

Test Report No. 617741-01-1



MASH 4-12 EVALUATION OF SINGLE SLOPE CONCRETE BRIDGE RAIL WITH FENCE SYSTEM MOUNTED ON TOP

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16. Abstract

This research was performed to develop and crash test a design of fence system mounted on top of a single slope concrete bridge rail. The design was developed using extensive finite element simulation analysis, followed by full-scale crash testing to verify the crashworthiness of the fence system mounted on top of a 36-inch tall permanent single slope concrete bridge rail. The performance of the fence and barrier system was assessed in accordance with the safetyperformance evaluation guidelines included in the second edition of the American Association of State Highway and Transportation Officials (AASHTO) *Manual for Assessing Safety Hardware* (*MASH*) (1). The crash test was performed in accordance with *MASH* Test 4-12 requirements for Test Level 4 (TL-4). This involves a 10000S single unit truck weighing 22,046 lb impacting the barrier system at an angle of 15 degrees while traveling at a speed of 56 mi/h.

This report provides details and results of the finite element analysis. It also provides the details of the fence and single slope bridge rail system, the crash tests and results, and the performance assessment of the fence and single slope bridge rail system for *MASH* Test 4-12 for longitudinal barriers.

The single slope bridge rail system with fence mounted on top met the performance criteria for *MASH* Test 4-12 for longitudinal barriers.

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MASH 4-12 Evaluation of Single Slope Concrete Bridge Rail with Fence System Mounted on Top

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The results reported herein apply only to the article tested. The full-scale crash test was performed according to TTI Proving Ground quality procedures and American Association of State Highway and Transportation Officials (AASHTO) Manual for Assessing Safety Hardware, Second Edition (*MASH*) guidelines and standards.

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	SI* (MODERN M	ETRIC) CONV	ERSION FACTORS		
	APPROXIMA	TE CONVERSIO	NS TO SI UNITS		
Symbol	When You Know	Multiply By	To Find	Symbol	
	·	LENGTH			
in	inches	25.4	millimeters	mm	
ft	feet	0.305	meters	m	
yd	yards	0.914	meters	m	
mi	miles	1.61	kilometers	km	
		AREA		2	
in ²	square inches	645.2	square millimeters	mm²	
ft ²	square feet	0.093	square meters	m²	
yd²	square yards	0.836	square meters	m²	
ac	acres	0.405	nectares	na km²	
mi-	square miles	2.59	square kilometers	Km ²	
floz	fluid ounces		milliliters	ml	
	allons	29.07	liters	1	
ft ³	cubic feet	0.028	cubic meters	∟ m ³	
vd ³	cubic vards	0.765	cubic meters	m ³	
۶a	NOTE: volumes	greater than 1000L	shall be shown in m ³		
		MASS			
oz	ounces	28.35	grams	a	
lb	pounds	0.454	kilograms	kg	
Т	short tons (2000 lb)	0.907	megagrams (or metric ton")	Mg (or "t")	
	TEMP	ERATURE (exac	t degrees)		
°F	Fahrenheit	5(F-32)/9	Celsius	°C	
		or (F-32)/1.8			
	FORCE	and PRESSURE	or STRESS		
lbf	poundforce	4.45	newtons	Ν	
lbf/in ²	poundforce per square inch	6.89	kilopascals	kPa	
	APPROXIMAT	E CONVERSION	S FROM SI UNITS		
Symbol	When You Know	Multiply By	To Find	Symbol	
		LENGTH			
mm	millimeters	0.039	inches	in	
m	meters	3.28	feet	ft .	
m	meters	1.09	yards	yd	
km	kilometers	0.621	miles	mi	
2		AREA		• 2	
mm ²	square millimeters	0.0016	square inches	IN ²	
m^2	square meters	10.764	square verde	It- vd ²	
ha	square meters	1.195	square yards	yu-	
km ²	Square kilometers	0.386	square miles	ac mi ²	
		VOLUME			
ml	milliliters	0.034	fluid ounces	07	
L	liters	0.264	gallons	dal	
m ³	cubic meters	35.314	cubic feet	ft ³	
m ³	cubic meters	1.307	cubic yards	yd ³	
		MASS			
g	grams	0.035	ounces	OZ	
kg	kilograms	2.202	pounds	lb	
Mg (or "t")	megagrams (or "metric ton")	1.103	short tons (2000lb)	Т	
	TEMP	ERATURE (exac	t degrees)		
°C	Celsius	1.8C+32	Fahrenheit	°F	
FORCE and PRESSURE or STRESS					
	FURGE				
N	newtons	0.225	poundforce	lbf	

*SI is the symbol for the International System of Units

Chapter 1. INTRODUCTION

It is sometimes desirable to install a chain link fence on top of a concrete barrier. In a past research project, Texas A&M Transportation Institute (TTI) performed crash testing of a 36-inch tall single slope median barrier with a chain link fence system installed on top (2). The posts of the fence system were installed at the centerline of the single slope median barrier. This system passed American Association of State Highway and Transportation Officials (AASHTO) *Manual for Assessing Safety Hardware's* (*MASH*) Test 4-11 with the pickup truck. However, it failed to pass Test 4-12 with the single unit truck. The posts of the fence system engaged the cab as the vehicle leaned over the barrier during redirection. This led to excessive occupant compartment deformation and protrusion of the fence posts into the occupant compartment through the windshield.

Based on the above-mentioned tests, it was concluded that the median single slope barrier with the fence installed on top is acceptable for *MASH* Test Level 3 (TL-3). However, it was not acceptable for *MASH* Test Level 4 (TL-4) due to the unsuccessful performance with the single unit truck.

While the fence system mounted on top of a median barrier failed to meet MASH TL-4, there was a possibility to design a fence system that could be mounted on a roadside concrete barrier or a bridge rail. This system could offset the fence posts away from the impact side of the barrier, thus reducing the interaction of the fence system with the single unit truck.

The objective of this project was to design and crash test a fence system mounted on top of a rigid single slope concrete bridge rail. The height of the single slope bridge rail was selected to be 36 inches. This report presents details of the design of this system using finite element (FE) simulation analysis and the evaluation of the final design through full-scale crash testing.

Details of the design and simulation analysis are presented in Chapter 2. Details of the crash testing are presented in Chapters 3 through 7. The crash test reported herein assessed the performance of the Single Slope Concrete Bridge Rail with Fence System Mounted on Top according to the safety-performance evaluation guidelines included in the AASHTO *MASH*, Second Edition (*1*). The crash test was performed in accordance with *MASH* Test 4-12 evaluation criteria.

Chapter 2. SIMULATION AND DESIGN

2.1. INTRODUCTION

As described in the previous chapter, a past MASH Test 4-12 of a fence system installed on top of a 36-inch tall single slope median barrier failed due to excessive occupant compartment deformation (2). Figure 2.1 shows the vehicle damage during and after the test. The posts of the fence system struck the cab during the test and penetrated the front windshield as the vehicle passed. The measured maximum occupant compartment deformation was 10.0 inches at the midpoint of the collapsed left A-pillar.



Figure 2.1. Vehicle Damage during and after Test No. 613131-03-2.

In this research project, the research team developed a design of a new fence system that can be installed on a roadside rigid single slope concrete barrier or a bridge rail. The research team first developed an FE model of the previously failed fence system (Figure 2.1) and performed impact simulation to evaluate the validation of the model. The researchers made several improvements to the vehicle and fence models to get better correlation with the failed test of the fence installed on the median barrier. The researchers then developed a model of the roadside fence system concept using the same fence and barrier modeling techniques to have greater confidence in the capability of the model to predict the crash performance of the fence and barrier system with the single unit truck model. The researchers used the simulation analysis to improve the design and made design recommendations for full scale crash testing. Details of the modeling and simulation are presented next.

2.2. FINITE ELEMENT MODEL VALIDATION

Prior to designing a new system, the FE model was calibrated and improved to achieve a more realistic estimation. To calibrate the FE model, it was set up with the same conditions as the full-scale crash test conducted by TTI (Test No. 613131-03-2). Simulation results were compared to the test results and changes to the models were made to enhance the accuracy of the FE model.

2.2.1. Fence Mounted on Top of the Single Slope Concrete Median Barrier

Figure 2.2 shows the fence system mounted on top of the single-slope concrete median barrier (CMB) installed for Test No. 613131-03-2.



Figure 2.2. Fence System Mounted on Top of CMB for Test No. 613131-01-2.

Key design details of the tested system are shown in Figure 2.3. The installation consisted of a 72-inch tall, 2-inch mesh chain link fence mounted on top of 36-inch-tall single-slope concrete barrier. The slope of the barrier was 10.8 degrees. The length of the barrier system was 120 ft and total length of the fence system was 103 ft-³/₄ inches. The barrier was 10 inches wide at the top. Further details of this system can be found in the full crash test report (2).



Figure 2.3. Details of Fence System Mounted on Top of CMB and Test Setup.

2.2.2. Test 4-12 Simulation with Fence System Mounted on Top of CMB

Figure 2.4 shows an overview of the FE model representing the fence mounted on top of CMB tested by TTI. The ground and CMB were modeled with a rigid material since no significant damage was observed in the test. Steel posts and chain link fence were modeled with deformable materials with elastic-plastic material properties.



(b) Closeup Model

Figure 2.4. FE Model of the Previously Tested Median Barrier Design.

In the full-scale test, the 2012 International 4300 single-unit truck (SUT) was used. The simulation model of the SUT was based on a 1996 Ford F800. To incorporate the actual test impact conditions, the test impact velocity of 55.91 mi/h and the test impact angle of 15 degrees were used in the impact simulation. Several improvements were made to the vehicle model and the chain link fence model to capture the failure modes observed in the crash testing. Figure 2.5 shows sequential images comparing the behavior of the improved simulation model to the crash test results.

In both the test and FE simulation, the post of the fence interacted with the cab and the box of the vehicle. In the simulation results, the posts struck the cab of the vehicle in a manner similar to what was observed in the crash test. The vehicle in the simulation had more pitch compared to the test vehicle, but the key mode of failure in the crash test, i.e., the fence posts striking the cab to cause excessive occupant compartment deformation, was captured with the simulation model. The model was thus considered suitable for further use in the project to evaluate the modified fence design and determine if it would reduce the fence posts-to-cab interaction.































Figure 2.5. Comparison of the FE Simulation with Crash Test of Fence Installed at the Center of the Barrier's Top.

2.3. DEVELOPMENT AND EVALUATION OF NEW FENCE DESIGN ON CONCRETE BRIDGE RAIL

To prevent the fence posts from striking the cab and causing excessive occupant compartment deformation, the research team attached the fence posts to the field side of the concrete bridge rail, and further offset them away from the impact side by bending them at the bottom. The posts were bent back toward the impact side at the top of the fence, resulting in a shallow U-shape posts. Adjacent fence posts were connected at the top using a horizontal pipe that helped in moving the posts further away from the vehicle's cab as the box of the single unit truck impacted the horizontal pipe. The FE model of this design concept is shown in Figure 2.6. This design was based on a previously developed concept of a fence system that prevented motorcyclists from interacting with the fence posts during motorcycle impacts (*3*).

The chain link fence was attached to the front of bent posts by attaching it the top and bottom horizontal pipes. The horizontal pipes were attached to the fence posts using steel bracket plates and U-bolts as shown in Figure 2.6. The fence posts were attached to the back of the concrete bridge rail using a bent bracket and epoxy anchor bolts. In the FE model, each steel component was modeled with their corresponding elastic-plastic material properties, while the concrete barrier was modeled as rigid. The chain link fence model was based on previously developed model with further improvements to allow material failure due to excessive plastic strain (*3*).

The researchers performed *MASH* Test 4-12 impact simulations with the fence and bridge rail system. The vehicle impacted the barrier at a speed and angle of 56 mi/h and 15 degrees, respectively. The sequential images from the simulation are shown in Figure 2.7.



Figure 2.6. FE Model of the Offset Fence System Design Mounted on Concrete Bridge Rail.







0.2 s

0.4 s



0.10 s



0.3 s



0.5 s







The vehicle damage was significantly reduced with the offset posts of the new fence design. The posts did not strike the cab or the A-pillar of the single unit truck during the impact. A comparison of the design improvement with the offset posts is shown in Figure 2.8. Since the primary mode of failure in Test 6136131-03-2 was the excessive occupant compartment deformation due to the fence posts striking the cab and the vehicle's A-pillar, the mitigation of these issues in the offset-post design simulation indicated a reasonable probability of the design to meet MASH Test 4-12 criteria. The researchers thus recommended performing this test to verify simulation results and the performance of the fence and the barrier system.

During the design review phase after the initial design, the chain link fence was moved laterally to attach to the fence posts. This was considered an improvement of the design that would provide better support for the fence as opposed to being supported just at the top and bottom. Details of the crash tested system and full scale crash testing results are presented in the following chapters.



Failed Test 613131-03-2



Simulation of Test 613131-03-2



Simulation of New Roadside Design

Figure 2.8. Comparison of Fence Post Interaction.

Chapter 3. SYSTEM DETAILS

3.1. TEST ARTICLE AND INSTALLATION DETAILS

The installation consisted of a 128 foot long fence system mounted on a 130 foot long single-slope concrete bridge rail. The bridge rail was 36 inches tall, 7.5 inches wide on the top, and 13 inches wide at the bottom. The sloped face of the bridge rail was on the impact side. The fence system was attached to the non-impact side of the bridge rail and extended 9 feet 5 inches above the top of the concrete bridge rail. The main portion of the fence mesh was chain link fabric mounted to fence posts that were spaced at 96 inches center to center. Near the top of the concrete bridge rail, the fence posts were offset toward the field side. At top of the fence posts, the post pipes were bent toward the impact side and connected to adjacent fence posts by a series of longitudinal pipes that were spliced together. A welded wire mesh panel was attached to the bent fence posts to cover the gap between the top of the concrete bridge rail and the chain link fence.

Figure 3.1 presents the overall information on the Fence System Mounted to Concrete Bridge Rail, and Figure 3.2 thru Figure 3.7 provide photographs of the installation. Appendix A provides further details on the fence and bridge rail system. Drawings of the test installation were developed by the Texas A&M Transportation Institute (TTI) Proving Ground, and construction was performed by TTI Proving Ground personnel.

The concrete bridge rail used in this test was also used for another crash test that involved constructing a steel-reinforced concrete mounting block on the non-impact side of the single slope bridge rail at one of the locations. It is noted that this mounting block was not incorporated in the concrete bridge rail design for the purposes of evaluating the performance of the Fence System Mounted to the Concrete Bridge Rail.

3.2. DESIGN MODIFICATIONS DURING TESTS

No modifications were made to the installation during the testing phase.



Figure 3.1. Details of Fence System Mounted to Concrete Bridge Rail.



Figure 3.2. Fence System Mounted to Concrete Bridge Rail Prior to Testing.



Figure 3.3. In-Line View of the Fence System Mounted to Concrete Bridge Rail Prior to Testing.



Figure 3.4. Elevation View of the Fence System Mounted to Concrete Bridge Rail at Impact Prior to Testing.



Figure 3.5. Fence System Mounted to Concrete Bridge Rail Mesh Detail Prior to Testing.



Figure 3.6. Field Side of the Fence System Mounted to Concrete Bridge Rail Prior to Testing.



Figure 3.7. Field Side Fence Post Attachment to Concrete Bridge Rail Prior to Testing.

3.3. MATERIAL SPECIFICATIONS

Appendix B provides material certification documents for the materials used to install/construct the Fence System Mounted to Concrete Bridge Rail. Table 3.1 shows the average compressive strengths of the concrete.

Location	Design Strength	Avg. Strength	Age	Detailed Location
Foundation Wall	4000 psi	4447 psi	17 days	Downstream 100 feet of the foundation wall.
Deck	4000 psi	4297 psi	17 days	Downstream 100 feet of the deck.
Deck and Foundation Wall	4000 psi	3953 psi	17 days	Remainder of deck and foundation wall.
Single Slope Bridge Rail and Mounting Block	3600 psi	3363 psi	7 days	A complete 40-foot section of the bridge rail was poured starting at the upstream end of the rail, then 50 percent of the bridge rail was poured over the next 70 feet. This section included the mounting block.
Bridge Rail and Mounting Block	3600 psi	3667 psi	7 days	The remaining half of the 70-foot section of bridge rail from the previous pour, including the mounting block, and 100 percent of the last 20 feet of the barrier on the downstream end.

Table 3.1. Concrete Strength^a.

^a The concrete barrier used was repurposed from a previous crash test (Project 440863-01-3), and the mounting block referred to was not used for this test. The strengths and ages represent the values from the day of the crash test for the prior project on 2023-06-22.

Chapter 4. TEST REQUIREMENTS AND EVALUATION CRITERIA

4.1. CRASH TEST PERFORMED

Table 4.1 shows the test conditions and evaluation criteria for *MASH* Test 4-12 for a longitudinal barrier. The target critical impact point (CIP) for the test was determined using the information provided in *MASH* Section 2.2.1 and Section 2.3.2 Figure 4.1 shows the target CIP for *MASH* Test 4-12 on the Fence System Mounted to Concrete Bridge Rail.

Table 4.1. Test Conditions and Evaluation Criteria Specified for MASH Test 4-12 for Longitudinal Barriers.

	Test Designation	Test Vehicle	Impact Speed	Impact Angle	E	valuation Cr	riteria	
	4-12	10000S	56 mi/h	15°		A, D, G		
1	2	3 4	Ļ .	5	6	7	8	
-A	î	anna de la company de la company	_	Ŷ	Ω.	Ω	n na star star star star star star star sta	
	15°			60"[5.0	ft]			

Figure 4.1. Target CIP for *MASH* Test 4-12 on Fence System Mounted to Concrete Bridge Rail.

The crash test and data analysis procedures were in accordance with guidelines presented in *MASH*. Chapter 5 presents brief descriptions of these procedures.

4.2. EVALUATION CRITERIA

The appropriate safety evaluation criteria from Tables 2-2 and 5-1 of *MASH* were used to evaluate the crash test reported herein. Table 4.1 lists the test conditions and evaluation criteria required for *MASH* Test 4-12, and Table 4.2 provides detailed information on the evaluation criteria.

Evaluation Factors	Evaluation Criteria
Α.	Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.
D.	Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present undue hazard to other traffic, pedestrians, or personnel in a work zone. Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of <i>MASH</i> .
G.	It is preferable, although not essential, that the vehicle remain upright during and after the collision.

 Table 4.2. Evaluation Criteria Required for MASH Test 4-12.

Chapter 5. TEST CONDITIONS

5.1. TEST FACILITY

The full-scale crash test reported herein was performed at the TTI Proving Ground, an International Standards Organization (ISO)/International Electrotechnical Commission (IEC) 17025-accredited laboratory with American Association for Laboratory Accreditation (A2LA) Mechanical Testing Certificate 2821.01. The full-scale crash test was performed according to TTI Proving Ground quality procedures, as well as *MASH* guidelines and standards.

The test facilities of the TTI Proving Ground are located on The Texas A&M University System RELLIS Campus, which consists of a 2000-acre complex of research and training facilities situated 10 mi northwest of the flagship campus of Texas A&M University. The site, formerly a United States Army Air Corps base, has large expanses of concrete runways and parking aprons well suited for experimental research and testing in the areas of vehicle performance and handling, vehicle-roadway interaction, highway pavement durability and efficacy, and roadside safety hardware and perimeter protective device evaluation. The sites selected for construction and testing are along the edge of an out-of-service apron/runway. The apron/runway consists of an unreinforced jointed-concrete pavement in 12.5-ft × 15-ft blocks nominally 6 inches deep. The aprons were built in 1942, and the joints have some displacement but are otherwise flat and level.

5.2. VEHICLE TOW AND GUIDANCE SYSTEM

The 10000S vehicle was towed into the test installation using a steel cable guidance and reverse tow system. A steel cable for guiding the test vehicle was tensioned along the path, anchored at each end, and threaded through an attachment to the front wheel of the test vehicle. An additional steel cable was connected to the test vehicle, passed around a pulley near the impact point and through a pulley on the tow vehicle, and then anchored to the ground such that the tow vehicle moved away from the test site. A 2:1 speed ratio between the test and tow vehicle existed with this system. Just prior to impact with the installation, the test vehicle was released and ran unrestrained. The vehicle remained freewheeling (i.e., no steering or braking inputs) until it cleared the immediate area of the test site.

5.3. DATA ACQUISITION SYSTEMS

5.3.1. Vehicle Instrumentation and Data Processing

The test vehicle was instrumented with a self-contained onboard data acquisition system. The signal conditioning and acquisition system is a multi-channel data acquisition system (DAS) produced by Diversified Technical Systems Inc. The accelerometers, which measure the x, y, and z axis of vehicle acceleration, are strain gauge type with linear millivolt output proportional to acceleration. Angular rate sensors,

measuring vehicle roll, pitch, and yaw rates, are ultra-small, solid-state units designed for crash test service. The data acquisition hardware and software conform to the latest SAE J211, Instrumentation for Impact Test. Each of the channels is capable of providing precision amplification, scaling, and filtering based on transducer specifications and calibrations. During the test, data are recorded from each channel at a rate of 10,000 samples per second with a resolution of one part in 65,536. Once data are recorded, internal batteries back these up inside the unit in case the primary battery cable is severed. Initial contact of the pressure switch on the vehicle bumper provides a time zero mark and initiates the recording process. After each test, the data are downloaded from the DAS unit into a laptop computer at the test site. The Test Risk Assessment Program (TRAP) software then processes the raw data to produce detailed reports of the test results.

Each DAS is returned to the factory annually for complete recalibration and to ensure that all instrumentation used in the vehicle conforms to the specifications outlined by SAE J211. All accelerometers are calibrated annually by means of an ENDEVCO® 2901 precision primary vibration standard. This standard and its support instruments are checked annually and receive a National Institute of Standards Technology (NIST) traceable calibration. The rate transducers used in the data acquisition system receive calibration via a Genisco Rate-of-Turn table. The subsystems of each data channel are also evaluated annually, using instruments with current NIST traceability, and the results are factored into the accuracy of the total data channel per SAE J211. Calibrations and evaluations are also made anytime data are suspect. Acceleration data are measured with an expanded uncertainty of ± 1.7 percent at a confidence factor of 95 percent (k = 2).

TRAP uses the DAS-captured data to compute the occupant/compartment impact velocities, time of occupant/compartment impact after vehicle impact, and highest 10-millisecond (ms) average ridedown acceleration. TRAP calculates change in vehicle velocity at the end of a given impulse period. In addition, maximum average accelerations over 50-ms intervals in each of the three directions are computed. For reporting purposes, the data from the vehicle-mounted accelerometers are filtered with an SAE Class 180-Hz low-pass digital filter, and acceleration versus time curves for the longitudinal, lateral, and vertical directions are plotted using TRAP.

TRAP uses the data from the yaw, pitch, and roll rate transducers to compute angular displacement in degrees at 0.0001-s intervals, and then plots yaw, pitch, and roll versus time. These displacements are in reference to the vehicle-fixed coordinate system with the initial position and orientation being initial impact. Rate of rotation data is measured with an expanded uncertainty of ± 0.7 percent at a confidence factor of 95 percent (k = 2).

5.3.2. Anthropomorphic Dummy Instrumentation

MASH does not recommend or require use of a dummy in the 10000S vehicle, and no dummy was placed in the vehicle.

5.3.3. Photographic Instrumentation Data Processing

Photographic coverage of the test included three digital high-speed cameras:

- One placed overhead with a field of view perpendicular to the ground and directly over the impact point.
- One placed with a field of view parallel to and aligned with the installation at the downstream end.
- One placed at an oblique angle upstream from the installation on the field side.

A flashbulb on the impacting vehicle was activated by a pressure-sensitive tape switch to indicate the instant of contact with the Fence System Mounted to Concrete Bridge Rail. The flashbulb was visible from each camera. The video files from these digital high-speed cameras were analyzed to observe phenomena occurring during the collision and to obtain time-event, displacement, and angular data. A digital camera recorded and documented conditions of each test vehicle and the installation before and after the test.
Chapter 6. MASH TEST 4-12 (CRASH TEST 617741-01-1)

6.1. TEST DESIGNATION AND ACTUAL IMPACT CONDITIONS

See Table 6.1 for details on *MASH* impact conditions for this test, and Table 6.2 for the exit parameters. Figure 6.1 and Figure 6.2 depict the target impact setup.

Test Parameter	Specification	Tolerance	Measured
Impact Speed	56 mi/h	±2.5 mi/h	58.2 mi/h
Impact Angle	15°	±1.5°	15.1°
Impact Severity	142 kip-ft	≥142 kip-ft	170.7 kip-ft
Impact Location	5 feet upstream from the centerline of fence post 5.	±12 inches	5 feet 1.9 inches upstream from the centerline of post 5.

Table 6.1. Impact Conditions for MASH TEST 4-12, Crash Test 617741-01-1.

Table 6.2. Exit Parameters for MASH TEST 4-12, Crash Test 617741-01-1.

Exit Parameter	Measured
Speed	The vehicle exited along the fence and barrier. Measurements could not be taken.
Trajectory	The vehicle exited along the fence and barrier. Measurements could not be taken.
Heading	The vehicle exited along the fence and barrier. Measurements could not be taken.
Brakes applied post impact	2.3 seconds
Vehicle at rest position	237 ft downstream of impact point.31 ft to the field side.Vehicle positioned 85° left relative to the installation.
Comments:	The vehicle remained upright and stable.



Figure 6.1. Fence System Mounted to Concrete Bridge Rail/Test Vehicle Geometrics for Test 617741-01-1.



Figure 6.2. Fence System Mounted to Concrete Bridge Rail/Test Vehicle Impact Location 617741-01-1.

6.2. WEATHER CONDITIONS

Table 6.3 provides the weather conditions for 617741-01-1.

Date of Test	2023-11-17
Wind Speed	7 mi/h
Wind Direction	194°
Temperature	65 °F
Relative Humidity	74 %
Vehicle Traveling	335°

6.3. TEST VEHICLE

Figure 6.3, Figure 6.4, and Figure 6.5 show the 2013 International Maxx Force truck used for the crash test. Table 6.4 shows the vehicle measurements. Figure C.1 in Appendix C.1 gives additional dimensions and information on the vehicle.



Figure 6.3. Impact Side of Test Vehicle before Test 617741-01-1.



Figure 6.4. Opposite Impact Side of Test Vehicle before Test 617741-01-1.



Figure 6.5. Interior of Test Vehicle before Test 617741-01-1.

Test Parameter	Specification	Tolerance	Measured
Curb Weight	13,200 lb	±2200 lb	13,480 lb
Vehicle Inertial Weight	22,046 lb	±660 lb	22,220 lb
Wheelbase	240 inches	≤240 inches	207 inches
Overall Length	394 inches	≤394 inches	329.5 inches
Cargo Bed Height ⁱ	49 inches	≤2 inches	50 inches
CG of Ballast above Ground ^e	63 inches	≤2 inches	62.5 inches

Table 6.4. Vehicle Measurements for Test 617741-01-1.

Note: N/A = not applicable; CG = center of gravity.

i – Without Ballast

e - See section 4.2.1.2 in MASH for recommended ballasting procedures

6.4. TEST DESCRIPTION

Table 6.5 lists events that occurred during Test 617741-01-1. Figures C.2, C.3, and C.4 in Appendix C.2 present sequential photographs during the test.

Time (s)	Events
0.000 s	Vehicle impacted the installation
0.034 s	Vehicle began to redirect
0.242 s	Vehicle was parallel with the installation
0.145 s	Drivers side, front corner of box contacted the top rail
0.156 s	Post 5 began to lean toward the field side
0.184 s	Post 6 began to lean toward the field side
0.278 s	Top pipe between posts 6 and 7 broke, and began to bend to field side
0.352 s	Box on the vehicle began to break up
0.643 s	A section of the top pipe began to penetrate through the rear roll-up door of the vehicle from the inside of the box.
0.700 s	Vehicle reached its maximum roll
0.820 s	The top pipe section that penetrated the rear door exits the vehicle
1.608 s	Vehicle lost contact with the installation.

Table 6.5. Events during Test 617741-01-1.

6.5. DAMAGE TO TEST INSTALLATION

The concrete barrier was gouged and scuffed at impact. The top pipe bracket was broken at post 5, and a lower post bracket was broken at posts 7 and 9. The lower wire mesh panel was loose from posts 5 through 8, and the chain link mesh fabric was damaged from posts 5 through 13. Posts 6 through 9 were leaning downstream, with post 9 leaning towards the traffic side as well. The top pipe released from posts 6 through 10 and post 12, with the pipe missing from posts 6 through 9. They landed on the field side and were severely deformed.

Table 6.6 describes the deflection and working width of the Fence System Mounted to Concrete Bridge Rail. Figure 6.6 and Figure 6.7 show the damage to the Fence System Mounted to Concrete Bridge Rail.

Table 6.6. Deflection and Working Width of the Fence System Mounted toConcrete Bridge Rail for Test 617741-01-1.

Test Parameter	Measured
Permanent Deflection/Location	None
Dynamic Deflection	None
Working Width ^a and Height	89.7 inches, at a height of 97.5 inches, at the top pipe between posts 6 and 7.

^a Per *MASH*, "The working width is the maximum dynamic lateral position of any major part of the system or vehicle. These measurements are all relative to the pre-impact traffic face of the test article." In other words, working width is the total barrier width plus the maximum dynamic intrusion of any portion of the barrier or test vehicle past the field side edge of the barrier.



Figure 6.6. Fence System Mounted to Concrete Bridge Rail at Impact Location after Test 617741-01-1.



Figure 6.7. Fence System Mounted to Concrete Bridge Rail at the Point of Maximum Damage after Test 617741-01-1.

6.6. DAMAGE TO TEST VEHICLE

Figure 6.8 and Figure 6.9 show the damage sustained by the vehicle. Figure 6.10 and Figure 6.11 show the interior of the test vehicle. Table 6.7 and Table 6.8 provide details on the occupant compartment deformation and exterior vehicle damage.



Figure 6.8. Impact Side of Test Vehicle after Test 617741-01-1.



Figure 6.9. Rear Impact Side of Test Vehicle after Test 617741-01-1.



Figure 6.10. Overall Interior of Test Vehicle after Test 617741-01-1.



Figure 6.11. Interior of Test Vehicle on Impact Side after Test 617741-01-1.

	Table 6.7. Occu	pant Compartmen	t Deformation fo	or Test 617741-01-1.
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Test Parameter	Specification	Measured
Roof	≤4.0 inches	0 inches
Windshield	≤3.0 inches	0 inches
A and B Pillars	≤5.0 overall/≤3.0 inches lateral	0 inches
Foot Well/Toe Pan	≤9.0 inches	0 inches
Floor Pan/Transmission Tunnel	≤12.0 inches	7 inches
Side Front Panel	≤12.0 inches	0 inches
Front Door (above Seat)	≤9.0 inches	0 inches
Front Door (below Seat)	≤12.0 inches	0 inches

Table 6.8. Exterior Vehicle Damage for Test 617741-01-1.

Side Windows	The side windows remained intact
Maximum Exterior Deformation	16 inches in the front plane at the left corner at bumper height
VDS	11LFQ4
CDC	11FLAW3
Fuel Tank Damage	None
Description of Damage to Vehicle:	The front bumper, hood, and left fender were damaged. The front left tire was ripped off, and the wheel bent. The steering control arm was broken. The left side mirror was ripped off, and the left door, side steps, and air tanks were dented. The left side of the box was heavily damaged, and the roll-up door was removed. The left rear wheel was bent, and the tire was punctured.

6.7. OCCUPANT RISK FACTORS

Data from the accelerometers were digitized for evaluation of occupant risk and the results are shown in Table 6.9. Figure C.5 in Appendix C.3 shows the vehicle angular displacements, and Figures C.6 through C.8 in Appendix C.4 show acceleration versus time traces.

Test Parameter	Measured	Time
OIV, Longitudinal	6.2 ft/s	0.1786 seconds on left side of interior
OIV, Lateral	11.5 ft/s	0.1786 seconds on left side of interior
Ridedown, Longitudinal	3.9 g	0.2847 - 0.2947 seconds
Ridedown, Lateral	8.4 g	0.3081 - 0.3181 seconds
Theoretical Head Impact Velocity (THIV)	4.1 m/s	0.1729 seconds on left side of interior
Acceleration Severity Index	0.7	0.3170 - 0.3670 seconds
50-ms Moving Avg. Accelerations (MA) Longitudinal	-2 g	0.0085 - 0.0585 seconds
50-ms MA Lateral	5.8 g	0.2875 - 0.3375 seconds
50-ms MA Vertical	-2.9 g	0.0411 - 0.0911 seconds
Roll	29.8°	0.6442 seconds
Pitch	5.8°	0.8189 seconds
Yaw	15.5	0.8026 seconds

Table 6.9. Occupant Risk Factors for Test 617741-01-1.

6.8. TEST SUMMARY

Figure 6.11 summarizes the results of MASH Test 617741-01-1.



$\frac{1}{1}$	0.000 s		0.200 s	0.400	S	0.60	0 s
-	GENERAL INFORMATION			EXIT CONDITIONS			
	Test Agency	Texas A&M	Transportation Institute (TTI)	Exit Speed		Along Fence and Barrie	er
	Test Standard/Test No.	MASH 2016	, Test 4-12	Trajectory/Heading Angl	е	Along Fence and Barrie	er
	TTI Project No.	617741-01- ⁻	I	Stopping Distance		237 ft downstream 31 ft to the field side	
	Test Date	2023-11-17					
	TEST ARTICLE			TEST ARTICLE DEFLE	CTIONS		
	Туре	Longitudinal	Barrier	Dynamic		None	
	Name	Fence Syste	em Mounted to Concrete Bridge Rail	Permanent		None	
	Length	130 feet		Working Width / Height		89.7 inches / 97.5 inche	es
	Soil Type and Condition	Concrete, da	amp	VEHICLE DAMAGE			
(1)	Key Materials	3-inch. Sch. Panel, Conc	40 Pipe, 1.25 sch. 40 Pipe, Chain Link Fabric, Wire rete Barrier	VDS		11LFQ4	
4	TEST VEHICLE			CDC		11FLAW3	
	Type/Designation	10000S		Max. Ext. Deformation		16 inches	
	Year, Make and Model	2013 Interna	ational Maxx Force	Max Occupant Compart	ment Deformation	7 inches in the floor par	n/transmission tunnel
	Curb Weight	13,480 lb		OCCUPANT RISK VAL	UES		
	Inertial Weight	22,220 lb		Long. OIV	6.2 ft/s	Max 50-ms Long.	-2 g
				Lat. OIV	11.5 ft/s	Max 50-ms Lat.	5.8 g
	IMPACT CONDITIONS			Long. Ridedown	3.9 g	Max 50-ms Vert.	-2.9 g
	Impact Speed / Impact Angle	58.2 mi/h / 1	5.1°	Lat. Ridedown	8.4 g	Max Roll	29.8°
	Impact Location	5 feet 1.9 in	ches upstream from centerline of post 5.	THIV	4.1 m/s	Max Pitch	5.8°
	Impact Severity	170.7 kip-ft		ASI	0.7	Max Yaw	15.5°
2024-06-20	Impact Angle	— 12.3' — Post 5	237'		9'-5" Chain Link 36" 0" 🔶	Fabric	

Figure 6.12. Summary of Results for *MASH* Test 4-12 on Fence System Mounted to Concrete Bridge Rail.

Chapter 7. SUMMARY AND CONCLUSIONS

7.1. ASSESSMENT OF TEST RESULTS AND CONCLUSIONS

The crash test reported herein was performed in accordance with the evaluation criteria for *MASH* Test 4-12 on the Fence System Mounted to Concrete Bridge Rail.

Table 7.1 shows that the Fence System Mounted to Concrete Bridge Rail met the performance criteria for *MASH* Test 4-12 for longitudinal barriers.

Table 7.1. Assessment Summary for MASH Test 4-12 on Fence System Mountedto Concrete Bridge Rail.

Evaluation Criteria	Description	Test 617741-01-1
A	Contain, Redirect, or Controlled Stop	S
D	No Penetration into Occupant Compartment	S
G	Rolling is acceptable	S
Overall	Evaluation	Pass

Note: S = Satisfactory

¹ See Error! Reference source not found. for details

7.2. IMPLEMENTATION*

MASH TL-4 evaluation criteria requires performing Test 4-10 (with 1100C small car) and Test 4-11 (with 2270P pickup truck) in addition to Test 4-12. Only Test 4-12 was performed for the fence and single slope bridge rail system under this project. Tests 4-10 and 4-11 were not performed since they are not critical tests for this system.

Test 4-11 with the 2270P pickup was performed for the fence system mounted on top of the median single slope barrier, as discussed in Chapter 1. In this test, the fence posts were located at the centerline of the single slope barrier, much closer than the offset posts tested in this new research. Since the pickup truck test passed successfully with the posts installed at the centerline of the barrier, it is expected to also pass with the fence posts installed at an offset away from the traffic side of the barrier.

^{*} The opinions/interpretations identified/expressed in this section of the report are outside the scope of TTI Proving Ground's A2LA Accreditation.

MASH Test 4-10 with a lighter 1100C small car is not likely to impart greater load into the barrier or climb high enough to interact significantly with the offset fence system. Furthermore, based on the performance of the single slope barrier in past testing, this test is not considered critical. As an example, Whitesel et al. preformed a MASH Test 3-10 (same conditions and criteria as MASH Test 4-10) on a permanent single slope barrier which passed the MASH testing criteria (*4*).

Based on the discussion above, the newly designed fence system mounted on a concrete bridge rail or a roadside concrete barrier can be considered MASH TL-4 compliant and are ready for field implementation.

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- 3. C. S. Dobrovolny, S. Shi, J. C. Kover, R. P. Bligh, D. L. Kuhn, and B. L. Griffith, *"Development and Evaluation of Concrete Barrier Containment Options for Errant Motorcycle Riders."* Report No. 0-6968-R6, Texas A&M Transportation Institute, College Station, Texas, 2019.
- D. Whitesel, J. Jewell, and R. Meline, *Compliance Crash Testing of the Type 60 Median Barrier*, Test 140MASH3C16-04. Research Report FHWA/CA17-2654, Roadside Safety Research Group, California Department of Transportation, Sacramento, CA, May 2018.

APPENDIX A. DETAILS OF FENCE SYSTEM MOUNTED TO CONCRETE BRIDGE RAIL



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APPENDIX B. SUPPORTING CERTIFICATION DOCUMENTS

 FOR
 TEXAS A&M TRANSPORTATION INST

 PB INVOICE
 166890

 CUSTOMER PO
 617741

 EST. SHIP DATE
 9/26/2023

Certificate of Conformance

We certify that the following items were manufactured and tested in accordance with the chemical, mechanical, dimensional and thread fit requirements of the specifications referenced.

Products

• ASTM A193 GRADE B7 ALL THREAD ROD

Coatings

ITEMS HOT-DIP GALVANIZED PER ASTM F2329

Other

ALL ITEMS MELTED & MANUFACTURED IN THE USA

Certification Department Quality Assurance Dane McKinnon

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Test Results			······						
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Macro K	Macro C	J1	J2	J3	J4	J5	36	J7	J8
1	1	57	57	57	57	57	54	52	50
10 12	J10	J12	J14	J16	J18	J20	J24	J28	J32
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Description	Tens	ile Strength (ksi)	Yield Strength (ksi)	Fiondation (4D)	(%) DOA (%)	NI - 4-
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		132	119	20	64	
		134	113	26	66	
		133	112	28	65	
		134	116	27	63	
		133	119	29	59	
		133	114	28	65	
		132	119	28	65	
		134	113	33	63	
		133	115	20	64	
		133	119	19	65	
		132	121	24	62	
		136	114	23	61	
		132	118	24	63	
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		29	29	30	HRC	
		29	27	29	HBC	
		31	29	30	HRC	
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		29	28	29	HRC	
		30	29	31	HRC	
		29	28	29	HRC	
		30	29	30	HRC	
		30	30	29	HRC	
		29	29	30	HRC	
		2¥ 20	28	29	HRC	
		3U 20	30	30	HRC	
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est No: 70156	Test; Carb/ D	ecarb Test	29	30	HRC	
Descri	ption	Surface	Carb.	Portial Conference	h	
		Pa	55	Partial Surface Dec	arb.	Note
		1 0		Pass		

		PO 63070		
Uaican THREADED PRODUCTS, INC.	Vulcan Threaded Produc 10 Cross Creek Trail Pelham, AL 35124 Tel (205) 620-5100 Fax (205) 620-5150	INV 088576 ^{⊐ts} 48 1/2" X 144" B7 SEPT 6, 2023 30F3	JOB MATERIAL CERT	IFICATION
Job No: 74	16048	Job Informati	on Certified Date: 4/7/22	2
Containers: S	19810426 \$19816097			
Material was manufactured, teste product standard and in accordan Management System registered J Vulcan Steel Products lab is ISO ' and Rockwell hardness, Charpy i Material was tested in accordanc F606, and F3228 test methods	d, and inspected as requin ce with Vulcans ISO 9001 une 30th, 2017. 17025:2017 accredited for I mpact, and carb/decarb te with the current revision	ed by the :2015 Quality tensile, Brinell sting, of ASTM A370,		
This test report shall not be repro- shall it be modified in any way with Steel Products.	duced or distributed, excer thout the written permissio	pt in full, nor in of Vulcan	Sallie Nowood	4/7/22
Document is in accordance with E	EN 10204 - 3.1B of 2004 (3	3.1).	Norwood, Sallie - Certification Engineer	Date

Plex 4/7/22 10:45 AM vulc.sano Page 2 of 2

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	Portland Bolt	ORI	DER #	166890	
			DATE	9/20/2023	
	800-547-6758 www.portlandbolt.com		PAGE	1 of 1	
sales@portlandbolt	.com Phone: 800.547.6758 Fax: 503.227.4634	SALI	ESPERSON	Shanna McKee	
www.portlandbolt	.com 3441 NW Guam St. Portland OR, 97210	DIRE	CT PHONE	888.602.8920	
SOLD TO		SHIP TO	EMAIL	shanna@portlan	dbolt.com
TEXAS A&M TRAI	SPORTATION INST	Adam Mayer @ 97931	72667		
TTI FINANCIAL SE	RVICES	1111 Rellis Parkway			
3135 TAMU		Bryan, TX, 77807			
COLLEGE STATIO	N, TX, 77843-3135				
Phone: 979.317.2	755 Fax: 979.227.7710				
ATTN	Adam Mayer <a-mayer@tti.tamu.edu></a-mayer@tti.tamu.edu>			CUSTOMER PO	617741
SHIP DATE	9 /26/ 2 0 23 (scheduled)	Ship Via	UPS Gro	und	
LINE QTY. DESCR	PTION				
1 34 1/2"	-13 x 8" domestic hot-dip galvanized ASTM A193 (Grade B7 all thread rod			
2 17 1/2"	-13 x 11" domestic hot-dip galvanized ASTM A193	Grade B7 all thread rod			

	exas A&M ransportation istitute	QF 7.3-01 Sam	Concrete pling	Doc. No. QF 7.3- 01	Revision Date: 2020-0 7- 29
Qualit	y Form	Revised by: B.L. Griffi Approved by: D. L. Ku	th ihn	Revision: 7	Page: 1 of 1
Project No:	440863-3	Casting Date:	2023-05-05	Mix Design (psi)	4000
Name of Technician Taking Sample	Terracon		Name of Technician Breaking Sample	Terracon	
Signature of Technician Taking Sample	Terracon		Signature of Technician Breaking Sample	Terracon	
Load No.	Truck No.	Ticket No.	Locat	ion (from concret	e map)
Check	Thomas, Trav13	77078	North Wall to Se	nsors	
Check	Cross, Dwante8	77081	North end of de	ck to sensors	
Check	Burns, Christ0	77085	Remainder of de	eck and wall	
Load No.	Break Date	Cylinder Age	Total Load (lbs)	Break (psi)	Average

REMIT PAYMEN	NT TO: 862 5222	Sandy Point Dr	FAC	RE	PI	NEHURST DISPATC	CE - 979-985-
RURTEN, TAT	Br	yan, Tx 77807	17534 SH 6 College Station	South 18 TX 77845 Pi	935 Circle Lake Dr nehurst, TX 77362	Define addy	
MAC MAN	AGEMENT		ant v abwards			UVER HILL,	RT
RELLIS	- TII WHITE	LHOUSE, BRY	AN TX AT	2818, RT HUY	47, LT INTE	RELLIS CH	HE GATE
		LOAD SIZE	ballinges al off	" SIRAIGHT	THE MAIN		THANT TRANSA
TIME	FORMOLA	10,00	YARD ORDERED	in training and the second	DRIVER/TRUCK	The second second	70084
9:29 DATE	DCLS4000	LOAD#	YARDS DEL	D#	THOMAS,	TRAVI3 SLUMP	TICKET NUM
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940	9.35		ON OTT	this address these	nadwitett nebr	Ticket Tot	al
FINISH UNLOADING	LEFT JOB		TERI TESTING LAB: GES	PACON SNER	Mces such as g	ADDITIONAL CHAR	GE 1
	Tot of dimension	ESTED	CME	OTHER CYLINDERS	THING DUST.	ADDITIONAL CHARG	GE 2
- B	YES		EMBINOU H. 28 ISON SO OF 971	nose and and by MAC and	ding pneumocr	GRAND TOTAL	
	WARNING	and the second	PROPERTY DA (TO BE SIGNED IF DELIVERY T	MAGE RELEASE	Excessive Wate H,0 A	r is Detrimental to Concr dded by Request/Authori	ete Performance
IDDITAT	ING TO THE SKIN A ant, Wear Rubber Boots a BURNS, Avoid Contact	IND EYES Ind Gloves, PROLONGED With Eyes and Prolonged	RELEASE to you for your sign size and weight of this truck i the premises and/or adjace material in this load where y	ature is of the opinion that the may possibly cause damage to nt property if he places the bu desire it. It is our wish to	GAL X	mis material.	
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	10:21 DATE DATE 5/5/23 OUANTITY 8.00 y 1.00 e LEFT PLANT LEFT PLANT Contains plottand Car FINISH UNILOADING FINISH UNILOADING CONTACT MAY CALO CONTACT FOR THE A DECEMBER OF THE ADDRESS CONTACT FOR THE ADDRESS CONTACT FOR THE ADDRESS UPDATE	DCLS4000 PROJECT SINGLES CODE d TDCLS400 a FUEL ARRIVED JOB LEFT JOB USE WARNING TING TO THE SKIN AI THE WARNING TO THE SKIN AI SE BURNS. Avid Contact V sis. Get Medical Alternion, Kel Mark Composition, Kel	START UNLOADING START UNLOADING ARRIVED AT PLANT ARRIVED AT PLANT STED NO ND EYES I Glovas PROLONGED With Eyes and Prophyly Was es Rinse Thorphology Was es Rinse Thorphol	CLASS GLASS Fuel C SLUMP ON SITE TESTING LAB: GESS CME AIR PROPERTY DAM (TO RESIDED & DELYERY TO RELEASE ON THE ON THE ONE AIR PROPERTY DAM (TO RESIDED & DELYERY TO RELEASE ON THE ONE OF DELYERY TO AIR DECEMBER 100 AND THE ONE AIR COME SIGNED & DELYERY TO AIR COME SIGNED & DELYERY COME SIG	BATCH# BATCH# S 40000 PS Change CONCRETE TEMP. CONCRETE TEMP.	Excessive Wate Barrier	SLUMP 5. @@ in UNIT PRICE 1 for your Tax Prev. AM Ticket Tota ADDITIONAL CHARG ADDITIONAL CHARG GRAND TOTAL ris Detrimental to Concre idee by Request/Authoriz	TICKET NUMBER 77085 EXTENDED PRIC business f 1 1 E 1 E 2
	10:21 DATE 5/5/23 QUANTITY 8.00 y 1.00 e LEFT PLANT //00 e LEFT PLANT //00 Contact Marken to FINISH UNLOADING FINISH UNLOADING CONTACT MARK TO CONTACT MARK TO CONTACT CONTACT CONTACT CONTACT CONTACT CONTACT	DCLS4000 PRDJECT SINGLES CODE d TDCLS400 a FUEL ARRIVED JOB LOSSO LEFT JOB TE VES WARNING TING TO THE SKIN AL NEW WARNING TING TO THE SKIN AL NEW WARNING THE SKIN AL NEW W	S. (20) LOAD# LOAD# B. (20) DESCRIPTION DESCRIPRO DESCRIPTION DESCRIPTION DESCRIPTION	CLASS GLASS Fuel C SLUMP ON SITE TESTING LAB: ON SITE TESTING	BATCH# BATCH# BATCH# BATCH# S 40000 PS Change CONCRETE TEMP. CONCR	I Thank you AIR TEMP Excessive Wate H,0 AC GAL X WEIGHMASTER Surcl	SLUMP 5. @@ in UNIT PRICE UNIT PRICE Tax Prev. AM Ticket Tota ADDITIONAL CHARG GRAND TOTAL r is Detrimental to Concre sded by Request/Authoriz	TICKET NUMBER 77085 EXTENDED PRIC business I atl E1 te Performance. ards
	10:21 DATE 5/5/23 OUANTITY 8.00 y 1.00 e LEFT PLANT //00 e LEFT PLANT //00 CONTACT FINISH UNLOADING	DCLS4000 PROJECT SINGLES CODE d TDCLS400 a FUEL ARRIVED JOB LOS5 LEFT JOB LEFT JOB TE LEFT JOB TE SINGLES	Control of the set of the se	CLASS GLASS GLAS GLA	BATCH# BATCH# BATCH# S 4000 PS Change CONCRETE TEMP. CONCRETE TEMP. TESTING ACON INFER CYLINDERS CYLINDERS CYLINDERS ACON INFER CYLINDE	Excessive Wate AIR TEMP AIR TEMP Excessive Wate Hg Ac GAL X WEIGHMASTER Surce	SLUMP 5. @@ in UNIT PRICE UNIT PRICE I for your Tax Prev. AM Ticket Tota ADDITIONAL CHARG ADDITIONAL CHARG GRAND TOTAL r is Detrimental to Concre Sded by Request/Authoriz I arge for credit c Story (MDICATES, THAT HASIDE CURE UNE	TICKET NUMBER 77085 EXTENDED PRIC EXTENDED PRIC business f 11 E1 E2 Ste Performance. sed By: ards MAKE READ THE HEAL

CONCRETE COMPRESSIVE STRENGTH TEST REPORT

Report Number: A1171057.0272 Service Date: 05/05/23 Report Date: 05/25/23 Revision 1 - 17-day results Task: PO# 440863-3

Client

Texas Transportation Institute Attn: Bill Griffith TTI Business Office 3135 TAMU College Station, TX 77843-3135

Material Information

Specified Strength: 4,000 psi @ 28 davs

Mix ID: TDCLS4000 Supplier: Texcrete Batch Time: Plant: Truck No.: **TEAVI3** Ticket No.: 77078

Field Test Data

Test	Result
Slump (in):	5 1/2
Air Content (%):	2.2
Concrete Temp. (F):	85
Ambient Temp. (F):	76
Plastic Unit Wt. (pcf):	148.0
Yield (Cu. Yds.):	

Project Riverside Campus Riverside Campus Bryan, TX

Project Number: A1171057

Sample Information 05/05/23 Sample Time: Sample Date: Sampled By: Justin Maass Weather Conditions: Clear, light wind Accumulative Yards: 10/30 Batch Size (cy): 10 Direct Discharge Placement Method: Water Added Before (gal): 0 Water Added After (gal): 0 Sample Location: East end Placement Location: Bridge wall deck Sample Description: 6-inch diameter cylinders

Laboratory Test Data

Set No.	Spec ID	Cyl. Cond.	Avg Diam. (in)	Area (sq in)	Date Received	Date Tested	Age at Test (days)	Max Load (lbs)	Comp Strength (psi)	Frac Type	Tested By
1	Α	Good	6.00	28.27		05/12/23	7 F	102,700	3,630	2	TJT
1	В	Good	6.01	28.37		05/22/23	17 F	130,610	4,600	2	TJT
1	С	Good	6.01	28.37		05/22/23	17 F	127,730	4,500	2	TJT
1	D	Good	6.01	28.37		05/22/23	17 F	120,400	4,240	3	TJT
Initial C	ure: Ou	tside Plastic Lic	ds	Final	Cure: Field (Cured					

Comments: F = Field Cured

Note: Reported air content does not include Aggregate Correction Factor (ACF).

Specification

Samples Made By: Terracon

Obtain samples of fresh concrete at the placement locations (ASTM C 172), perform required field tests and cast, cure, and test Services: compressive strength samples (ASTM C 31, C 39, C 1231).

Start/Stop:

Terracon Rep.: Justin Maass Reported To: Bill w/ TTI Contractor: MDC **Report Distribution:**

(1) Texas Transportation Institute, Bill Griffith (1) Texas Transportation Institute, Adam Mayer

Test Methods: ASTM C 31, ASTM C143, ASTM C231, ASTM C1064

The tests were performed in general accordance with applicable ASTM, AASHTO, or DOT test methods. This report is exclusively for the use of the client indicated above and shall not be reproduced except in full without the written consent of our company. Test results transmitted herein are only applicable to the actual samples tested at the location(s) referenced and are not necessarily indicative of the properties of other apparently similar or identical materials.

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lerracon

1010
Report Number:	A1171057.0	272
Service Date:	05/05/23	
Report Date:	05/25/23	Revision 1 - 17-day results
Task:	PO# 440863	3-3

Client

Texas Transportation Institute Attn: Bill Griffith TTI Business Office 3135 TAMU College Station, TX 77843-3135

Material Information

Specified Strength: 4,000 psi @ 28 davs

Mix ID: TDCLS4000 Supplier: Texcrete Batch Time: 1004 Plant: Truck No.: DWANTE8 Ticket No.: 77081

Field Test Data

Test	Result
Slump (in):	6
Air Content (%):	2.0
Concrete Temp. (F):	84
Ambient Temp. (F):	75
Plastic Unit Wt. (pcf):	147.7
Yield (Cu. Yds.):	

Riverside Campus **Riverside** Campus Bryan, TX Project Number: A1171057

Project

Sample Information 05/05/23 Sample Time: Sample Date: Sampled By: Justin Maass Weather Conditions: Accumulative Yards: 20/30 Placement Method: Water Added Before (gal): 0 Water Added After (gal): 0 Sample Location: Middle of wall Placement Location: Bridge wall deck Sample Description:

1046 Clear, light wind Batch Size (cy): 10 Direct Discharge

lerracon

College Station, TX 77845-5765 979-846-3767 Reg No: F-3272

6198 Imperial Loop

6-inch diameter cylinders

Laboratory Test Data

Set No.	Spec ID	Cyl. Cond.	Avg Diam. (in)	Area (sq in)	Date Received	Date Tested	Age at Test (days)	Max Load (Ibs)	Comp Strength (psi)	Frac Type	Tested By
2	А	Good	6.01	28.37		05/22/23	17 F	124,390	4,380	2	TJT
2	В	Good	6.01	28.37		05/22/23	17 F	120,780	4,260	2	TJT
2	С	Good	6.01	28.37		05/22/23	17 F	120,460	4,250	2	TJT
2	D						Hold				
Initial C	ure: C	Outside Plastic Lid	S	Final	Cure: Field (Cured					

Comments: F = Field Cured

Note: Reported air content does not include Aggregate Correction Factor (ACF).

Specification

Samples Made By: Terracon

Obtain samples of fresh concrete at the placement locations (ASTM C 172), perform required field tests and cast, cure, and test compressive strength samples (ASTM C 31, C 39, C 1231). Services:

Start/Stop:

Terracon Rep.: Justin Maass Reported To: Bill w/ TTI Contractor: MDC **Report Distribution:**

(1) Texas Transportation Institute, Bill Griffith (1) Texas Transportation Institute, Adam Mayer

Test Methods: ASTM C 31, ASTM C143, ASTM C231, ASTM C1064

The tests were performed in general accordance with applicable ASTM, AASHTO, or DOT test methods. This report is exclusively for the use of the client indicated above and shall not be reproduced except in full without the written consent of our company. Test results transmitted herein are only applicable to the actual samples tested at the location(s) referenced and are not necessarily indicative of the properties of other apparently similar or identical materials.

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Report Number: A1171057.0272 05/05/23 Service Date: Report Date: 05/25/23 Revision 1 - 17-day results Task: PO# 440863-3

Client

Texas Transportation Institute Attn: Bill Griffith TTI Business Office 3135 TAMU College Station, TX 77843-3135

Material Information

Specified Strength: 4,000 psi @ 28 davs

Result

TDCLS4000 Mix ID: Supplier: Texcrete Batch Time: 1021 Plant: Truck No.: CHEISTO1 Ticket No.: 77085

Field Test Data Test Slump (in):

6 3/4 Air Content (%): 1.5 Concrete Temp. (F): 84 Ambient Temp. (F): 75 Plastic Unit Wt. (pcf): 146.8 Yield (Cu. Yds.):

Riverside Campus Riverside Campus Bryan, TX Project Number: A1171057

Project

05/05/23 Sample Time: Justin Maass Weather Conditions: Clear, light wind Accumulative Yards: Cloudy, lig Batch Size (cy): 10 Placement Method: Direct Discharge Water Added Before (gal): 0 Water Added After (gal): 0 West end of wall Sample Location: Placement Location: Bridge wall deck Sample Description: 6-inch diameter cylinders

Terracon

1100

College Station, TX 77845-5765

979-846-3767 Reg No: F-3272

6198 Imperial Loop

Laboratory Test Data

Set No.	Spec ID	Cyl. Cond.	Avg Diam. (in)	Area (sq in)	Date Received	Date Tested	Age at Test (days)	Max Load (Ibs)	Comp Strength (psi)	Frac Type	Tested By
3	Α	Good	6.01	28.37		05/22/23	17 F	113,600	4,000	2	TJT
3	В	Good	6.01	28.37		05/22/23	17 F	112,140	3,950	2	TJT
3	С	Good	6.01	28.37		05/22/23	17 F	110,790	3,910	2	TJT
3	D						Hold				
Initial C	ure: Out	tside Plastic Lid	ds	Final	Cure: Field (Cured					

Comments: F = Field Cured

Note: Reported air content does not include Aggregate Correction Factor (ACF).

Specification

Samples Made By: Terracon

Obtain samples of fresh concrete at the placement locations (ASTM C 172), perform required field tests and cast, cure, and test Services: compressive strength samples (ASTM C 31, C 39, C 1231).

Terracon Rep.: Justin Maass Reported To: Bill w/ TTI Contractor: MDC **Report Distribution:**

(1) Texas Transportation Institute, Bill Griffith (1) Texas Transportation Institute, Adam Mayer

Start/Stop:

Reviewed By:

kander Durigan, P.E.

Project Manager

Test Methods: ASTM C 31, ASTM C143, ASTM C231, ASTM C1064

The tests were performed in general accordance with applicable ASTM, AASHTO, or DOT test methods. This report is exclusively for the use of the client indicated above and shall not be reproduced except in full without the written consent of our company. Test results transmitted herein are only applicable to the actual samples tested at the location(s) referenced and are not necessarily indicative of the properties of other apparently similar or identical materials.

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Sample Information Sample Date: Sampled By:

	exas A&M ransportation istitute	QF 7.3-01 Sam	Concrete pling	Doc. No. QF 7.3- 01	Revision Date: 2020-0 7- 29				
Qualit	y Form	Revised by: B.L. Griffi Approved by: D. L. Ku	th 1hn	Revision: 7	Page: 1 of 1				
Project No:	440863-01-3	Casting Date:	2023-05-15	Mix Design (psi)	3600				
Name of Technician Taking Sample	Terracon		Name of Technician Breaking Sample	Terracon					
Signature of Technician Taking Sample	Terracon		Signature of Technician Breaking Sample	Terracon					
Load No.	Truck No.	Ticket No.	Locat	ion (from concret	e map)				
Check	111	80543	Full barrier from south	end 40ft north. Half	ift till 20 ft from north				
Check	116	80544	Top half lift starting 40ft from south end. Full barrier 20 ft from north end to north finish						
Load No.	Break Date	Cylinder Age	Total Load (lbs)	Break (psi)	Average				



	TIME	FORMULA	LOAD SIZE	YARD ORDERED	.co#	DRIVER/TRUCK		PLANT TRANSACTION#
	9:41	TDCLC360	104.00	17.00 YARDS DEL.	BATCH#	WATER TRIM	116 SLUMP	16 TICKET NUMBER
	DATE	STNG/ES	7.00	17.00	PLT Ø2		5.00 ir	80544
	QUANTITY	CODE	DESCRIPTION				UNIT PRICE	EXTENDED PRICE
1	LEFT PLANT	ARRIVED JOB	START UNLOADING	SLUMP	CONCRETE TEMP.	AIR TEMP	Ta Prev. P	
1	62	1024					Ticket To	
FIN	NISH UNLOADING	LEFT JOB	ARRIVED AT PLANT	ON SIT	E TESTING RRACON			
				TESTING LAB: GES CM	SSNER E OTHER		ADDITIONAL CHA	ARGE 1
				AIR	CYLINDEHS		GRAND TOTA	
ains TAC Ict v If CRES INAL This ed in 1, N at Ti 00 S s. De	IRRITATING a Portland Cement, T MAY CAUSE Bi with Skin. In Case of Imitation Persists. G TE is a PERISHABLE SER UPON LEAVING INSTRUCTION IN	WARNING TO THE SKIN AI Wear Rubber Boots an JUNS. Avoid Contact V Contact with Skin or Eye et Medical Attention KEE coMMODIT' and BECOM the TELEPHONED to the to pay all costs, including ad. so dealucery will bear interest with Aggregate or Color Osa dot the Cash Discontact An other Cash Discontact An in will be Stocomer.	ND EYES d Gloves. PROLONGED drift Eyes and Prolonged se, Rinse Thoroughly With P CHLDREN AWAY. Bes The PROPERTY of the Son CanteeLLATION of SPECE DEFORE LOADING to Charles LOADING son charles LOADING the rate of 18% per ity. No Claim Allowed Unless se Collected on all Returned	PROPERTUD (TO be signate in Pollument Part 2 uptomer - The dwy RELEASE to you for your a sea and weight of this flux sea and weight of this flux and weight of this flux are and weight of this flux may occur to the prem may occur to the prem buildings sidwards, drive this flux are and the sea and for a casimed by anyone to have SIGNED:	AMAGE RELEASE VTO BE HACE INDEC CARD LO ar of this truck in presentry of grature is of the control that K may nogably of the places you deen it. This car wat we can bulk in order to so the ease and or adjacent profe- responsibility releases and or adjacent responsibility releases and or adjacent responsibility releases the will not the same additional consideration: supplier for any and all dama arisen out of delivery of this c	Excessive W his H; his H; his GAL WEIGHMAST WEIGHMAST WARNING NOTCE AI WARNING NOTCE AI WARNING NOTCE AI WARNING NOTCE AI UOAD RECEIVE X_	later is Detrimental to C 0 Added by Request/Ar X ER urcharge for cr/ ure, below Indicates by Supplice, will, NOT restrict Notice Cutted IN D BY	Concrete Performance. uthorized By: edit cards a THAT I HAVE READ THE BE RESPONSIBLE FOR ANY E.
The second second								1294

 Report Number:
 A1171057.0273

 Service Date:
 05/15/23

 Report Date:
 05/25/23

 Task:
 PO# 440863-3

Client

Texas Transportation Institute Attn: Bill Griffith TTI Business Office 3135 TAMU College Station, TX 77843-3135

Material Information

Field Test Data

Air Content (%):

Yield (Cu. Yds.):

Concrete Temp. (F):

Ambient Temp. (F):

Plastic Unit Wt. (pcf):

Slump (in):

Test

Specified Strength: 3,600 psi @ 28 days

Result

7 1/2

0.8

95

78

147.2

 Mix ID:
 TDCLC3600

 Supplier:
 Texcrete

 Batch Time:
 0923
 Plant:

 Truck No.:
 111
 Ticket No.:
 80543

 Sample Information
 0

 Sample Date:
 0

 Sampled By:
 D

 Weather Conditions:
 S

 Accumulative Yards:
 1

 Placement Method:
 D

 Water Added Before (gal):
 5

 Water Added After (gal):
 0

 Sample Location:
 Location:

Sample Description:

Project Number: A1171057

Project

Bryan, TX

Riverside Campus

Riverside Campus

05/15/23 Sample Time: 1021 Daniel Calvo Sunny 10.00/17.0Batch Size (cy): 10 Direct Discharge 5 0

lerracon

College Station, TX 77845-5765

979-846-3767 Reg No: F-3272

6198 Imperial Loop

u Luminaire Bridge Deck 20' North of South end Luminaire Bridge Deck 6-inch diameter cylinders

Laboratory Test Data

Set No.	Spec ID	Cyl. Cond.	Avg Diam. (in)	Area (sq in)	Date Received	Date Tested	Age at Test (days)	Max Load (Ibs)	Comp Strength (psi)	Frac Type	Tested By
1	Α	Good	6.01	28.37		05/22/23	7	93,380	3,290	3	TJT
1	В	Good	6.01	28.37		05/22/23	7	97,430	3,430	2	TJT
1	С	Good	6.01	28.37		05/22/23	7	95,680	3,370	2	TJT
							Avera	ge (7 days)	3,370		
1	D						Hold				
Initial C	ure: Cu	re Blanket		Final	Cure: Field (Cured					

Comments: Note: Reported air content does not include Aggregate Correction Factor (ACF).

Specification

Samples Made By: Terracon

Services: Obtain samples of fresh concrete at the placement locations (ASTM C 172), perform required field tests and cast, cure, and test compressive strength samples (ASTM C 31, C 39, C 1231).

Start/Stop: 0830-1245

Terracon Rep.: Daniel Calvo Reported To: Contractor: MBC Management

Report Distribution:

(1) Texas Transportation Institute, Bill Griffith (1) Texas Transportation Institute, Adam Mayer

Test Methods: ASTM C 31, ASTM C143, ASTM C231, ASTM C1064

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TR No. 617741-01-1

Report Number: A1171057.0273 Service Date: 05/15/23 Report Date: 05/25/23 Task: PO# 440863-3

Client

Texas Transportation Institute Attn: Bill Griffith TTI Business Office 3135 TAMU College Station, TX 77843-3135

Material Information

Specified Strength: 3,600 psi @ 28 davs

Result

5 1/4

0.9

95

80

147.5

TDCLC3600 Mix ID: Supplier: Texcrete Batch Time: 0941 Plant: Truck No.: 116 Ticket No.: 80544

Sample Date: Sampled By: Weather Conditions: Accumulative Yards: Placement Method: Water Added After (gal):

Specification

Project

Bryan, TX

Riverside Campus

Riverside Campus

Project Number: A1171057

Sample Information

05/15/23 Sample Time: 1055 Daniel Calvo Sunny 17.00/17.0Batch Size (cy): 7 Direct Discharge Water Added Before (gal): 10 0 Luminaire Bridge Deck 15' South of North

Terracon

College Station, TX 77845-5765

979-846-3767 Reg No: F-3272

6198 Imperial Loop

Sample Location: end **Placement Location:** Luminaire Bridge Deck Sample Description: 6-inch diameter cylinders

Concrete Temp. (F): Ambient Temp. (F): Plastic Unit Wt. (pcf):

Field Test Data

Air Content (%):

Yield (Cu. Yds.):

Slump (in):

Test

Laboratory Test Data

Set No.	Spec ID	Cyl. Cond.	Avg Diam. (in)	Area (sq in)	Date Received	Date Tested	Age at Test (days)	Max Load (Ibs)	Comp Strength (psi)	Frac Type	Tested By
2	А	Good	6.01	28.37		05/22/23	7	101,700	3,580	3	TJT
2	В	Good	6.01	28.37		05/22/23	7	101,730	3,590	2	TJT
2	С	Good	6.01	28.37		05/22/23	7	108,790	3,830	2	TJT
							Avera	ige (7 days)	3,670		
2	D						Hold				
Initial C	ure: Cu	ıre Blanket		Final	Cure: Field (Cured					

Comments: Note: Reported air content does not include Aggregate Correction Factor (ACF).

Samples Made By: Terracon

Obtain samples of fresh concrete at the placement locations (ASTM C 172), perform required field tests and cast, cure, and test Services: compressive strength samples (ASTM C 31, C 39, C 1231).

Terracon Rep.: Daniel Calvo Reported To: Contractor: MBC Management

Report Distribution:

(1) Texas Transportation Institute, Bill Griffith (1) Texas Transportation Institute, Adam Mayer

Start/Stop: 0830-1245

Reviewed By: kander Durigan, P.E.

Project Manager

Test Methods: ASTM C 31, ASTM C143, ASTM C231, ASTM C1064

The tests were performed in general accordance with applicable ASTM, AASHTO, or DOT test methods. This report is exclusively for the use of the client indicated above and shall not be reproduced except in full without the written consent of our company. Test results transmitted herein are only applicable to the actual samples tested at the location(s) referenced and are not necessarily indicative of the properties of other apparently similar or identical materials.

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APPENDIX C. MASH TEST 4-12 (CRASH TEST 617741-01-1)

C.1. VEHICLE PROPERTIES AND INFORMATION

TR No. 617741-01-1



Printed copies are not controlled documents.

ISO/IEC 17025-2017

LF-VPW:10000S

Figure C.1. Vehicle Properties for Test 617741-01-1.

Proving Ground 3100 SH 47, Bidg 7091 Broan TX 77897	Texas A&M Transportation Institute Texas A&M University College Station, TX: 77843 Phone 979-485-8375	LF-VPW:10000 Parameters Wor MASH 100	S Vehicle ksheet for 000S	Doc. No. LF-VPW: 10000S	Revision Date: 2018-07-27
Labora	ntory Form	Revised by: W. L. Menges Approved by: D. L. Kuhn		Revision: 9	Page: 2 of 2
The information containe	d in this document is confidential t Vehicle Inve	to TTI Proving Ground.	1701		
Date: 2023	-11-17 Test No.:	617741-01-1	VIN No.:	 1HTMMAAN	J4DH156266
Year: 20	013 Make:	INTERNATIONAL	Model:	MAXX	FORCE
	WEIGHTS (∬ lb or _ kg) Wfront axle Wrear axle WTOTAL Allowable Range for CURE	CURB 7320 6160 13480 3 = 13,200 ±2200 lb Allowable R	TEST I	NERTIAL 8620 13600 22220 16 ±660 lb	
Ballast: ⁸	740	(as-nee (√Ib or kg) (See M/	ded) A <i>SH</i> Section 4.2.1	.2 for recommer	nded ballasting)
— Mass Distributic (✔Ib or ☐kg):	on LF: <u>4310</u>	RF: <u>4310</u>	LR: <u>6870</u>	RR	<u>6730</u>
Engine Type: D	.6L	Accelero	meter Location x¹	s (∏inches y	or 🗌 mm) z²
		 Front:	0.00	0.00	0.00
Transmission Ty	pe: or 🗖 Manual	Center:	126.69	0.00	50.00
		Rear:	256.69	0.00	50.00
Describe any dar	nage to the vehicle pr	ior to test:			
Other notes to in attachment:	nclude ballast type, o	dimensions, mass, loc	ation, center o	of mass, and	method of
	MIDDLE OF BED				
TIED DOWN V	VITH FOUR 3/8 CABL	ES PER BLOCK			
62.5 INCHES F	FROM GROUND TO	CENTER OF BLOCK			
Performed by:	RK		Date	:2023	-11-17
Referenced to the f Above ground rinted copies are no	front axle ot controlled documents	ISO/IEC 17025:2017		LF	F-VPW:10000S

Figure C.1. Vehicle Properties for Test 617741-01-1 (continued).

C.2. SEQUENTIAL PHOTOGRAPHS









(c) 0.200 s





(e) 0.400 s









(a) 0.000 s

(b) 0.100 s



(c) 0.200 s

(d) 0.300 s



(e) 0.400 s

(f) 0.500 s



(g) 0.600 s (h) 0.700 s Figure C.3. Sequential Photographs for Test 617741-01-1 (Frontal Views).



(a) 0.000 s



(d) 0.300 s

(c) 0.200 s



(f) 0.500 s

(e) 0.400 s



(g) 0.600 s (h) 0.700 s Figure C.4. Sequential Photographs for Test 617741-01-1 (Rear Views).

C.3. VEHICLE ANGULAR DISPLACEMENTS



2.5



C.4. VEHICLE ACCELERATIONS





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