	01FREW2
Fuel Tank Damage	None
Description of Damage to Vehicle:	The front bumper, hood, grill, right headlight, right front quarter fender, right front tire and rim, right front strut and tower, right lower control arm, right CV shaft and joints, right front and rear door, right rear quarter fender, rear bumper, front rack and pinion, steering shaft, and right rocker panel were damaged. The right front door had a 1.5-inch gap at the top.

6.7. OCCUPANT RISK FACTORS

Data from the accelerometers were digitized for evaluation of occupant risk, and the results are shown in Table 6.9. Figure C.7 in Appendix C.3 shows the vehicle angular displacements, and Figures C.8 through C.10 in Appendix C.4 show acceleration versus time traces.

Test Parameter	Specification ^a	Measured	Time
OIV, Longitudinal (ft/s)	≤40.0	14.0	0.1182 seconds on right side of
	30.0		interior
OIV, Lateral (ft/s)	≤40.0	19.1	0.1182 seconds on right side of
	30.0		interior
Ridedown, Longitudinal	≤20.49	8.5	0.3034 - 0.3134 seconds
(g)	15.0		
Ridedown, Lateral (g)	≤20.49	10.2	0.2599 - 0.2699 seconds
	15.0		
Theoretical Head Impact	N/A	7.1	0.1149 seconds on right side of
Velocity (THIV) (m/s)			interior
Acceleration Severity	N/A	0.8	0.0950 - 0.1450 seconds
Index (ASI)			
50-ms Moving Avg.	N1/A	4.0	0.0664 0.1164 accords
Accelerations (MA)	N/A	-4.8	0.0664 - 0.1164 seconds
50 ms MA Lateral (g)	Ν/Λ	6.6	0.0387 0.0887 seconds
		-0.0	
50-ms MA Vertical (g)	N/A	2.6	0.3159 - 0.3659 seconds
Roll (deg)	≤75	9.2	2.0000 seconds
Pitch (deg)	≤75	8.2	2.0000 seconds
Yaw (deg)	N/A	105.6	2.0000 seconds

Table 6.9. Occupant Risk Factors for Test 617231-01-1.

^{a.} Values in italics are the preferred MASH values

6.8. TEST SUMMARY

Figure 6.11 summarizes the results of MASH Test 617231-01-1.

Test Agency			Теха	s A&M Trans	portation Institute (TT	TI)			
			Test Standard/Test No.			MASH 2016, Test 3-10			
and the second his life		TTI Project No. 6			6172	617231-01-1			
		Test Date			2023-02-13				
	Æ	ANTI	TEST /	ARTICL	E				
		Туре		Long	itudinal Barrie	r			
				Name	Long	-Span Guardr	ail with Fall-Protection	on Fence	
		and a state of the second			Length	181 f	eet 3 inches		
0	.000 s				Key Materials	W-be posts Grad	eam guardrail, s, CRT timber e A pipe	72-inch wide-flange posts, sch. 40 ASTM	steel 1 A53
and a state	1. 11.			Soil Ty	vpe and Condition	AASI conc	HTO M147 gra rete	ading D type 1 crush	ed
	ANZ.		TEST \	/EHICL	E				
		-5-9-0-0			Type/Designation	1100	С		
	THE !!			Year,	Make and Model	2019	Nissan Versa	1	
Construction of the second of the second of the	1.	ar the		l	nertial Weight (lb)	2430	1		
		and the second se			Dummy (lb)	165			
					Gross Static (lb)	2595			
0	.200 s		IMPAC		DITIONS				
				Im	pact Speed (mi/h)	62.7			
				In	npact Angle (deg)	24.8			
	and the				Impact Location	44 in	ches upstrear	n from centerline of p	oost 11
	JAR VINY	2000 m		Impa	ct Severity (kip-ft)	56.18	367426757816	6	
A State			EXIT C	ONDIT	IONS				
			Exit Speed (mi/h) N			Not N	Not Measurable		
		And I am	Trajec	Trajectory/Heading Angle (deg)		Not N	/leasurable / N	Not Measurable	
		-			Exit Box Criteria	Vehio from	cle crossed the loss of contact	e exit box a 14 ft dov st.	vnstream
0	.400 s	-		5	Stopping Distance	72 ft 58 ft	downstream to the traffic s	ide	
			TEST /	ARTICL	E DEFLECTIONS				
					Dynamic (inches)	38.2			
	and they	-		Pe	ermanent (inches)	18.87	75		
here and a second	100-	D	Workir	ng Width	n / Height (inches)	46.2	/ 16		
an side	TEAS'	10	VEHIC	LE DAN	IAGE				
and a famile	- Bries				VDS	01RF	EQ3		
and the second se	MR. A.	and the second second			CDC	01FF	REW2		
			Max.	Ext. Def	ormation (inches)	10			
0	600 0	-	Max	(Occup	ant Compartment	1.5 ir	nches in the rig	ght floor pan and righ	nt driver's
0	.000 5		0	CCUPA	NT RISK VALUES	side	0001		
Long, OIV (ft/s)	14.0	Lona, Ridedo	wn (a)	8.5	Max 50-ms Long	(a)	-4.8	Max Roll (deg)	9.2
Lat. OIV (ft/s)	19.1	Lat. Ridedowi	n (g)	10.2	Max 50-ms Lat. (q)	-6.6	Max Pitch (deg)	8.2
THIV (m/s)	7.1	ASI	0.8 Max 50-ms Vert. (a)			(g)	2.6	Max Yaw (deg)	105.6
58'						ana Bat, xi ar exist Ru (part conta train version Part Candrale Bat Pr Wate-Parage Guardial Poul Section B.B Type anterpart (1) - 10 Section B.C Type anterpart (1) - 10 Pr Vide-Parage Guardial Poul Pr Vide-P	n: Blochout, for Wood Pood All X 2 Washer: 56 F364 —22° Guadriani Bok CRT Tenter:Pool for 31° rail		
	1								

Figure 6.11. Summary of Results for *MASH* Test 3-10 on Long-Span Guardrail with Fall-Protection Fence.

Chapter 7. MASH TEST 3-11 (CRASH TEST 617231-01-2)

7.1. TEST DESIGNATION AND ACTUAL IMPACT CONDITIONS

See Table 7.1 for details of *MASH* impact conditions for this test and Table 7.2 for the exit parameters. Figure 7.1 and Figure 7.2 depict the target impact setup.

Test Parameter	Specification	Tolerance	Measured
Impact Speed (mi/h)	62	±2.5 mi/h	62.2
Impact Angle (deg)	25	±1.5°	24.9
Impact Severity (kip-ft)	106	≥≥106 kip-ft	115.6
Impact Location	45 inches upstream from the centerline of post 11.	±12 inches	46.3 inches upstream from the centerline of post 11.

Table 7.1. Impact Conditions for MASH TEST 3-11, Crash Test 617231-01-2.

Table 7.2. Exit Parameters for	MASH TEST 3-11,	Crash Test 617231-01-2.
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Exit Parameter	Measured
Speed (mi/h)	Not Measurable
Trajectory (deg)	Not Measurable
Heading (deg)	Not Measurable
Brakes applied post impact (s)	3.25
Vehicle at rest position	182 ft downstream of impact point 8 ft to the field side 75° right
Comments:	Vehicle remained upright and stable. Vehicle crossed the exit box a 47 ft downstream from loss of contact.

^a Not less than 32.8 ft downstream from loss of contact for cars and pickups is optimal.



Figure 7.1Test Installation/Test Vehicle Geometrics for Test 617231-01-2.



Figure 7.2. Test Installation/Test Vehicle Impact Location for Test 617231-01-2.

7.2. WEATHER CONDITIONS

Table 7.3 provides the weather conditions for Test 617231-01-2.

Date of Test	2023-02-23 AM
Wind Speed (mi/h)	8
Wind Direction (deg)	66
Temperature (°F)	76
Relative Humidity (%)	75
Vehicle Traveling (deg)	195

 Table 7.3. Weather Conditions for Test 617231-01-2.

7.3. TEST VEHICLE

Figure 7.3 and Figure 7.4 show the 2017 RAM 1500 used for the crash test. Table 7.4 shows the vehicle measurements. Figure D.1 in Appendix D.1 gives additional dimensions and information on the vehicle.



Figure 7.3. Impact Side of Test Vehicle before Test 617231-01-2.



Figure 7.4. Opposite Impact Side of Test Vehicle before Test 617231-01-2.

Test Parameter	Specification	Tolerance	Measured
Dummy (if applicable)ª (lb)	165	N/A	165
Inertial Weight (lb)	5000	±110	5043
Gross Static ^a (lb)	5165	±5000	5208
Wheelbase (inches)	148	±12	140.5
Front Overhang (inches)	39	±3	40.0
Overall Length (inches)	237	±13	227.5
Overall Width (inches)	78	±2	78.5
Hood Height (inches)	43	±4	46.0
Track Width ^b (inches)	67	±1.5	68.25
CG aft of Front Axle ^c (inches)	63	±4	60.9
CG above Ground ^{c,d} (inches)	28	≥28	28.5

Table 7.4. Vehicle Measurements for Test 617231-01-2.

Note: N/A = not applicable; CG = center of gravity.

^a If a dummy is used, the gross static vehicle mass should be increased by the mass of the dummy.

^b Average of front and rear axles.
 ^c For test inertial mass.

^d 2270P vehicle must meet minimum CG height requirement.

7.4. TEST DESCRIPTION

Table 7.5 lists events that occurred during Test 617231-01-2. Figures D.4, D.5, and D.6 in Appendix D.2 present sequential photographs during the test.

Time (s)	Events
0.0000	Vehicle impacted the installation
0.0080	Post 11 and 10 began to lean toward field side
0.0470	Vehicle began to redirect
0.0480	Post 12 began to lean toward field side
0.0910	Post 13 began to lean toward field side
0.1330	Handrail post #2 was contacted by the W-beam guardrail just past guardrail post 13 and began leaning downstream and toward field side.
0.1500	Guardrail contacted handrail post 3, and the handrail and post began leaning toward field side
0.1660	Guardrail contacted handrail post 4, and the handrail and post began leaning toward field side
0.2200	Front passenger side tire left ground over embankment
0.3370	Vehicle was parallel with installation
0.5070	Vehicle right side left embankment area, leaving the front passenger side tire behind.

Table 7.5. Events during Test 617231-01-2.

7.5. DAMAGE TO TEST INSTALLATION

The rail released from post 2 through 17. Posts 8 and 9 were twisted clockwise, posts 11 through 14 broke off at grade, and post 15 was split at the guardrail bolt. Handrail posts 2 through 7 were bent over and their crossmembers released from the posts. Table 7.6 presents the soil gap around the posts and the post lean after the crash test. Table 7.7 presents the deflection and working width of the Long-Span Guardrail. Figure 7.5 and Figure 7.6 show the damage to the test installation.

Post	Soil Gap	Post Lean (from vertical)
1	3 inches u/s	8.1° d/s
2	2.5 inches u/s	4.8° d/s
8	soil disturbed	-
9	0.125 inches	1.6° f/s
10	0.5 inches f/s; 2 inches t/s	11.4° f/s
15	0.25 inches t/s	0.9 [°] f/s
16	soil disturbed	-

Table 7.6 Soil Gap Around Post and Post Lean after Test 617231-01-2.

u/s: upstream; d/s: downstream; f/s: field side; t/s: traffic side; -:zero measurement

Table 7.7. Deflection and Working Width of the Long-Span Guardrail for Test617231-01-2.

Test Parameter	Measured
Permanent Deflection/Location	48 inches toward field side, 22 inches upstream from the centerline of handrail post 5
Dynamic Deflection	64.9 inches toward field side, between posts 13 and 14
Working Width ^a and Height	72.3 inches, at a height of 59.4 inches at the right-side mirror

^a Per *MASH*, "The working width is the maximum dynamic lateral position of any major part of the system or vehicle. These measurements are all relative to the pre-impact traffic face of the test article." In other words, working width is the total barrier width plus the maximum dynamic intrusion of any portion of the barrier or test vehicle past the field side edge of the barrier.



Figure 7.5. Overall View of Test Installation after Test 617231-01-2.



Figure 7.6. Long-Span Guardrail at the Maximum Permanent Deformation after Test 617231-01-2.

7.6. DAMAGE TO TEST VEHICLE

Figure 7.7 and Figure 7.8 show the damage sustained by the vehicle. Figure 7.9 and Figure 7.10 show the interior of the test vehicle. Table 7.8 and Table 7.9 provide details on the occupant compartment deformation and exterior vehicle damage. Figures D.2 and D.3 in Appendix D.1 provide exterior crush and occupant compartment measurements.



Figure 7.7. Front Impact Side of Test Vehicle after Test 617231-01-2.



Figure 7.8. Rear Impact Side of Test Vehicle after Test 617231-01-2.



Figure 7.9. Overall Interior of Test Vehicle after Test 617231-01-2.



Figure 7.10. Interior of Test Vehicle on Impact Side after Test 617231-01-2.

Test Parameter	Specification	Measured
Roof	≤4.0 inches	0 inches
Windshield	≤3.0 inches	0 inches
A and B Pillars	≤5.0 overall/≤3.0 inches lateral	0 inches
Foot Well/Toe Pan	≤9.0 inches	0 inches
Floor Pan/Transmission	≤12.0 inches	0 inches
Tunnei		
Side Front Panel	≤12.0 inches	0 inches
Front Door (above Seat)	≤9.0 inches	0 inches
Front Door (below Seat)	≤12.0 inches	0 inches

Table 7.8. Occu	pant Compartmer	nt Deformation fo	r Test 617231-01-2.
	pant oomparanoi	it bololination lo	

Side Windows	The side windows remained intact	
Maximum Exterior Deformation	12 inches in the front plane at the right front corner at bumper height	
VDS	01RFQ3	
CDC	01FREW2	
Fuel Tank Damage	None	
Description of Damage to Vehicle:	The front bumper, hood, grill, right headlight, right front quarter fender, right frame rail, right front tire and rim, right upper and lower control arms, right front tire and rim, sway bar and tie rod end, right front door, right rear door, right cab corner, right rear quarter fender, right rear tire and rim, and rear bumper were damaged. The right front door had a 0.5-inch gap at the top of the door.	

 Table 7.9. Exterior Vehicle Damage for Test 617231-01-2.

7.7. OCCUPANT RISK FACTORS

Data from the accelerometers were digitized for evaluation of occupant risk, and the results are shown in Table 7.10. Figure D.7 in Appendix D.3 shows the vehicle angular displacements, and Figures D.8 through D.10 in Appendix D.4 show acceleration versus time traces.

Test Parameter	Specification ^a	Measured	Time
OIV, Longitudinal (ft/s)	≤40.0	9.6	0.1714 seconds on right side of
	30.0		interior
OIV, Lateral (ft/s)	≤40.0	12.3	0.1714 seconds on right side of
	30.0		interior
Ridedown, Longitudinal	≤20.49	6.4	0.4973 - 0.5073 seconds
(g)	15.0		
Ridedown, Lateral (g)	≤20.49	6.6	0.2640 - 0.2740 seconds
	15.0		
THIV (m/s)	N/A	4.6	0.1655 seconds on right side
			of interior
ASI	N/A	0.6	0.2719 - 0.3219 seconds
50-ms MA Longitudinal (g)	N/A	-4.0	0.4575 - 0.5075 seconds
50-ms MA Lateral (g)	N/A	-4.9	0.2529 - 0.3029 seconds
50-ms MA Vertical (g)	N/A	-2.2	1.2033 - 1.2533 seconds
Roll (deg)	≤75	10.2	1.1884 seconds
Pitch (deg)	≤75	7.0	0.8950 seconds
Yaw (deg)	N/A	43.2	0.9086 seconds

 Table 7.10. Occupant Risk Factors for Test 617231-01-2.

^{a.} Values in italics are the preferred MASH values.

7.8. TEST SUMMARY

Figure 7.11 summarizes the results of *MASH* Test 617231-01-2.

Test Agend				Test Agency	Теха	is A&M Trar	nsportation Institute (T	ГІ)		
			Test Standard/Test No. A			MAS	MASH 2016, Test 3-11			
and the state of the second		TTI Project No.			6172	617231-01-2				
					Test Date	2023-02-23				
		TEST ARTICLE								
				Type	Lona	itudinal Bar	rier			
				Name	Long	-Span Guai	rdrail			
State of Lot of		and the second second			Length	181 f	eet 3 inche	S		
C).000 s	5	Key Materials			W-beam guardrail, 72-inch wide-flange steel posts, CRT timber posts, sch. 40 ASTM A53 Grade A pipe				
-	-		Soil Type and Condition			AASI conc	AASHTO M147 grading D type 1 crushed concrete			
A La Manthereta [1]			TEST VEHICLE							
		ANTA			Type/Designation	2270	2270P			
				Year	, Make and Model	2017	RAM 1500			
		the second second			nertial Weight (lb)	5043				
Statement and a statement		the second second second			Dummy (lb)	165				
The American Street Street		and the second			Gross Static (lb)	5208				
	0.100 s	6	IMP	ACT CON	DITIONS					
		Webser .		Im	pact Speed (mi/h)	62.2	62.2			
in all all all				Ir	npact Angle (deg)	24.9	·		<u> </u>	
		all the			Impact Location	46.3	Inches upst	ream from centerline c	r post 11.	
		DAN WA		Impa	ict Seventy (kip-it)	115.0	5207028377	95		
	72.					Not N	Accounchic			
	H	and the second	Tro	iooton//Ho		Not N	Not Measurable			
			Exit Box Criteria			Vehic	Vehicle crossed the exit box a 47 ft downstream from loss of contact.			
) 200 s		Stopping Distance		182 f	182 ft downstream 8 ft to the field side				
		•	TEST ARTICLE DEFLECTIONS		0111		40			
42	No. A. S.	a day	Dynamic (inches)		64.9					
Lain Stranding P	Torona a	MARTIN	Permanent (inches)		48					
			Working Width / Height (inches) 72		72.3	72.3 / 59.4				
		PANA	VEF	VEHICLE DAMAGE						
		the state of the s	VDS		01RF	=Q3				
and the second second	1		CDC		01FREW2					
State of the second		the strength of days	Max. Ext. Deformation (inches)		12					
C).300 s	5	Max Occupant Compartment Deformation		No occupant compartment deformation					
				OCCUPA	ANT RISK VALUES	;				
Long. OIV (ft/s)	9.6	Long. Ridedown	(g)	6.4	Max 50-ms Long.	(g)	-4.0	Max Roll (deg)	10.2	
Lat. OIV (ft/s)	12.3	Lat. Ridedown (g	g)	6.6	Max 50-ms Lat. (g)	-4.9	Max Pitch (deg)	7.0	
THIV (m/s) 4.6 ASI 0.6 Max 50-ms Vert.			(g)	-2.2	Max Yaw (deg)	43.2				
B' Exit Angle Box							1 Guadral Bok, 4 B if esh Ra (pirt more Bosted, tw Woods on Post 	m Biochael for Wated Pred all x 2 Alasher 56 PS44 —22° Quadrael Bolt CRT Tenber Post for 31° rail		



Chapter 8. SUMMARY AND CONCLUSIONS

8.1. ASSESSMENT OF TEST RESULTS AND CONCLUSIONS

The crash tests reported herein were performed in accordance with *MASH* TL-3, which involves two tests on the Long-Span Guardrail with fall-protection fence.

Table 8.1 shows that the Long-Span Guardrail with fall-protection fence met the performance criteria for *MASH* TL-3 for longitudinal barriers.

Table 8.1. Assessment Summary for MASH TL-3 Tests on Long-Span Guardrail with Fall-Protection Fence.

Evaluation Criteria	Description	Test 617231-01-1	Test 617231-01-2
A	Contain, Redirect, or Controlled Stop	S	S
D	No Penetration into Occupant Compartment	S	S
F	Roll and Pitch Limit	S	S
н	OIV Threshold	S	S
I	Ridedown Threshold	S	S
Overall	Summary of Results	Pass	Pass

Note: S = Satisfactory; N/A = Not Applicable.

¹ See Table 4.2 for details

REFERENCES

- 1. AASHTO. *Manual for Assessing Safety Hardware*, Second Edition. American Association of State Highway and Transportation Officials, Washington, DC, 2016.
- Bielenberg, R.W., Faller, R.K., Rohde, J.R., Reid, J.D., Sicking, D.L., Holloway, J.C., Allison, E.M., and Polivka, K.A., *"Midwest Guardrail System for Long-Span Culvert Applications."* Research Report TRP-030187-07, Midwest Roadside Safety Facility, Lincoln, Nebraska, 2007.
APPENDIX A. DETAILS OF LONG-SPAN GUARDRAIL WITH FALL PROTECTION FENCE







57



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T:\Drafting Department\Solidworks\Standard Parts\Guardrail Parts and Subs\Guardrail Drawings\Midwest Terminal



T:\Drafting Department\Solidworks\Standard Parts\Guardrail Parts and Subs\Guardrail Drawings\Midwest Terminal





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APPENDIX B. SUPPORTING CERTIFICATION DOCUMENTS

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I D www.P65Wemings.ca.gov	10 www.P65Wamings.ca.gov	Bend Test 1 Passed		or other reprov	tuctive harm. For more information go
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Page 1 OF 1 11/09/2022 14:46:27

GMG	Rebar Road nville FL 3223.	-4100	CENTIFIED MILL IE For addition 9.3-	al copies call 266-1468	accortate and con	sions to the reported grade specificatio
AT NO.:5021242 CTTON: REBAN 16MM (#5) 2010". ADE: ASTM AG15-20 Gr 420/60 GL DATE: 07/04/2022 LT DATE: 05/29/2022 LT DATE: 05/22/2022	120/60	C C C C C C C C C C C C C C C C C C C	C Construction Svcs College Stat: 550 State Hwy 30 Tlege Station TX 7745 7950 9 774 5960	<pre>S CMC Construction Svc: H 1 10650 State Hwy 30 P College Station TX US 77845-7950 T 979 774 5900 0</pre>	ollinge Stati	try Assurance Manager Deliverry+: 85221258 BOL#: 75662294 CUST POH: 933308 CUST P/M: DLVRY LAS / HEAT: 2003.000 LB DLVRY PCS / HEAT: 96 EA
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	0.87%		Elongation Cage Lgth 1 (m Bend Te:	etri 200mm St 1 Passed		
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т.	0.335					
5	0.18%					
NA	0.08%					
MC	0.019%				The Following is tr	ue of the material represented by this MTR:
~	0.003%				Material is tully	killed and is Hot Rolled Steel
8	0.001%				- 100% movied, 10	olled, and manufactured in the USA
S	0.013%		2		-EN10204:2004 3	l. t. compliant
					Contains no welt	d repar
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TR No. 617231-01

xas A&M insportation ititute	QF 7.3-01 Samj	Concrete pling	Doc. No. QF 7 .3-01	Revision Date: 2020-0 7- 29
Form	Revised by: B.L. Griffi Approved by: D. L. Ku	th hn	Revision: 7	Page: 1 of 1
617231	Casting Date:	12/12/2022	Mix Design (psi):	4500
Terra	acon	Name of Technician Breaking Sample	Terr	acon
Terra	acon	Signature of Technician Breaking Sample	Terr	acon
Truck No.	Ticket No.	Locat	ion (from concrete	e map)
119	130396	1	00% of moment sla	ıb
Break Date	Cylinder Age	Total Load (lbs)	Break (psi)	Average
	As A&M Asportation titute Form 617231 Terr Truck No. 119 Break Date Break Date	Kas A&M sportation tituteQF 7.3-01 SamFormRevised by: B.L. Griffi Approved by: D. L. Ku617231Casting Date:TerraconTerraconTruck No.Ticket No.1191303969991303969910130396999130396991013039699913039699913039699913039699913039699913039699913039699913039699	QF 7.3-01 Concrete Sampling Form Revised by: B.L. Griffith Approved by: D. L. Kubn 617231 Casting Date: 12/12/2022 617231 Casting Date: 12/12/2022 617231 Casting Date: 12/12/2022 617231 Casting Date: 12/12/2022 Form Signature of Technician Breaking Sample Terracon Signature of Technician Breaking Truck No. Ticket No. Locat 119 130396 1 Break Date Cylinder Age Total Load (lbs) Break Date Cylinder Age Incomparison Incomparison Incomparison Incomparison <td>Kass A&M Insportation itute QF 7.3-01 Concrete Sampling Doe. No. QF 7.3-01 Form Revised by: B.L. Griftin Approved by: D. L. Kuhn Revision: 7 617231 Casting Date: 12/12/2022 Mix Design (psi): Terracon Signature of Technician Breaking Sample Terr Truck No. Ticket No. Location (from concrete Signature of Technician Breaking Break Date Cylinder Age Total Load (lbs) Break (psi) Break Date Cylinder Age Total Load (lbs) Break (psi) Image: Construct of Constr</td>	Kass A&M Insportation itute QF 7.3-01 Concrete Sampling Doe. No. QF 7.3-01 Form Revised by: B.L. Griftin Approved by: D. L. Kuhn Revision: 7 617231 Casting Date: 12/12/2022 Mix Design (psi): Terracon Signature of Technician Breaking Sample Terr Truck No. Ticket No. Location (from concrete Signature of Technician Breaking Break Date Cylinder Age Total Load (lbs) Break (psi) Break Date Cylinder Age Total Load (lbs) Break (psi) Image: Construct of Constr

REMIT PAYME P.O. BOX138 KURTEN, TX 7	27862 5222 B	Sandy Point RD. ryan, Tx 77807	17534 SH College Station	6 South n, TX 77845	18935 Circle Lake E Pinehurst, TX 7736	BCS DISPAT PINEHURST DISPAT Dr. OFF 2	130396 CH - 979-316-2906 CH - 936-232-5815 CE - 979-985-3636
RELLIS	CAMPUS, BR	VRTATIO YAN TX			HWY 21,LT S HWY 47,LT I HTALL THE W		, RT AT ENTRANCE, THE GATE
TIME	FORMULA	LOAD SIZE	YARD ORDERED		DRIVER/TRUCK		PLANT TRANSACTION#
10:23 (N94520050	6.00	6.00 P	D#	JJ	119	72252
DATE		LOAD#	YARDS DEL.	BATCH#	WATER TRIM	SLUMP	
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QUANTITY	CODE	DESCRIPTION	CALLER ALLER & LER	AND THE REAL PROPERTY.	THE CARE STREET		70341
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LEFT PLANT	ARRIVED JOB	START UNLOADING	SLUMP	CONCRETE TEMP.	AIR TEMP		
1131						Prev. AMT	
FINISH UNLOADING	LEFT JOB	ARRIVED AT PLANT	ON SITE	TESTING			1
			TESTING LAB: GES	RACON			
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						1	30396

CONCRETE COMPRESSIVE STRENGTH TEST REPORT

Report Number: A1171057.0261 Service Date: 12/12/22 Report Date: 01/24/23 Revision 1 -Task: PO# 617231

Client

Texas Transportation Institute Attn: Bill Griffith TTI Business Office 3135 TAMU College Station, TX 77843-3135

Material Information

Specified Strength: 4,500 psi @ 28 davs

Mix ID:	FN94520050	> >>> > (?	
Supplier:	Texcrete		
Batch Time:	1115	Plant:	
Truck No.:	119	Ticket No.:	72353

Field Test Data

Laboratory Test Data

Test	Result
Slump (in):	6
Air Content (%):	1.6
Concrete Temp. (F):	81
Ambient Temp. (F):	64
Plastic Unit Wt. (pcf):	147.0
Yield (Cu. Yds.):	

6198 Imperial Loop College Station, TX 77845-5765 979-846-3767 Reg No: F-3272

Project

Riverside Campus

Accumulative Yards:

Placement Method:

Sample Location:

Placement Location:

Water Added After (gal):

Riverside Campus Bryan, TX Project Number: A1171057 Sample Information 12/12/22 Sample Time: Sample Date: Sampled By: Randy Rippstein Weather Conditions:

Cloudy, Heavy Wind 6 Batch Size (cy): 6 Direct Discharge Water Added Before (gal): 10 0 Middle

2315

lerracon

North West Runway

Set No.	Spec ID	Cyl. Cond.	Avg Diam. (in)	Area (sq in)	Date Received	Date Tested	Age at Test (days)	Max Load (Ibs)	Comp Strength (psi)	Frac Type	Tested By
1	Α	Good	6.00	28.27		01/04/23	23	126,960	4,490	5	CRM
1	В	Good	6.00	28.27		01/04/23	23	131,110	4,640	5	CRM
1	С	Good	6.00	28.27		01/04/23	23	127,370	4,500	5	CRM
							Averaç	ge (23 days)	4,540		
1	D						Hold				
Initial C	ure: Out	side Plastic Li	ds	Final	Cure: Field (Cured	S	ample Descri	ption: 6-inch d	liameter cyl	inders

Comments: Note: Reported air content does not include Aggregate Correction Factor (ACF).

Specification

Samples Made By: Terracon

Services:

Obtain samples of fresh concrete at the placement locations (ASTM C 172), perform required field tests and cast, cure, and test compressive strength samples (ASTM C 31, C 39, C 1231).

Start/Stop: 1100-1300

Reviewed By:

Terracon Rep.: Randy Rippstein Reported To: Bill w/ TTI MBC Management Contractor: **Report Distribution:**

(1) Texas Transportation Institute, Bill Griffith

Test Methods: ASTM C 31, ASTM C143, ASTM C231, ASTM C1064

The tests were performed in general accordance with applicable ASTM, AASHTO, or DOT test methods. This report is exclusively for the use of the client indicated above and shall not be reproduced except in full without the written consent of our company. Test results transmitted herein are only applicable to the actual samples tested at the location(s) referenced and are not necessarily indicative of the properties of other apparently similar or identical materials.

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lexander Dunigan Project Manager

	exas A&M ransportation istitute	QF 7.3-01 Sam	Concrete pling	Doc. No. QF 7 .3-01	Revision Date: 2020-0 7- 29
Qualit	y Form	Revised by: B.L. Griffi Approved by: D. L. Ku	th hn	Revision: 7	Page: 1 of 1
Project No:	617231	Casting Date:	12/21/2022	Mix Design (psi):	4500
Name of Technician Taking Sample	Terr	acon	Name of Technician Breaking Sample	Terr	acon
Signature of Technician Taking Sample	Terr	acon	Signature of Technician Breaking Sample	Terr	acon
Load No.	Truck No.	Ticket No.	Locat	ion (from concrete	e map)
T1	Justin Hosey13	144247		100% of Deck	
Load No.	Break Date	Cylinder Age	Total Load (lbs)	Break (psi)	Average

REMIT PAYME P.O. BOX138 KURTEN, TX 7	NT TO: 7862 5222 Br	Sandy Point RD. yan, Tx 77807	TT534 SH College Station	6 South 1, TX 77845 2818, RT M 2818, RT M 4 STRAIGH	1935 Circle Lake D inehurst, TX 77362 WY 21, LT S WY 47, LT II TALL THE W	BCS DISPAT PINEHURST DISPAT r. OFFI 2 ILVER HILL NTORELLIS AY DOWN TO	144247 CH - 979-316-2906 CH - 936-232-5815 CE - 979-985-3636 , RT AT ENTRANCE, THE GATE
TIME	FORMULA	LOAD SIZE	YARD ORDERED		DRIVER/TRUCK		PLANT TRANSACTION#
10+54-7	N94520050	4	4.00 P	D#	JUSTIN	HOSEY13	72707
DATE	COLLEFT	LOAD#	YARDS DEL.	BATCH#	WATER TRIM	SLUMP	TICKET NUMBER
12/21/22	TTIRELLAND	4. 210	4.00	. Then this post	vy chims of end		70901
QUANTITY	CODE	DESCRIPTION				UNIT PRICE	EXTENDED PRICE
1.00 es	FUEL	shon, Juan son shon, Juan so borg, chullor 2 part a to aver a	Fuel	Charge	Thank you	for your	business
	ARRIVED JOB	START UNLOADING	SLUMP	CONCRETE TEMP.	AIR TEMP	Tax Prev. AM	
	LEET IOR			and the second second			1
TINGH UNEOADING	LEFT JOB	ARRIVED AT PLANT	TER TER	RACON	te sis filàna antoina P		
10	TE	STED	CME	OTHER	THING MINIT	ADDITIONAL CHARG	E1
			AIR	CYLINDERS	ding preumoto	ADDITIONAL CHARG	E 2
	WARNING		PROPERTY DA		Excessive Water	GRAND TOTAL	to Porformance
IRRITATI Contains Portland Come CONTACT MAY CAUSE Contact with Skin. In Case Water. II rittation Persists CONCRETE is a PERIGHAR PURCHASE UPON Leave ORIGINAL INSTRUCTIONED Incurred in Collecting any sum All accounts not paid within 30 annum. Not Reponsible For Made at Time Material is Deiri As25.00 Service Charge allor	NG TO THE SKIN AI N, Wear Rubber Boots ar BURNS. Avoid Contact V of Contact with Skin or Ey. Get Medical Attention, KEE Get Medical Attention, KEE Get Medical Attention, KEE State Contact Attention Attention Mars To PELEPHONED to the lower and a costs. Including lower and a costs. Including days of deliven will bear interess freed. A garegate or Color Gus ered. Ges of the Case Discounted will Bornin. will be \$100 Donne.	ND EYES Id Gloves. PROLONGED With Eyes and Prolonged es, Rinse Thoroughly With EP CHILDREN AWAY. MES THE PROPERTY of the IES or CANCELLATION of VESCOME LOADING reasonable automy's feas. It at the rate of 18% per reasonable automy's teas. It at the rate of 18% per Mity. No Calam Allowed Unless be Collected on all Returned	TO BE GIONED IF DELIVERY! Dear Customer . The driver tare and weight of the nucle the premises and/or adjace and weight of the nucle the premises and/or adjace the premises and/or adjace and/or adjacet to the premise and/or adjacet to the premise advacet of this truck and this as advacet of this truck and this as advacet of this truck and this as advacet of the sub-	TO DE MADE INSIDE CURE LUNE; of this truck in presenting this mature is of the control that the mature is of the control that the mature is of the control that the mature is of the control that the control that the control that the control that the control that the solution of the control that the solution of the control that the poly dense to help him sterove additional consoleration; the control that the control that the mature control that the control that control that the control that the control that the control that the solution of the control the contro	Hộ Ad GAL X WEIGHMASTER Surch NOTICE: MY SIGNATING B CATRING HOTCE AND SUP CATRING HOTCE	ded by Request/Authoriz	ITCS
							144247

CONCRETE COMPRESSIVE STRENGTH TEST REPORT

 Report Number:
 A1171057.0263

 Service Date:
 12/21/22

 Report Date:
 01/24/23
 Revision 1

 Task:
 PO# 617231

Client

Texas Transportation Institute Attn: Bill Griffith TTI Business Office 3135 TAMU College Station, TX 77843-3135

Material Information

Specified Strength: 4,500 psi @ 28 days

 Mix ID:
 Fn945200500

 Supplier:
 Texcrete

 Batch Time:
 1054
 Plant:
 2

 Truck No.:
 13
 Ticket No.:
 7001

Field Test Data

Test	Result
Slump (in):	5 1/2
Air Content (%):	3.7
Concrete Temp. (F):	64
Ambient Temp. (F):	44
Plastic Unit Wt. (pcf):	146.3
Yield (Cu. Yds.):	

Fierracon

6198 Imperial Loop College Station, TX 77845-5765 979-846-3767 Reg No: F-3272

Bryan, TX Project Number: A1171057 Sample Information 12/21/22 Sample Time: 1150 Sample Date: Sampled By: Brian Maass Weather Conditions: Cloudy moderate wind Accumulative Yards: 4/4 Batch Size (cy): 10 Placement Method: Direct Discharge Water Added Before (gal): 10 Water Added After (gal): 0 Sample Location: Center

Northwest barier

Laboratory Test Data

Set No.	Spec ID	Cyl. Cond.	Avg Diam. (in)	Area (sq in)	Date Received	Date Tested	Age at Test (days)	Max Load (lbs)	Comp Strength (psi)	Frac Type	Tested By
1	Α	Good	6.00	28.27		01/04/23	14 F	133,680	4,730	2	CRM
1	В	Good	6.00	28.27		01/04/23	14 F	129,480	4,580	5	CRM
1	С	Good	6.00	28.27		01/04/23	14 F	133,900	4,740	2	CRM
1	D						Hold				
Initial C	ure: Ou	tside Plastic Li	ds	Final	Cure: Field (Cured	S	ample Descri	ption: 6-inch d	iameter cyl	inders

Project

Riverside Campus

Riverside Campus

Placement Location:

Comments: F = Field Cured

Note: Reported air content does not include Aggregate Correction Factor (ACF).

Specification

Samples Made By: Terracon

Services:

Obtain samples of fresh concrete at the placement locations (ASTM C 172), perform required field tests and cast, cure, and test compressive strength samples (ASTM C 31, C 39, C 1231).

Start/Stop: 1030-1300

Reviewed By:

Terracon Rep.: Brian Maass Reported To: Contractor: MBC Management Report Distribution:

(1) Texas Transportation Institute, Bill Griffith

Test Methods: ASTM C 31, ASTM C143, ASTM C231, ASTM C1064

The tests were performed in general accordance with applicable ASTM, AASHTO, or DOT test methods. This report is exclusively for the use of the client indicated above and shall not be reproduced except in full without the written consent of our company. Test results transmitted herein are only applicable to the actual samples tested at the location(s) referenced and are not necessarily indicative of the properties of other apparently similar or identical materials.

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Nexander Dunigan Project Manager

APPENDIX C. MASH TEST 3-10 (CRASH TEST 617231-01-1)

C.1. VEHICLE PROPERTIES AND INFORMATION

Date:	2023-02-13	Test No.:	617231-01-1	VIN No.:	3N1CN7AP1KL865491
Year:	2019	Make:	Nissan	Model:	Versa







OCCUPANT COMPARTMENT DEFORMATION MEASUREMENT

	Before	After	Differ.
		(inches)	
A1	67.50	67.50	0.00
A2	67.25	67.25	0.00
A3	67.75	67.75	0.00
B1	40.50	40.50	0.00
B2	39.00	39.00	0.00
В3	40.50	40.50	0.00
B4	36.25	36.25	0.00
B5	36.00	36.00	0.00
B6	36.25	36.25	0.00
C1	26.00	26.00	0.00
C2	0.00	0.00	0.00
C3	26.00	26.00	0.00
D1	9.50	9.50	0.00
D2	0.00	0.00	0.00
D3	9.50	8.00	-1.50
E1	51.50	50.00	-1.50
E2	51.00	51.50	0.50
F	51.00	51.00	0.00
G	51.00	51.00	0.00
Н	37.50	37.50	0.00
I	37.50	37.50	0.00
J*	51.00	50.00	-1.00

*Lateral area across the cab from

driver's side kick panel to passenger's side kick panel.

Figure C.1. Vehicle Properties for Test 617231-01-1.

Date:	2023-02-13	Test No.:	617231-01-1	VIN No.:	3N1CN7AP1KL865491		
Year:	2019	– – Make:	Nissan	Model:	Versa		

VEHICLE CRUSH MEASUREMENT SHEET¹ Complete When Applicable End Damage Side Damage Undeformed end width Bowing: B1 X1 Corner shift: A1 B2 X2 A2 Bowing constant Bowing constant (check one) X1 + X2 2 < 4 inches 2 2

Note: Measure C_1 to C_6 from Driver to Passenger Side in Front or Rear Impacts – Rear to Front in Side Impacts.

~		Direct Damage									
Impact	Plane* of	Width**	Max***	Field	C1	C ₂	C ₃	C4	C_5	C_6	±D
Number	C-Measurements	(CDC)	Crush	L**							
1	AT FT BUMPER	12	10	28							14
2	ABOVE FT BUMPER	12	8	36							52
	Measurements recorded										
	🖌 inches or 🗌 mm										

¹Table taken from National Accident Sampling System (NASS).

*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

**Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

***Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

Figure C.2. Exterior Crush Measurements for Test 617231-01-1.

Date:	2023-02-13	Test No.:	617231-01-1	VIN No.:	3N1CN7AP1KL865491		
Year:	2019	Make:	Nissan	Model:	Vers	а	
	H-		D	OCCUPANT EFORMATIC	COMPARTI	MENT EMENT	
	F			Before	After (inches)	Differ.	
	G		A1	67.50	67.50	0.00	
¶\		7	∽ ∭ _ A2	67.25	67.25	0.00	
\$ <u> </u>				67.75	67.75	0.00	
			B1	40.50	40.50	0.00	
			B2	39.00	39.00	0.00	
	B1, B2,	B3, B4, B5, B6	B3	40.50	40.50	0.00	
			B4	36.25	36.25	0.00	
	A1, A2	.&A 3	В5	36.00	36.00	0.00	
	D1, D2, & D3	D1, D2, & D3 C1 C2 & C3	ве ве	36.25	36.25	0.00	
)) C1	26.00	26.00	0.00	
			C2	0.00	0.00	0.00	
			C3	26.00	26.00	0.00	
			D1	9.50	9.50	0.00	
			D2	0.00	0.00	0.00	
		D3	9.50	8.00	-1.50		
		E1	51.50	50.00	-1.50		
			E2	51.00	51.50	0.50	
			F	51.00	51.00	0.00	
			G	51.00	51.00	0.00	
		н	37.50	37.50	0.00		

*Lateral area across the cab from driver's side kick panel to passenger's side kick panel.

Figure C.3. Occupant Compartment Measurements for Test 617231-01-1.

T J* 37.50

51.00

37.50

50.00

0.00

-1.00

C.2. SEQUENTIAL PHOTOGRAPHS









(c) 0.200 s





(e) 0.400 s





(g) 0.600 s (h) 0.700 s Figure C.4. Sequential Photographs for Test 617231-01-1 (Overhead Views).



(a) 0.000 s





(e) 0.400 s

(f) 0.500 s



(g) 0.600 s (h) 0.700 s Figure C.5. Sequential Photographs for Test 617231-01-1 (Frontal Views).





(b) 0.100 s



(c) 0.200 s

(d) 0.300 s



(e) 0.400 s

(f) 0.500 s



(g) 0.600 s

(h) 0.700 s

Figure C.6. Sequential Photographs for Test 617231-01-1 (Rear Views).
C.3. VEHICLE ANGULAR DISPLACEMENTS



Roll, Pitch and Yaw Angles

Figure C.7. Vehicle Angular Displacements for Test 617231-01-1.

C.4. VEHICLE ACCELERATIONS



Figure C.8. Vehicle Longitudinal Accelerometer Trace for Test 617231-01-1 (Accelerometer Located at Center of Gravity).



Figure C.9. Vehicle Lateral Accelerometer Trace for Test 617231-01-1 (Accelerometer Located at Center of Gravity).



Figure C.10. Vehicle Vertical Accelerometer Trace for Test 617231-01-1 (Accelerometer Located at Center of Gravity).

APPENDIX D. MASH TEST 3-11 (CRASH TEST 617231-01-2)

D.1. VEHICLE PROPERTIES AND INFORMATION

Date: 2	2023-02-23	Test No.:	617231	-01-2	VIN No.:	1C6RR6	FT5HS	542672
Year:	2017	Make:	RAN	N	Model:		1500	
Tire Size:	265/70 R	17		Tire I	Inflation Pre	ssure:	35	osi
Tread Type:	Highway				Odo	meter: <u>15566</u>	5	
Note any dar	mage to the	vehicle prior to t	est: <u>None</u>	1				
● Denotes a	Icceleromet	er location			▲X —			
			<u>ا</u>	 			<u>)</u>	
NOTES: NO	one		· †		7// 7		2	
Engine Type Engine CID:	:: V-8 5.7 lite	r	A M WHEEL TRACK					WHEEL TRACK
Transmissio	n Type:	_	1		June		ERTIAL C. M.	J
Auto	or TZIRW			, ▲♀	1			
			P —					⇒ Ī
None	apment.		^	6			2	ДВ
Dummy Data Type:	a: 50th P	ercentile Male	J- I-				P	
Seat Positio	on:	di			•	— G - Е —•	▲D	•
Geometry:	inches			Ť	M FRONT		▼ M rear	
A 78	50 F	= 40.00	К	20.00	P	-c- 3.00	U	26.75
в 74	.00 (G 28.50	L	30.00	Q	30.50	V	30.25
C 227	.50 H	- 60.90	Μ	68.50	R	18.00	W	60.90
D 44	.00	11.75	N	68.00	s	13.00	Х	79.00
E <u>140</u>	.50 .	J27.00	0 <u> </u>	46.00	_ т_	77.00	-	
Wheel Ce Height F	ront	14.75 Cle	Wheel Well arance (Front)		6.00	Bottom Frame Height - Fron	e t	12.50
Wheel Ce Height F	nter Rear	14.75 Cle	Wheel Well arance (Rear)		9.25	Bottom Frame Height - Rea	e r	22.50
RANGE LIMIT : A=	=78 ±2 inches; C=2	37 ±13 inches; E=148 ±12	inches; F=39 ±3 inc	hes; G = > 28 ir	nches; H = 63 ±4 ii	nches; O=43 ±4 inches;	(M+N)/2=6	7 ±1.5 inches
GVWR Ratir	ıgs:	Mass: Ib	Curt	2	Test	Inertial	<u>Gros</u>	<u>ss Static</u>
Front	3700	Mfront	2964			2857	2857	
Back	3900	M _{rear}		2085		2186		2186
Total	6700	M _{Total}		049 (Allowable	Range for TIM and	5043 GSM = 5000 lb ±110 lb)	5043
Mass Distril	bution:	_F:1426	RF:	1431	LR:	<u>1113</u> F	R:	1073



Date:	2023-02-23	Test No.:	617231-01-2	VIN No.:	1C6RR6FT5HS542672
		=			

Year: 2017 Make: RAM Model:

1500

VEHICLE CRUSH MEASUREMENT SHEET¹

Complete Wh	en Applicable			
End Damage	Side Damage			
Undeformed end width	Bowing: B1 X1			
Corner shift: A1	B2 X2			
A2				
End shift at frame (CDC)	Bowing constant			
(check one)	$X1+X2$ _			
< 4 inches	2			
\geq 4 inches				

Note: Measure C₁ to C₆ from Driver to Passenger Side in Front or Rear Impacts – Rear to Front in Side Impacts.

a .c		Direct I	Damage								
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max**** Crush	Field L**	C ₁	C2	C3	C4	C ₅	C_6	±D
1	AT FT BUMPER	14	12	60							9
2	SAME	14	10	56							72
	Measurements recorded										
	√inches or ☐mm										

¹Table taken from National Accident Sampling System (NASS).

*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

**Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

***Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

Figure D.2. Exterior Crush Measurements for Test 617231-01-2.

Date:	2023-02-23	_ Test No.:	617231-01-2	VIN No.:	1C6RR6FT5HS542672		
Year:	2017	_ Make: _	RAM	Model:	150	0	
			T D	OCCUPANT EFORMATIO	COMPARTI N MEASUR	MENT EMENT	
	F			Before	After (inches)	Differ.	
	J E1	E2 E3	E4 A1	65.00	65.00	0.00	
			A2	63.00	63.00	0.00	
		н	1) 🗠 🛛 АЗ	65.50	65.50	0.00	
			B1	45.00	45.00	0.00	
			B2	38.00	38.00	0.00	
			ВЗ	45.00	45.00	0.00	
			B4	39.50	39.50	0.00	
		B1-3 B4	-6 B5	43.00	43.00	0.00	
6	D1-	-3	B6	39.50	39.50	0.00	
	C1-3		C1	26.00	26.00	0.00	
))		 C2	0.00	0.00	0.00	
			Ca	3 26.00	26.00	0.00	
			D1	11.00	11.00	0.00	
			D2	0.00	0.00	0.00	
		1	D3	3 11.50	11.50	0.00	
		25	E1	58.50	58.50	0.00	
	B1,4	<u> </u>	E2	63.50	63.50	0.00	
	E	1-4	E3	63.50	63.50	0.00	
			E4	63.50	63.50	0.00	
			F	59.00	59.00	0.00	
			G	59.00	59.00	0.00	

*Lateral area across the cab from driver's side kickpanel to passenger's side kickpanel.

Figure D.3. Occupant Compa	artment Measurements for Test 617231-01-2.
----------------------------	--

Н

J*

37.50

37.50

25.00

37.50

37.50

25.00

0.00

0.00

0.00

D.2. SEQUENTIAL PHOTOGRAPHS





(b) 0.100 s



(c) 0.200 s





(e) 0.400 s





(g) 0.600 s (h) 0.700 s Figure D.4. Sequential Photographs for Test 617231-01-2 (Overhead Views).



(a) 0.000 s

(b) 0.100 s



(c) 0.200 s

(d) 0.300 s



(e) 0.400 s

(f) 0.500 s



(g) 0.600 s (h) 0.700 s Figure D.5. Sequential Photographs for Test 617231-01-2 (Frontal Views).



(a) 0.000 s

(b) 0.100 s



(c) 0.200 s

(d) 0.300 s



(e) 0.400 s

(f) 0.500 s



(g) 0.600 s

(h) 0.700 s

Figure D.6. Sequential Photographs for Test 617231-01-2 (Rear Views).

D.3. VEHICLE ANGULAR DISPLACEMENTS



Roll, Pitch and Yaw Angles

Figure D.7. Vehicle Angular Displacements for Test 617231-01-2.

D.4. VEHICLE ACCELERATIONS



Figure D.8. Vehicle Longitudinal Accelerometer Trace for Test 617231-01-2 (Accelerometer Located at Center of Gravity).



Figure D.9. Vehicle Lateral Accelerometer Trace for Test 617231-01-2 (Accelerometer Located at Center of Gravity).



Figure D.10. Vehicle Vertical Accelerometer Trace for Test 617231-01-2 (Accelerometer Located at Center of Gravity).

TR No. 617231-01