



Test Report No. 620281-01-1&2



GUIDELINES FOR OVERLAPPING PRECAST PORTABLE CONCRETE BARRIERS

Sponsored by
The Roadside Safety Pooled Fund

**TEXAS A&M TRANSPORTATION
INSTITUTE PROVING GROUND**
Roadside Safety & Physical Security
Texas A&M University System
RELLIS Campus
Building 7091
1254 Avenue A
Bryan, TX 77807



1. Report No.	2. Government Accession No.	3. Recipient's Catalog No.	
4. Title and Subtitle Guidelines for Overlapping Precast Portable Concrete Barriers		5. Report Date May 2026	
		6. Performing Organization Code	
7. Author(s) Sofokli Cakalli, Roger P. Bligh, Nauman M. Sheikh, Aniruddha Zalani and William J. L. Schroeder		8. Performing Organization Report No. TRNo. 620281-01-1&2	
9. Performing Organization Name and Address Texas A&M Transportation Institute Proving Ground 3135 TAMU College Station, Texas 77843-3135		10. Work Unit No. (TRAIS)	
		11. Contract or Grant No. Contract T 1969	
12. Sponsoring Agency Name and Address The Roadside Safety Pooled Fund Research Office MS 47372 Olympia, WA 98504-7372		13. Type of Report and Period Covered Technical Report: April 2024 - May 2026	
		14. Sponsoring Agency Code	
15. Supplementary Notes Name of Contacting Representative: Derwood Sheppard			
16. Abstract Overlapping free-standing portable concrete barriers (PCBs) are commonly used in work zones. Despite widespread implementation, overlapping configurations have not been evaluated through full-scale crash testing under the Manual for Assessing Safety Hardware (MASH) (1). As a result, transportation agencies rely largely on engineering judgment when deploying overlapping PCBs. This study evaluated the safety performance of overlapping free-standing F-shape PCBs under MASH Test Level 3 (TL-3) conditions through a combination of survey research, finite element (FE) simulations, and full-scale crash testing. A survey of Roadside Safety Pooled Fund members identified common barrier profiles, connections, and overlap configurations. FE models were developed and validated against prior MASH TL-3 crash tests involving free-standing F-shape barriers (2). The validated models were then used for parametric simulations to evaluate the effects of overlap length, gap size, and impact location, leading to identification of the recommended configuration. The configuration with 1.5-barrier-segment-length overlap and no gap between parallel barrier runs was selected for full-scale crash testing. MASH tests 3-10 and 3-11 were conducted and met the evaluation criteria. The results establish a practical, crash-tested configuration for overlapping free-standing F-shape PCBs and support safer work zone barrier installations.			
17. Key Words Longitudinal Barrier, MASH, Portable Concrete Barrier, PCB, Occupant Risk, Overlapping, Simulation, Finite Element Analysis		18. Distribution Statement No Restrictions	
19. Security Classification. (of this report) Unclassified	20. Security Classification. (of this page) Unclassified	21. No. of Pages 126	22. Price

Form DOT F 1700.7 (8-72) Reproduction of completed page authorized.

Guidelines for Overlapping Precast Portable Concrete Barriers

by

Sofokli Cakalli
Associate Research Engineer
Texas A&M Transportation Institute

Roger P. Bligh
Senior Research Engineer
Texas A&M Transportation Institute

Nauman M. Sheikh
Senior Research Engineer
Texas A&M Transportation Institute

Aniruddha Zalani
Graduate Assistant Researcher
Texas A&M Transportation Institute

and

William J. L. Schroeder
Research Engineering Associate
Texas A&M Transportation Institute

Report 620281-01-1&2
Contract No.: T 1969

Sponsored by the

The Roadside Safety Pooled Fund

May 2026

TEXAS A&M TRANSPORTATION INSTITUTE
College Station, Texas 77843-3135

DISCLAIMER

The contents of this report reflect the views of the authors, who are solely responsible for the facts and accuracy of the data and the opinions, findings, and conclusions presented herein. The contents do not necessarily reflect the official views or policies of the Roadside Safety Pooled Fund, The Texas A&M University System, or the Texas A&M Transportation Institute (TTI). This report does not constitute a standard, specification, or regulation. In addition, the above listed agencies/companies assume no liability for its contents or use thereof. The names of specific products or manufacturers listed herein do not imply endorsement of those products or manufacturers.

The results reported herein apply only to the article tested. The full-scale crash tests were performed according to TTI Proving Ground quality procedures and American Association of State Highway and Transportation Officials (AASHTO) Manual for Assessing Safety Hardware, Second Edition (*MASH*) guidelines and standards.

The Proving Ground Laboratory within TTI's Roadside Safety and Physical Security Division ("TTI Lab") strives for accuracy and completeness in its crash test reports. On rare occasions, unintentional or inadvertent clerical errors, technical errors, omissions, oversights, or misunderstandings (collectively referred to as "errors") may occur and may not be identified for corrective action prior to the final report being published and issued. If, and when, the TTI Lab discovers an error in a published and issued final report, the TTI Lab will promptly disclose such error to the Roadside Safety Pooled Fund, and both parties shall endeavor in good faith to resolve this situation. The TTI Lab will be responsible for correcting the error that occurred in the report, which may be in the form of errata, amendment, replacement sections, or up to and including full reissuance of the report. The cost of correcting an error in the report shall be borne by the TTI Lab. Any such errors or inadvertent delays that occur in connection with the performance of the related testing contract will not constitute a breach of the testing contract.

ACKNOWLEDGEMENTS

This research project was performed under a pooled fund program between the following States and Agencies. The authors acknowledge and appreciate their guidance and assistance.

Roadside Safety Research Pooled Fund Committee Revised April 2024

ALABAMA

Wade Henry, P.E.

Assistant State Design Engineer
Design Bureau, Final Design Division
Alabama Dept. of Transportation
1409 Coliseum Boulevard, T-205
Montgomery, AL 36110
(334) 242-6464
henryw@dot.state.al.us

Stanley (Stan) C. Biddick, P.E.

State Design Engineer
Alabama Dept. of Transportation
1409 Coliseum Boulevard, T-205
Montgomery, AL 36110
(334) 242-6488
biddicks@dot.state.al.us

ALASKA

Mary F. McRae

Assistant State Traffic & Safety
Engineer Alaska Depart. of Transportation &
Public Facilities
3132 Channel Drive
P.O. Box 112500
Juneau, AK 99811-2500
(907) 465-6963
mary.mcrae@alaska.gov

Micheal Hills

Alaska Depart. of Transportation & Public
Facilities
micheal.hills@alaska.gov

CALIFORNIA

Bob Meline, P.E.

Caltrans
Office of Materials and Infrastructure
Division of Research and Innovation
5900 Folsom Blvd
Sacramento, CA 95819
(916) 227-7031
Bob.Meline@dot.ca.gov

John Jewell, P.E.

Senior Crash Testing Engineer
Office of Safety Innovation & Cooperative
Research
(916) 227-5824
John_Jewell@dot.ca.gov

COLORADO

David Kosmiski, P.E.

Miscellaneous (M) Standards Engineer
Division of Project Support, Construction
Engineering Services (CES) Branch
Colorado Dept. of Transportation (CDOT)
2829 W. Howard Pl.
Denver, CO 80204
303-757-9021
david.kosmiski@state.co.us

Andy Pott, P.E.

Senior Bridge Design and Construction
Engineer
Division of Project Support, Staff Bridge
Design and Construction Management
Colorado Dept. of Transportation (CDOT)
4201 E Arkansas Ave, 4th Floor
Denver, CO 80222
303-512-4020
andrew.pott@state.co.us

Shawn Yu, P.E.

Miscellaneous (M) Standards and
Specifications Unit Manager
Division of Project Support, Construction
Engineering Services (CES) Branch
Colorado Dept. of Transportation (CDOT)
4201 E Arkansas Ave, 4th Floor
Denver, CO 80222
303-757-9474
shawn.yu@state.co.us

Amin Fakhimalizad

Assistant Miscellaneous (M) Standards
Engineer
Division of Project Support, Construction
Engineering Services (CES) Branch
Colorado Dept. of Transportation (CDOT)
303-757-9229
amin.fakhimalizad@state.co.us

Man (Steven) Yip

Division of Project Support, Construction
Engineering Services (CES) Branch
Colorado Dept. of Transportation (CDOT)
man.yip@state.co.us

CONNECTICUT**David Kilpatrick**

Transportation Supervising Engineer
State of Connecticut Depart. of
Transportation
2800 Berlin Turnpike
Newington, CT 06131-7546
(806) 594-3288
David.Kilpatrick@ct.gov

Todd Ingarra

todd.ingarra@ct.gov

DELAWARE**Cassidy Blowers**

Construction Resource Engineer
Construction Section
Delaware DOT
(302)760-2336
Cassidy.Blowers@delaware.gov

James Osborne

Traffic Safety Programs Manager
Traffic Operations
Delaware DOT
(302)659-4651
James.Osborne@delaware.gov

FLORIDA**Richard Stepp**

Florida Department of Transportation
Richard.Stepp@dot.state.fl.us

Derwood C. Sheppard, Jr., P.E.

State Roadway Design Engineer
Florida Depart. of Transportation
Roadway Design Office
605 Suwannee Street, MS-32
Tallahassee, FL 32399-0450
(850) 414-4334
Derwood.Sheppard@dot.state.fl.us

IDAHO**Marc Danley, P.E.**

Technical Engineer
(208) 334-8558
Marc.danley@itd.idaho.gov

Kevin Sablan

Design/Traffic Engineer
Idaho Transportation Department
(208) 334-8558
Kevin.sablan@itd.idaho.gov

ILLINOIS**Martha A. Brown, P.E.**

Safety Design Bureau Chief
Bureau of Safety Programs and Engineering
Illinois Depart. of Transportation
2300 Dirksen Parkway, Room 005
Springfield, IL 62764
(217) 785-3034
Martha.A.Brown@illinois.gov

Edgar A. Galofre, MSCE, P.E.

Safety Design Engineer
Bureau of Safety Programs and Engineering
Illinois Department of Transportation
2300 S. Dirksen Parkway, Room 007
Springfield, IL 62764
(217) 558-9089
Edgar.Galofre@illinois.gov

IOWA**Daniel Harness**

Design Bureau – Methods Section
Iowa Department of Transportation
Daniel.Harness@iowadot.us

Chris Poole

State Traffic Engineer
Traffic and Safety Bureau
Iowa Department of Transportation
Chris.Poole@iowadot.us

LOUISIANA**Ryan Owens, P.E.**

Bridge Design Section
Louisiana Department of Transportation and
Development
Bridge & Structural Design Section
P.O. Box 94245
Baton Rouge, LA 70804-9245
(225) 379-1869
Ryan.Owens@la.gov

Chris Guidry

Assistant Bridge Design Administrator
Louisiana Department of Transportation and
Development
Bridge & Structural Design Section
P.O. Box 94245
Baton Rouge, LA 79084-9245
(225) 379-1328
Chris.Guidry@la.gov

MARYLAND**Philip Brentlinger**

Maryland State Highway Administration
pbrentlinger@mdot.maryland.gov

MASSACHUSETTS**James Danila**

Assistant State Traffic Engineer
Massachusetts Depart. of Transportation
(857) 368-9640
James.danila@state.ma.us

Alex Bardow

Director of Bridges and Structure
Massachusetts Depart. of Transportation
10 Park Plaza, Room 6430
Boston, MA 02116
(857) 368-9430
Alexander.Bardow@state.ma.us

MICHIGAN**Carlos Torres, P.E.**

Roadside Safety Engineer
Geometric Design Unit, Design Division
Michigan Depart. of Transportation
P. O. Box 30050
Lansing, MI 48909
(517) 335-2852
TorresC@michigan.gov

MINNESOTA**Khamsai Yang**

Design Standards Engineer
Office of Project Management and
Technical Support
(612) 322-5601
Khamsai.Yang@state.mn.us

Brian Tang

Assistant Design Standards Engineer
Office of Project Management and
Technical Support
Minnesota Department of Transportation
brian.tang@state.mn.us

MISSOURI**Gidget Koestner**

Policy & Innovations Engineer
Central Office- Design
Missouri Department of Transportation
(573) 751-6905
gidget.koestner@modot.mo.gov

Kirby Woods

Roadside Design Engineer
Missouri Department of Transportation
(573) 472-5333
kirby.woodsjr@modot.mo.gov

NEW MEXICO**Brad Julian**

New Mexico Department of Transportation
Traffic Technical Support Engineer
(505) 469-1405
Brad.Julian@dot.nm.gov

NEVADA**David Fox, P.E.**

Specifications Engineer
Roadway Design Division
Nevada Dept. of Transportation
1263 S. Stewart St.
Carson City, NV 89712
(775) 888-7053
DWFox@dot.nv.gov

Tim Rudnick

Standards and Manuals Supervisor
Roadway Design Division
Nevada Dept. of Transportation
1263 S. Stewart St.
Carson City, NV 89712
(775) 888-7598
TRudnick@dot.nv.gov

OHIO**Don P. Fisher, P.E.**

Ohio Depart. of Transportation
1980 West Broad Street
Mail Stop 1230
Columbus, OH 43223
(614) 387-2614
Don.fisher@dot.ohio.gov

OREGON**Christopher Henson**

Senior Roadside Design Engineer
Oregon Depart. of Transportation
Technical Service Branch
4040 Fairview Industrial Drive, SE
Salem, OR 97302-1142
(503) 986-3561
Christopher.S.Henson@odot.state.or.us

PENNSYLVANIA**James A. Borino, Jr., P.E.**

Chief, Standards and Criteria Unit
Highway Design and Technology Division
Pennsylvania DOT
(717) 612-4791
jborino@pa.gov

Evan Pursel

Senior Civil Engineer
Highway Design and Technology Division
Pennsylvania DOT
(717) 705-8535
epursel@pa.gov

Nina Ertel

Project Development Engineer
Highway Design and Technology Division
Pennsylvania DOT
(717) 425-7679
nertel@pa.gov

TENNESSEE**Laura Chandler**

Engineering Production Support Manager
Engineering Division
Tennessee Dept. of Transportation
(615) 253-4769
Laura.Chandler@tn.gov

Ali Hangul M.S., P.E

State Standards Transportation Engineer
Engineering Production Support,
Engineering Division
Tennessee Dept. of Transportation
(615) 741-0840
Ali.Hangul@tn.gov

TEXAS

Chris Lindsey

Transportation Engineer
Design Division
Texas Department of Transportation
125 East 11th Street
Austin, TX 78701-2483
(512) 416-2750
Christopher.Lindsey@txdot.gov

Taya Retterer

TxDOT Bridge Standards Engineer
Bridge Division
Texas Department of Transportation
(512) 993-0330
Taya.Retterer@txdot.gov

Wade Odell

Research Project Manager
Research & Technology Implementation
Division
Texas Department of Transportation
(512) 416-4737
wade.odell@txdot.gov

UTAH

Clint McCleery

Barrier and Attenuation Specialist
Traffic and Safety Operations
Utah Department of Transportation
(801)712-8685
cmccleery@utah.gov

WASHINGTON

Tim Moeckel

Roadside Safety Engineer
Washington State Department of
Transportation
Development Division
P.O. Box 47329
Olympia, WA 98504-7246
(360) 704-6377
moecket@wsdot.wa.gov

Mustafa Mohamedali

Research Manager/Engineering
Transportation Safety & System Analysis
Research & Library Services
(360) 704-6307
mohamem@wsdot.wa.gov

Kevin Burch

Policy Support Engineer
Washington State Department of
Transportation
Development Division
burchk@wsdot.wa.gov

WEST VIRGINIA

Donna J. Hardy, P.E.

Mobility, ITS & Safety Engineer
West Virginia Depart. of
Transportation – Traffic Engineering
Building 5, Room A-550
1900 Kanawha Blvd E.
Charleston, WV 25305-0430
(304) 414-7338
Donna.J.Hardy@wv.gov

Ted Whitmore

Traffic Services Engineer
Traffic Engineering
WV Division of Highways
(304)414-7373
Ted.J.Whitmore@wv.gov

WISCONSIN

Erik Emerson, P.E.

Standards Development Engineer –
Roadside Design
Wisconsin Department of Transportation
Bureau of Project Development
4802 Sheboygan Avenue, Room 651
P. O. Box 7916
Madison, WI 53707-7916
(608) 266-2842
Erik.Emerson@wi.gov

CANADA – ONTARIO

Kenneth Shannon, P. Eng.

Senior Engineer, Highway Design (A)
Ontario Ministry of Transportation
301 St. Paul Street
St. Catharines, ON L2R 7R4
CANADA
(904) 704-3106
Kenneth.Shannon@ontario.ca

FEDERAL HIGHWAY ADMINISTRATION (FHWA)

Website: safety.fhwa.dot.gov

Eduardo Arispe

Research Highway Safety Specialist
U.S. Department of Transportation
Federal Highway Administration
Turner-Fairbank Highway Research Center
Mail Code: HRDS-10
6300 Georgetown Pike
McLean, VA 22101
(202) 493-3291
Eduardo.arispe@dot.gov

Richard B. (Dick) Albin, P.E.

Senior Safety Engineer
Office of Innovation Implementation, Safety
& Design Team
(303) 550-8804
Dick.Albin@dot.gov

Paul LaFleur, P.E.

Safety Design Team - Roadway Departure
Program Manager
FHWA Office of Safety
U.S. Department of Transportation
(515) 233-7308
paul.lafleur@dot.gov

Christine Black

Highway Safety Engineer
Central Federal Lands Highway Division
12300 West Dakota Ave.
Lakewood, CO 80228
(720) 963-3662
Christine.black@dot.gov

Isbel Ramos-Reyes

Lead Safety and Transportation Operations
Engineer
Eastern Federal Lands Highway Division
(703) 948-1442
isbel.ramos-reyes@dot.gov

TEXAS A&M TRANSPORTATION INSTITUTE (TTI)

Website: tti.tamu.edu
www.roadsidepooledfund.org

D. Lance Bullard, Jr., P.E.

Senior Research Engineer
Roadside Safety & Physical Security Div.
Texas A&M Transportation Institute
3135 TAMU
College Station, TX 77843-3135
(979) 317-2855
L-Bullard@tti.tamu.edu

Roger P. Bligh, Ph.D., P.E.

Senior Research Engineer
Roadside Safety and Physical Security
Division
(979) 317-2703
R-Bligh@tti.tamu.edu

Nauman Sheikh, P.E.

Senior Research Engineer
Roadside Safety and Physical Security
Texas A&M Transportation Institute
(979) 317-2703
n-sheikh@tti.tamu.edu

Ariel Sheil

Research Assistant
Roadside Safety and Physical Security
Texas A&M Transportation Institute
(979) 317-2250
A-Sheil@tti.tamu.edu

REPORT AUTHORIZATION

REPORT REVIEWED BY:



Glenn Schroeder
Research Specialist
Drafting & Reporting



Ken Reeves
Research Specialist
Electronics Instrumentation



Adam Mayer
Research Specialist
Construction



Richard Badillo
Research Specialist
Photographic Instrumentation



Tristen Janca
Engineering Technician
Mechanical Instrumentation



Bill L. Griffith
Research Specialist
Quality Manager



William J. L. Schroeder
Research Engineering Associate
Research Evaluation and Reporting



Matthew N. Robinson
Research Specialist
Test Facility Manager & Technical
Manager



Sofokli Cakalli
Associate Research Engineer
Research Supervisor

REVISION LOG

Revision Number	Change(s) Made	Date	Approved by

TABLE OF CONTENTS

	Page
Disclaimer	vii
Acknowledgements	ix
Report Authorization	xv
Revision Log	xvi
List of Figures	xix
List of Tables	xxii
Chapter 1. Introduction	1
Chapter 2. Literature Review and Survey	3
Chapter 3. Computer Simulations	9
3.1. Validation of FE Model	9
3.2. Simulations with Overlapping Barriers	12
3.3. Recommended Configuration for Full-Scale Crash Testing	14
Chapter 4. System Details	15
4.1. Test Article and Installation Details	15
4.2. Design Modifications during Tests	15
4.3. Material Specifications	20
Chapter 5. Test Requirements and Evaluation Criteria	21
5.1. Crash Test Performed/Matrix	21
5.2. Evaluation Criteria	21
Chapter 6. Test Conditions	23
6.1. Test Facility	23
6.2. Vehicle Tow and Guidance System	23
6.3. Data Acquisition Systems	24
6.3.1. Vehicle Instrumentation and Data Processing	24
6.3.2. Anthropomorphic Dummy Instrumentation	25
6.3.3. Photographic Instrumentation Data Processing	25
Chapter 7. MASH Test 3-10 (Crash Test 620281-01-1)	27
7.1. Critical Impact Point Location	27
7.2. Test Vehicle Details Prior to Impact	29
7.3. Test Description	31
7.3.1. Weather Conditions	31
7.3.2. Test Events	31
7.4. Test Actual Impact Conditions	32
7.5. Damage to Test Installation	32
7.6. Damage to Test Vehicle	34
7.7. Occupant Risk Factors	38
7.8. Test Summary	38
Chapter 8. MASH Test 3-11 (Crash Test 620281-01-2)	41
8.1. Critical Impact Point Location	41

8.2.	Test Vehicle Details Prior to Impact	43
8.3.	Test Description	45
8.3.1.	Weather Conditions.....	45
8.3.2.	Test Events	45
8.4.	Test Actual Impact Conditions.....	46
8.5.	Damage to Test Installation	46
8.6.	Damage to Test Vehicle.....	49
8.7.	Occupant Risk Factors	52
8.8.	Test Summary	52
Chapter 9. Results of Crash Testing		55
Chapter 10. Summary, Implementation, and Future Research.....		56
10.1.	Summary	56
10.2.	Implementation	57
10.3.	Future Research.....	57
References		59
Appendix A. Standards Drawings		61
A.1.	FDOT Standard Drawings.....	62
A.2.	Ontario Provincial Standard Drawing	65
A.3.	WisDOT Standard Drawings	66
Appendix B. Survey Template		68
Appendix C. Details of Overlapping Precast Portable Concrete Barriers.....		72
Appendix D. Supporting Certification Documents		79
Appendix E. MASH Test 3-10 (Crash Test 620281-01-1)		104
E.1.	Vehicle Properties and Information	104
E.2.	Sequential Photographs.....	107
E.3.	Vehicle Accelerations.....	110
Appendix F. MASH Test 3-11 (Crash Test 620281-01-2)		115
F.1.	Vehicle Properties and Information	115
F.2.	Sequential Photographs.....	118
F.3.	Vehicle Accelerations.....	121

LIST OF FIGURES

	Page
Figure 2.1. FDOT Overlapping PCBs Standards.....	4
Figure 2.2. WisDOT Overlapping PCBs Standards	5
Figure 2.3. Ontario Overlapping PCBs Standards	5
Figure 3.1. FE Model of F-Shape PCB	10
Figure 3.2. Frame 1 of MASH Crash Test 3-10 (2).....	10
Figure 3.3. Frame 2 of MASH Crash Test 3-10 (2).....	10
Figure 3.4. Frame 3 of MASH Crash Test 3-10 (2).....	10
Figure 3.5. Frame 4 of MASH Crash Test 3-10 (2).....	10
Figure 3.6. Frame 1 of Simulation for MASH Test 3-10.....	11
Figure 3.7. Frame 2 of Simulation for MASH Test 3-10.....	11
Figure 3.8. Frame 3 of Simulation for MASH Test 3-10.....	11
Figure 3.9. Frame 4 of Simulation for MASH Test 3-10.....	11
Figure 3.10. Critical Impact Points.....	12
Figure 4.1. Details of Overlapping Precast Portable Concrete Barriers.	16
Figure 4.2. Overlapping Precast Portable Concrete Barriers prior to Testing.	17
Figure 4.3. In-line View of the Overlapping Precast Portable Concrete Barriers prior to Testing.	17
Figure 4.4. Downstream View of the Overlapping Precast Portable Concrete Barriers prior to Testing.	18
Figure 4.5. Field-Side of the Overlapping Precast Portable Concrete Barriers prior to Testing.	18
Figure 4.6. In-line View of the Overlapping Precast Portable Concrete Barriers at the Overlap prior to Testing.	19
Figure 4.7. Connection Hardware for the Overlapping Precast Portable Concrete Barriers prior to Testing.	19
Figure 7.1. Target CIP for <i>MASH</i> Test 3-10 on Overlapping Precast Portable Concrete Barriers.....	27
Figure 7.2. Overlapping Precast Portable Concrete Barriers/Test Vehicle Geometrics for Test 620281-01-1.	28
Figure 7.3. Overlapping Precast Portable Concrete Barriers/Test Vehicle Impact Location 620281-01-1.....	28
Figure 7.4. Impact Side of Test Vehicle before Test 620281-01-1.....	30
Figure 7.5. Opposite Impact Side of Test Vehicle before Test 620281-01-1.	30
Figure 7.6. Overlapping Precast Portable Concrete Barriers at Impact Location after Test 620281-01-1.	33
Figure 7.7. Upstream View of the Overlapping Precast Portable Concrete Barriers after Test 620281-01-1.	34
Figure 7.8. Impact Side of Test Vehicle after Test 620281-01-1.....	35
Figure 7.9. Rear Impact Side of Test Vehicle after Test 620281-01-1.	35

Figure 7.10. Overall Interior of Test Vehicle after Test 620281-01-1	36
Figure 7.11. Interior of Test Vehicle on Impact Side after Test 620281-01-1	36
Figure 7.12. Summary of Results for <i>MASH</i> Test 3-10 on Overlapping Precast Portable Concrete Barriers.....	39
Figure 8.1. Target CIP for <i>MASH</i> Test 3-11 on Overlapping Precast Portable Concrete Barriers	41
Figure 8.2. Overlapping Precast Portable Concrete Barriers/Test Vehicle Geometrics for Test 620281-01-2.	42
Figure 8.3. Overlapping Precast Portable Concrete Barriers/Test Vehicle Impact Location 620281-01-2.....	42
Figure 8.4. Impact Side of Test Vehicle before Test 620281-01-2.....	44
Figure 8.5. Opposite Impact Side of Test Vehicle before Test 620281-01-2.	44
Figure 8.6. Overlapping Precast Portable Concrete Barriers at Impact Location after Test 620281-01-2.	48
Figure 8.7. Field-Side of the Overlapping Precast Portable Concrete Barriers at Impact after Test 620281-01-2.	48
Figure 8.8. Impact Side of Test Vehicle after Test 620281-01-2.....	49
Figure 8.9. Rear Impact Side of Test Vehicle after Test 620281-01-2.	49
Figure 8.10. Overall Interior of Test Vehicle after Test 620281-01-2.....	50
Figure 8.11. Interior of Test Vehicle on Impact Side after Test 620281-01-2.....	50
Figure 8.12. Summary of Results for <i>MASH</i> Test 3-11 on Overlapping Precast Portable Concrete Barriers.....	53
Figure E.1. Vehicle Properties for Test 620281-01-1.....	104
Figure E.2. Exterior Crush Measurements for Test 620281-01-1.....	105
Figure E.3. Occupant Compartment Measurements for Test 620281-01-1.....	106
Figure E.4. Sequential Photographs for Test 620281-01-1 (Overhead Views).	107
Figure E.5. Sequential Photographs for Test 620281-01-1 (Downstream In-line Views).	108
Figure E.6. Sequential Photographs for Test 620281-01-1 (Upstream Field Side Oblique Views).....	109
Figure E.7. Vehicle Longitudinal Accelerometer Trace for Test 620281-01-1 (Accelerometer Located at Center of Gravity).....	111
Figure E.8. Vehicle Lateral Accelerometer Trace for Test 620281-01-1 (Accelerometer Located at Center of Gravity).....	112
Figure E.9. Vehicle Vertical Accelerometer Trace for Test 620281-01-1 (Accelerometer Located at Center of Gravity).....	113
Figure F.1. Vehicle Properties for Test 620281-01-2.....	115
Figure F.2. Exterior Crush Measurements for Test 620281-01-2.....	116
Figure F.3. Occupant Compartment Measurements for Test 620281-01-2.....	117
Figure F.4. Sequential Photographs for Test 620281-01-2 (Overhead Views).	118
Figure F.5. Sequential Photographs for Test 620281-01-2 (Downstream In-line Views).	119
Figure F.6. Sequential Photographs for Test 620281-01-2 (Upstream Field Side Oblique Views).....	120

Figure F.7. Vehicle Longitudinal Accelerometer Trace for Test 620281-01-2 (Accelerometer Located at Center of Gravity).....	122
Figure F.8. Vehicle Lateral Accelerometer Trace for Test 620281-01-2 (Accelerometer Located at Center of Gravity).....	123
Figure F.9. Vehicle Vertical Accelerometer Trace for Test 620281-01-2 (Accelerometer Located at Center of Gravity).....	124

LIST OF TABLES

	Page
Table 2.1. Summary of Survey Results.....	7
Table 3.1. Comparison of Key Metrics between MASH Test 3-10 Simulation and Crash Test	11
Table 3.2. Comparison of Key Metrics between MASH Test 3-11 Simulation and Crash Test	11
Table 3.3. Maximum RDA (g) at Impact Point E+2ft for MASH Test 3-10 Simulations	13
Table 3.4. Dynamic Deflection (inches) for MASH Test 3-11 Simulations at Impact Point C	13
Table 3.5. Dynamic Deflection (inches) for MASH Test 3-11 Simulations at Impact Point E	14
Table 3.6. Dynamic Deflection (inches) for MASH Test 3-11 Simulations at Impact Point E+2ft.....	14
Table 4.1. Concrete Strength	20
Table 5.1. Test Conditions and Evaluation Criteria Specified for <i>MASH</i> TL-3 Longitudinal Barrier.....	21
Table 5.2. Test Conditions and Evaluation Criteria Specified for <i>MASH</i> TL-3 Longitudinal Barrier.....	22
Table 7.1. Vehicle Measurements for Test 620281-01-1	29
Table 7.2. Weather Conditions 620281-01-1	31
Table 7.3. Events during Test 620281-01-1.....	31
Table 7.4. Impact Conditions for <i>MASH TEST 3-10</i> , Crash Test 620281-01-1	32
Table 7.5. Exit Parameters for <i>MASH TEST 3-10</i> , Crash Test 620281-01-1	32
Table 7.6. Deflection and Working Width of the Overlapping Precast Portable Concrete Barriers for Test 620281-01-1.....	33
Table 7.7. Occupant Compartment Deformation 620281-01-1	37
Table 7.8. Exterior Vehicle Damage 620281-01-1	37
Table 7.9. Occupant Risk Factors for Test 620281-01-1	38
Table 8.1. Vehicle Measurements for Test 620281-01-2	43
Table 8.2. Weather Conditions 620281-01-2	45
Table 8.3. Events during Test 620281-01-2.....	45
Table 8.4. Impact Conditions for <i>MASH TEST 3-11</i> , Crash Test 620281-01-2	46
Table 8.5. Exit Parameters for <i>MASH TEST 3-11</i> , Crash Test 620281-01-2	46
Table 8.6. Deflection and Working Width of the Overlapping Precast Portable Concrete Barriers for Test 620281-01-2.....	47
Table 8.7. Occupant Compartment Deformation 620281-01-2.....	51
Table 8.8. Exterior Vehicle Damage 620281-01-2	51
Table 8.9. Occupant Risk Factors for Test 620281-01-2	52
Table 9.1. Assessment Summary for <i>MASH</i> TL-3 Tests on Overlapping Precast Portable Concrete Barriers.....	55

SI* (MODERN METRIC) CONVERSION FACTORS				
APPROXIMATE CONVERSIONS TO SI UNITS				
Symbol	When You Know	Multiply By	To Find	Symbol
LENGTH				
in	inches	25.4	millimeters	mm
ft	feet	0.305	meters	m
yd	yards	0.914	meters	m
mi	miles	1.61	kilometers	km
AREA				
in ²	square inches	645.2	square millimeters	mm ²
ft ²	square feet	0.093	square meters	m ²
yd ²	square yards	0.836	square meters	m ²
ac	acres	0.405	hectares	ha
mi ²	square miles	2.59	square kilometers	km ²
VOLUME				
fl oz	fluid ounces	29.57	milliliters	mL
gal	gallons	3.785	liters	L
ft ³	cubic feet	0.028	cubic meters	m ³
yd ³	cubic yards	0.765	cubic meters	m ³
NOTE: volumes greater than 1000L shall be shown in m ³				
MASS				
oz	ounces	28.35	grams	g
lb	pounds	0.454	kilograms	kg
T	short tons (2000 lb)	0.907	megagrams (or metric ton")	Mg (or "t")
TEMPERATURE (exact degrees)				
°F	Fahrenheit	5(F-32)/9 or (F-32)/1.8	Celsius	°C
FORCE and PRESSURE or STRESS				
lbf	poundforce	4.45	newtons	N
lbf/in ²	poundforce per square inch	6.89	kilopascals	kPa
APPROXIMATE CONVERSIONS FROM SI UNITS				
Symbol	When You Know	Multiply By	To Find	Symbol
LENGTH				
mm	millimeters	0.039	inches	in
m	meters	3.28	feet	ft
m	meters	1.09	yards	yd
km	kilometers	0.621	miles	mi
AREA				
mm ²	square millimeters	0.0016	square inches	in ²
m ²	square meters	10.764	square feet	ft ²
m ²	square meters	1.195	square yards	yd ²
ha	hectares	2.47	acres	ac
km ²	Square kilometers	0.386	square miles	mi ²
VOLUME				
mL	milliliters	0.034	fluid ounces	oz
L	liters	0.264	gallons	gal
m ³	cubic meters	35.314	cubic feet	ft ³
m ³	cubic meters	1.307	cubic yards	yd ³
MASS				
g	grams	0.035	ounces	oz
kg	kilograms	2.202	pounds	lb
Mg (or "t")	megagrams (or "metric ton")	1.103	short tons (2000lb)	T
TEMPERATURE (exact degrees)				
°C	Celsius	1.8C+32	Fahrenheit	°F
FORCE and PRESSURE or STRESS				
N	newtons	0.225	poundforce	lbf
kPa	kilopascals	0.145	poundforce per square inch	lb/in ²

*SI is the symbol for the International System of Units

CHAPTER 1.

INTRODUCTION

Portable concrete barriers (PCBs) are widely used in temporary traffic control applications to provide positive protection for motorists and roadway workers in work zones. In practice, work zone geometry, staging requirements, and site constraints often necessitate deviations from standard barrier layouts. One common deviation is the use of overlapping free-standing PCBs, in which adjacent barrier runs are offset to provide continuity of protection where standard alignments are not feasible. Overlapping barrier configurations are frequently used to accommodate changes in roadway width, transitions between protected and unprotected areas, construction access openings, and other constrained conditions encountered during work zone operations.

Despite their widespread use, overlapping free-standing PCBs have not been evaluated through full-scale crash testing under the Manual for Assessing Safety Hardware (MASH). As a result, there is limited information available regarding how overlap length, gap between barrier runs, and impact location affect vehicle kinematics, occupant risk, and barrier system performance. While some transportation agencies have developed internal standards or drawings that include overlapping barrier configurations, these recommendations vary considerably and are not supported by crash-testing data.

The absence of research-based guidance for overlapping PCBs creates uncertainty for designers, contractors, and agencies responsible for implementing work zone traffic control plans. To address this gap, the research documented in this report evaluated the safety performance of overlapping free-standing F-shape portable concrete barriers under MASH Test Level 3 conditions. The study combined a survey of current practices, finite element (FE) computer simulations, and full-scale crash testing to identify critical impact conditions, assess system performance, and develop practical recommendations. This report provides recommendations for safer implementation of overlapping PCBs in work zones and identifies areas where additional research may further expand applicable guidance.

CHAPTER 2.

LITERATURE REVIEW AND SURVEY*

The research team conducted a comprehensive search of prior research related to the overlapping of PCBs. No published studies were identified that evaluated overlapping PCBs using computer simulations, full-scale crash testing, or other forms of detailed engineering analysis. Although some research exists on portable concrete barrier performance and barrier terminations, the specific configuration involving overlapping barrier runs has not been directly addressed in the technical literature.

During the literature search, overlapping barriers were identified as a recommended positive protection practice in work zones, particularly in constrained or transitional areas where continuous barrier alignment is not feasible (3). In addition, the literature review identified four standards and guidance documents issued by public transportation agencies that include recommendations for overlapping barrier configurations.

Florida Department of Transportation (FDOT) provides standard drawings illustrating several overlapping configurations using free-standing concrete barriers. A notable recommendation in the FDOT standards is the inclusion of a 2-ft clear space between overlapping barrier runs. Examples of these configurations are shown in Figure 2.1.

The Wisconsin Department of Transportation (WisDOT) also provides standard drawings for overlapping free-standing concrete barriers. WisDOT recommends a minimum overlap of eight barrier segments, corresponding to approximately 100 ft in length, as illustrated in Figure 2.2.

Similarly, the Minnesota Department of Transportation (MnDOT) provides guidance for overlaps involving PCBs and other temporary barrier systems (4). MnDOT recommends a minimum overlap length of 100 ft, with a space between overlapping barrier runs ranging from 6 to 12 inches.

In addition to U.S. practices, Ontario provincial standard drawings include a table specifying minimum overlap lengths and recommended spacing between overlapping barriers, as shown in Figure 2.3. The minimum overlap length is specified as 20 m (65.6 ft) for posted speed limits less than 70 km/h and 32 m (105.0 ft) for posted speed limits of 70

* The opinions/interpretations identified/expressed in this section of the report are outside the scope of TTI Proving Ground's A2LA Accreditation.

km/h or greater, with a recommended gap between overlapping barrier runs ranging from 0.15 m to 0.30 m (6 to 12 in.). For a typical temporary concrete barrier unit measuring approximately 4 m in length, these values correspond to a minimum overlap of five barrier units for speeds below 70 km/h and eight barrier units for speeds of 70 km/h or higher.

Note that none of the standards and recommendations provided by these four states are based on published studies.

The complete standard drawings referenced in this section are provided in Appendix A.

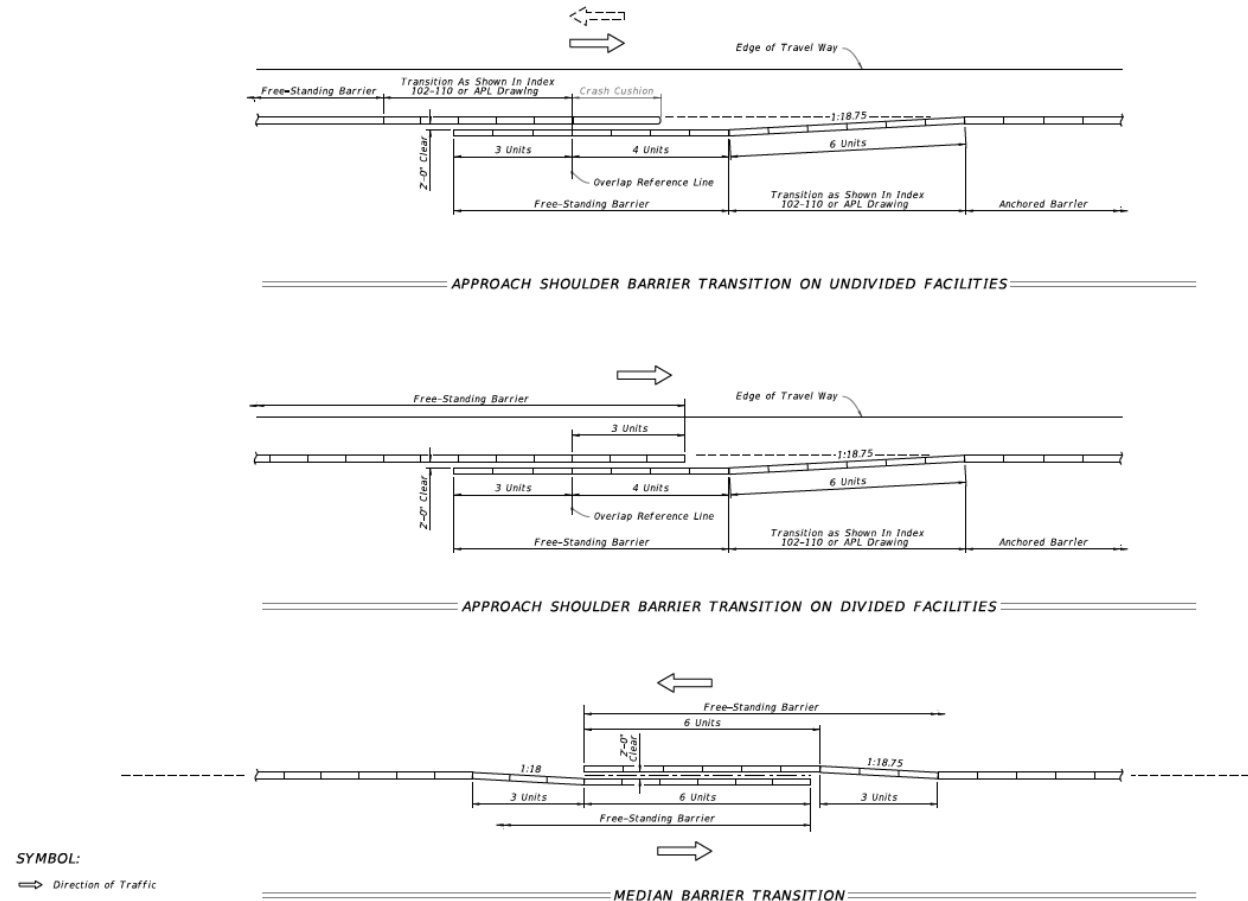


Figure 2.1. FDOT Overlapping PCBs Standards

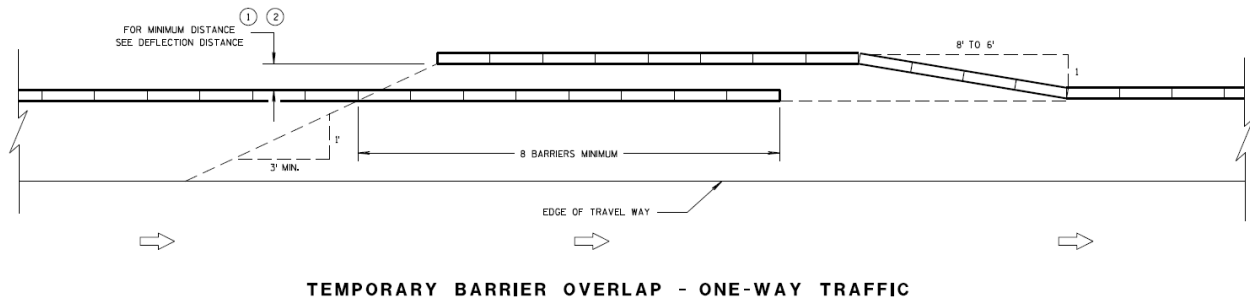


Figure 2.2. WisDOT Overlapping PCBs Standards

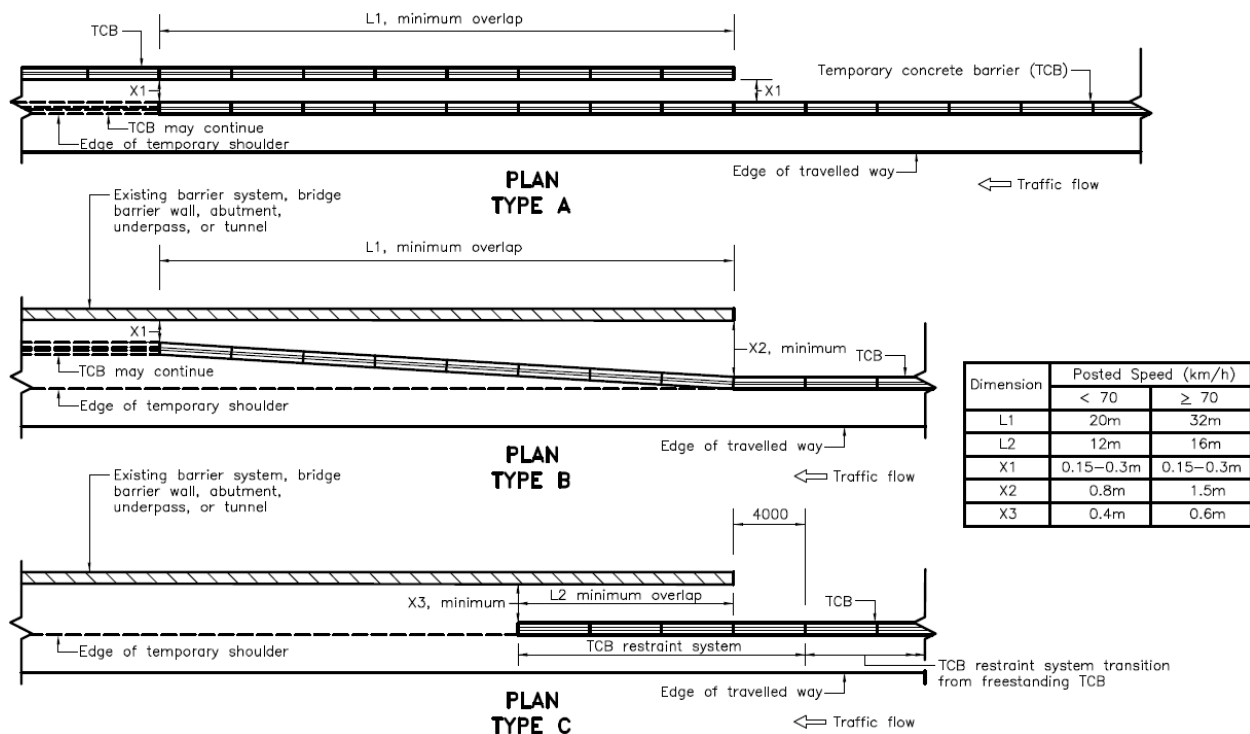


Figure 2.3. Ontario Overlapping PCBs Standards

A survey was conducted with members of the Roadside Safety Pooled Fund to document current state practices related to overlapping PCBs. Technical representatives from participating agencies were asked to provide information regarding the use of overlapping barrier configurations, including whether formal standards exist, the types of barriers and connections typically used, and initial configuration of overlapping barriers runs.

A summary of the key survey questions and responses is presented in Table 2.1. The full survey questionnaire used to collect information is provided in Appendix B.

Survey responses indicated that most responding agencies did not have formal standards specifically addressing overlapping PCB installations. This result highlights the

fact that overlapping barrier installations are often implemented based on project-specific considerations or engineering judgment.

Respondents were asked to identify the type of portable concrete barrier most commonly used when overlapping configurations are installed. The majority of agencies reported use of F-shape portable concrete barriers, with 12 responses identifying this barrier profile. Agencies were also asked how overlapping barrier runs are typically configured in the field. Responses showed variability in practice. Five agencies indicated that barrier runs remain parallel when overlapping is used, while seven agencies reported that barrier runs are initially aligned and then laterally offset to create the overlap.

Table 2.1. Summary of Survey Results

State / Province	Does your state have standards for overlapping PCBs?	Which type of PCB does your DOT use when overlapping?	When overlapping is used, are the barrier runs initially in the same line and then offset to make the overlap, or do they initiate and remain in parallel?	What connection type does your DOT typically use for PCBs when overlapping is used?
Alabama	No	F-Shape	N/A	Pin & loop or Proprietary
Alaska	No	F-Shape	Initiate and remain in parallel	Pin & loop
Colorado	No	F-Shape	Nothing specific	N/A
Florida	Yes	F-Shape	Initiate in same line and offset to overlap	Pin & loop and JJ-Hook
Idaho	No	F-Shape, New Jersey	Initiate in same line and offset to overlap	Pin & loop
Michigan	No	Other	Initiate in same line and offset to overlap, Initiate and remain in parallel	Various
Minnesota	Yes	F-Shape	Initiate and remain in parallel	Pin & loop
Ontario	Yes	F-Shape	Initiate and remain in parallel	Standard is not specific
Pennsylvania	No	Other	No overlapping standard	N/A
TDOT	No	F-Shape, New Jersey	Initiate in same line and offset to overlap	Pin & loop
Texas	No	F-Shape, Single Slope Barrier	Mostly Parallel (unsure)	J-J Hook is probably used most often
Utah	No	F-Shape	Initiate in same line and offset to overlap	Pin & loop
Wisconsin	Yes	F-Shape	Initiate in same line and offset to overlap	Pin & loop
Washington	No	F-Shape, New Jersey	Initiate in same line and offset to overlap	Pin & loop
Total	4 Yes / 10 No	12 F-Shape	5 remain in parallel / 7 offset to overlap	9 Pin & loop Connection

With respect to barrier connections, respondents reported that pin-and-loop connections are most commonly used for overlapping PCB installations. Nine agencies identified pin-and-loop connections as their standard connection type when overlapping barriers are installed.

Overall, the survey results demonstrate that overlapping PCB installations are commonly used across multiple agencies despite the limited availability of formal standards or no MASH crash-tested guidance.

Based on the survey results, the F-shape barrier profile, the pin-and-loop connection type, and the configuration in which barrier runs are laterally offset to create the overlap were selected for further evaluation.

CHAPTER 3.

COMPUTER SIMULATIONS*

Computer simulations using FEA were conducted to evaluate the performance of overlapping portable concrete barrier configurations and to inform the selection of configurations for full-scale crash testing. The simulations were performed using LS-DYNA, a commercially available explicit finite element analysis code widely used for impact and crashworthiness applications. All computational analyses were executed using the High Performance Research Computing (HPRC) resources at Texas A&M University, which enabled the efficient execution of large-scale simulations.

3.1. VALIDATION OF FE MODEL

The finite element model of the barrier used in this study and its interaction with the vehicles were validated using results from previous MASH Test Level 3 full-scale crash tests conducted by TTI involving free-standing PCBs (2). Specifically, the validation effort used the crash test results documented in Test Report No. 607911-1&2, which evaluated a free-standing F-shape portable concrete barrier under MASH Tests 3-10 and 3-11.

The barrier consisted of a 32-in. tall free-standing F-shape barrier with pin-and-loop connections, which is the same barrier profile and connection type selected for evaluation in the overlapping barriers configurations examined in this study. The barrier's FE model is shown in Figure 3.1. For the purposes of this study, the researchers modeled the barrier segments with a rigid material, while the barrier connections were modeled using deformable elastic-plastic materials.

* The opinions/interpretations identified/expressed in this section of the report are outside the scope of TTI Proving Ground's A2LA Accreditation.

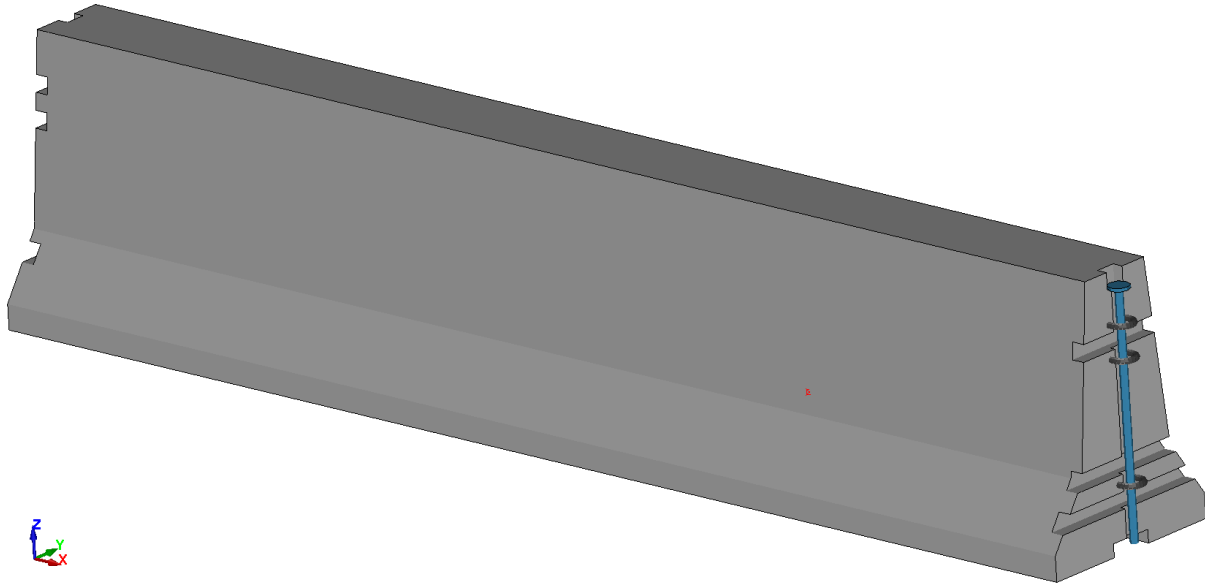


Figure 3.1. FE Model of F-Shape PCB

Researchers performed computer simulations replicating MASH Test 3-10, involving the 1100C small passenger car, and MASH Test 3-11, involving the 2270P pickup truck. Sequential frames from the crash test (Figures Figure 3.2 - Figure 3.5) and the corresponding MASH Test -10 simulation (Figures Figure 3.6 - Figure 3.9) are presented for comparison. A comparison of key simulation results and measured full-scale test data for MASH Test 3-10 and 3-11 are presented in Table 3.1 and Table 3.2, respectively.



Figure 3.2. Frame 1 of MASH Crash Test 3-10 (2)



Figure 3.3. Frame 2 of MASH Crash Test 3-10 (2)



Figure 3.4. Frame 3 of MASH Crash Test 3-10 (2)



Figure 3.5. Frame 4 of MASH Crash Test 3-10 (2)



Figure 3.6. Frame 1 of Simulation for MASH Test 3-10

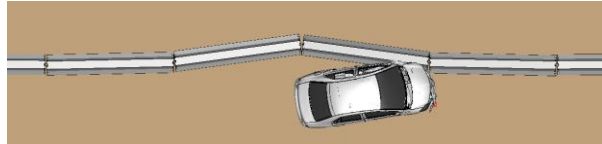


Figure 3.7. Frame 2 of Simulation for MASH Test 3-10

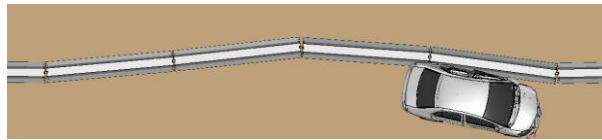


Figure 3.8. Frame 3 of Simulation for MASH Test 3-10

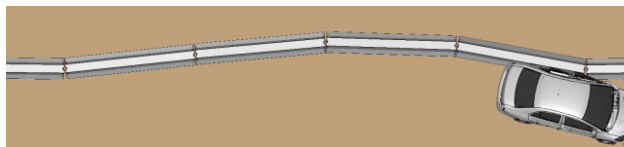


Figure 3.9. Frame 4 of Simulation for MASH Test 3-10

Table 3.1. Comparison of Key Metrics between MASH Test 3-10 Simulation and Crash Test

Parameter	Simulation	Crash Test
Dynamic Deflection	32 in	34 in
Lateral RDA (g)	4.6	4.7
Longitudinal RDA (g)	4.5	9.2
Lateral OIV (ft/s)	22.8	18.4
Longitudinal OIV (ft/s)	28.3	22.6

Table 3.2. Comparison of Key Metrics between MASH Test 3-11 Simulation and Crash Test

Parameter	Simulation	Crash Test
Dynamic Deflection	65 in	63 in
Lateral RDA (g)	12	14.4
Longitudinal RDA (g)	8.8	3.7
Lateral OIV (ft/s)	14.5	18.4
Longitudinal OIV (ft/s)	25.8	12.1

Overall, validation of the system was achieved in a satisfactory manner through comparison of vehicle interaction behavior, with some discrepancies observed, including underprediction of longitudinal RDA for MASH Test 3-10 and longitudinal OIV for MASH Test 3-11.

3.2. SIMULATIONS WITH OVERLAPPING BARRIERS

Using the validated FE models described in Section 3.1, the researchers conducted a comprehensive series of simulations to evaluate the performance of overlapping F-shape PCBs configurations. The objective of this effort was to identify configurations that provide acceptable structural performance and occupant safety under MASH TL-3 impact conditions.

The simulation matrix developed for this study included variations in three primary parameters: gap (clearance) between overlapping barrier runs, impact location, and overlap length. Specifically, three different gap sizes were considered, seven impact points were initially evaluated, and overlap lengths ranging from 1.5 barrier segments to 6 barrier segments were investigated. In total, 82 simulations were conducted as part of this study.

The impact locations evaluated are illustrated in Figure 3.10. Early in the simulation effort, it was determined that impact points A, B, and F were not critical for the overlapping configurations examined and were therefore excluded from further analysis. Impact Point C was located 4.3 ft upstream of the connection for MASH Test 3-11 and 3.6 ft upstream for MASH Test 3-10. Impact Point D was located at the same offsets upstream of the closest connection to the center of the overlap. Although Impact Point D was initially considered potentially critical with respect to occupant safety metrics, subsequent simulations indicated that it did not govern system performance. Impact Point E was defined as 4.3 ft (Test 3-11) and 3.6 ft (Test 3-10) upstream of the end of the overlapping barrier, while Impact Point E + 2 ft was positioned 2 ft downstream of Point E. Parametric simulation results demonstrated that Impact Point E + 2 ft was the most critical location for occupant safety metrics for MASH Test 3-10 impacts involving the small car.

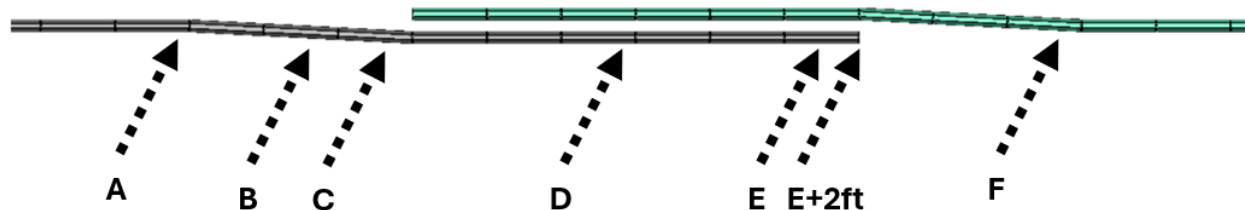


Figure 3.10. Critical Impact Points

For simulations conducted under MASH Test 3-10 conditions with the 1100C small car, the critical response parameters of interest were the occupant risk metrics, particularly ridedown acceleration. The results showed that as the gap between overlapping barrier runs increased from 0 ft to 1 ft and 2 ft, the maximum longitudinal ridedown acceleration increased, exceeding the MASH allowable limit of 20.49 g in all simulations with impact

point at E + 2ft. Table 3.3 presents the maximum ridedown acceleration obtained from selected simulations at the most critical impact location. In Table 3.3, simulation results exceeding the MASH allowable limit are shown in *italics*.

Table 3.3. Maximum RDA (g) at Impact Point E+2ft for MASH Test 3-10 Simulations

Gap	Overlap Length of 1.5 Segments	Overlap Length of 2.5 Segments	Overlap Length of 4 Segments	Overlap Length of 6 Segments
2 ft	25.3	27.0		25.0
1 ft	22.9	21.7	21.1	22.2
0 ft	14.9	15.5	18.8	19.0

As shown in Table 3.3, maintaining zero gap between overlapping barrier runs is necessary to remain below the MASH allowable ridedown acceleration limit. In addition, the simulation results indicated a general trend in which shorter overlap lengths resulted in lower ridedown accelerations. From a constructability, cost, and operational standpoint, an overlap length of 1.5 barrier segments represents an efficient and desirable configuration for work zone applications. It should be noted that the validation effort demonstrated that the simulations tend to underpredict ridedown acceleration; therefore, based on the observed trends, the range of overlapping configurations that satisfy MASH test 3-10 occupant risk criteria is limited.

For simulations conducted under MASH Test 3-11 conditions with the 2270P pickup truck, the primary performance measures of interest were maximum barrier deflection, working width, and overall vehicle stability. Particular attention was given to assessing any potential vehicle instability as the pickup truck interacted with the overlapping barrier system. The simulation results indicated no stability concerns or occupant risk issues for the pickup truck across the configurations evaluated.

Table 3.4, Table 3.5 and Table 3.6 present the maximum rear-barrier deflection in inches obtained for various overlapping configurations at Impact Point C, E and E+2ft, respectively. Based on the constraints imposed by the small car simulations, which limited acceptable configurations to those with 1.5 barrier segment overlap and zero gap, the pickup truck simulations show that the maximum deflection for this configuration occurs at Impact Point C, with a value of 77 in (Table 3.4).

Table 3.4. Dynamic Deflection (inches) for MASH Test 3-11 Simulations at Impact Point C

Gap	Overlap Length of 1.5 Segments	Overlap Length of 2.5 Segments	Overlap Length of 4 Segments	Overlap Length of 6 Segments
2 ft	47.4		57.3	44.5
1 ft				50.0
0 ft	77.0	76.8		63.3

Table 3.5. Dynamic Deflection (inches) for MASH Test 3-11 Simulations at Impact Point E

Gap	Overlap Length of 1.5 Segments	Overlap Length of 2.5 Segments	Overlap Length of 4 Segments	Overlap Length of 6 Segments
2 ft	54.0	56.5	62.6	
1 ft		51.9		
0 ft	46.0	45.0	45.3	39.1

Table 3.6. Dynamic Deflection (inches) for MASH Test 3-11 Simulations at Impact Point E+2ft

Gap	Overlap Length of 1.5 Segments	Overlap Length of 2.5 Segments	Overlap Length of 4 Segments	Overlap Length of 6 Segments
2 ft	54.0	56.5	62.6	
1 ft		51.9		
0 ft	46.0	45.0	45.3	39.1

3.3. RECCOMENDED CONDIFURATION FOR FULL-SCALE CRASH TESTING

Based on the finite element simulation results presented in Section 3.2, the configuration consisting of a 1.5-barrier-length overlap with no gap between parallel barrier runs was selected for full-scale crash testing under MASH TL-3 conditions. For the pickup truck test, Impact Point C was selected to evaluate maximum barrier deflection and working width, while for the small-car test, Impact Point E + 2 ft was selected to assess compliance with MASH occupant safety criteria.

CHAPTER 4.

SYSTEM DETAILS

4.1. TEST ARTICLE AND INSTALLATION DETAILS

The installation was approximately 383 feet and 2 inches long, consisting of thirty-two reinforced concrete barriers. These barriers were F-shape, 32 inches tall and 12.5 feet long. The first sixteen barriers and the last sixteen barriers were connected to adjoining barriers with pin and loop connections. The barriers were free-standing (not secured to the pavement).

For the first run of barriers, barriers 1 through 11 were placed parallel to traffic, barrier 12 through 13 were placed at a 12:1 lateral offset toward traffic, and barrier 15 and 16 were parallel to traffic. The lateral offset between the first eleven and the last two segments of this run was 37-3/4 inches.

For the second run of barriers, barriers 17 and 18 were placed on the field side of barriers 15 and 16, with the upstream end of barrier 17 aligned with the midpoint of barrier 15. Barriers 19-21 were angled toward the traffic side parallel to barriers 12-14, and barriers 22-32 were parallel to traffic, offset 51 inches toward the traffic side from barriers 1-11.

Figure 4.1 presents the overall information on the Overlapping Precast Portable Concrete Barriers, and Figure 4.2 thru Figure 4.7 provide photographs of the installation. Appendix C provides further details on the Overlapping Precast Portable Concrete Barriers. Drawings were provided by the Texas A&M Transportation Institute (TTI) Proving Ground, and assembly of the barrier configuration was performed by TTI Proving Ground personnel.

4.2. DESIGN MODIFICATIONS DURING TESTS

No modifications were made to the installation during the testing phase.

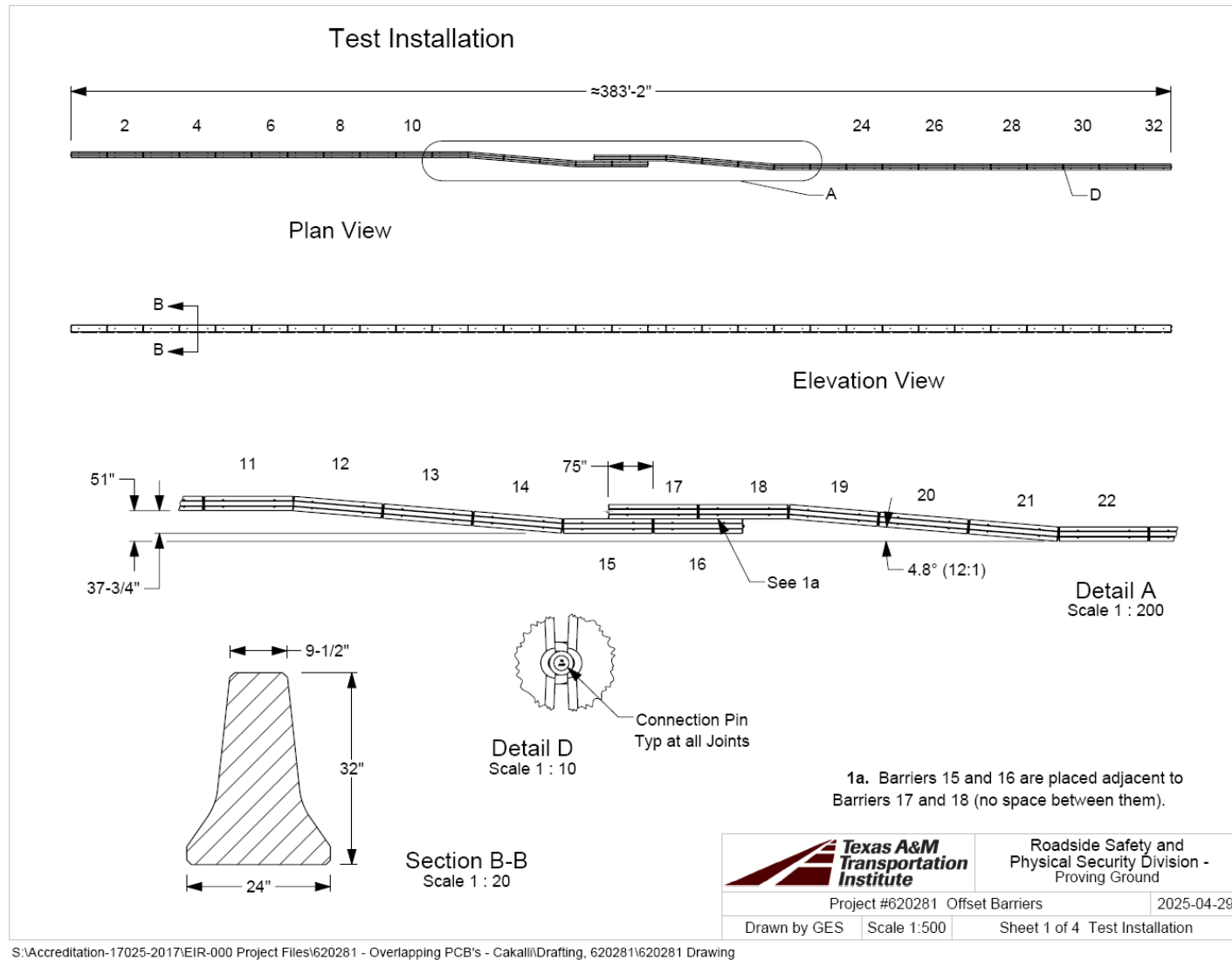


Figure 4.1. Details of Overlapping Precast Portable Concrete Barriers.



Figure 4.2. Overlapping Precast Portable Concrete Barriers prior to Testing.



Figure 4.3. In-line View of the Overlapping Precast Portable Concrete Barriers prior to Testing.



Figure 4.4. Downstream View of the Overlapping Precast Portable Concrete Barriers prior to Testing.



Figure 4.5. Field-Side of the Overlapping Precast Portable Concrete Barriers prior to Testing.



Figure 4.6. In-line View of the Overlapping Precast Portable Concrete Barriers at the Overlap prior to Testing.



Figure 4.7. Connection Hardware for the Overlapping Precast Portable Concrete Barriers prior to Testing.

4.3. MATERIAL SPECIFICATIONS

Appendix D provides material certification documents for the materials used to install/construct the Overlapping Precast Portable Concrete Barriers. Table 4.1 shows the average compressive strengths of concrete core samples taken on the impacted barriers after testing was completed.

Table 4.1. Concrete Strength

Location	Design Strength (psi)	Avg. Strength (psi)
Two barriers from each test	5000	7668

CHAPTER 5.

TEST REQUIREMENTS AND EVALUATION CRITERIA

5.1. CRASH TEST PERFORMED/MATRIX

Table 5.1 shows the test conditions and evaluation criteria for *MASH* TL-3 for Longitudinal Barrier.

Table 5.1. Test Conditions and Evaluation Criteria Specified for *MASH* TL-3 Longitudinal Barrier

Test Designation	Test Vehicle	Impact Speed (mi/h)	Impact Angle (°)	Evaluation Criteria
3-10	1100C	62	25	A, D, F, H, I
3-11	2270P	62	25	A, D, F, H, I

The crash tests and data analysis procedures were in accordance with guidelines presented in *MASH*. Chapter 6 presents brief descriptions of these procedures.

5.2. EVALUATION CRITERIA

The appropriate safety evaluation criteria from Tables 2-2 and 5-1 of *MASH* were used to evaluate the crash tests reported herein. **Error! Reference source not found.** lists the test conditions and evaluation criteria required for *MASH* TL-3, and Table 5.2 provides detailed information on the evaluation criteria.

Table 5.2. Test Conditions and Evaluation Criteria Specified for *MASH* TL-3 Longitudinal Barrier

Evaluation Factors	Evaluation Criteria
A.	Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.
D.	Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present undue hazard to other traffic, pedestrians, or personnel in a work zone. Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of <i>MASH</i> .
F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.
H.	Occupant impact velocities (OIV) should satisfy the following limits: Preferred value of 30 ft/s, or maximum allowable value of 40 ft/s.
I.	The occupant ridedown accelerations should satisfy the following: Preferred value of 15.0 g, or maximum allowable value of 20.49 g.

CHAPTER 6.

TEST CONDITIONS

6.1. TEST FACILITY

The full-scale crash tests reported herein were performed at the TTI Proving Ground, an International Standards Organization (ISO)/International Electrotechnical Commission (IEC) 17025-accredited laboratory with American Association for Laboratory Accreditation (A2LA) Mechanical Testing Certificate 2821.01. The full-scale crash tests were performed according to TTI Proving Ground quality procedures, as well as *MASH* guidelines and standards.

The test facilities of the TTI Proving Ground are located on The Texas A&M University System RELLIS Campus, which consists of a 3100-acre complex of research and training facilities situated 10 mi northwest of the flagship campus of Texas A&M University. The site, formerly a United States Army Air Corps base, has large expanses of concrete runways and parking aprons well suited for experimental research and testing in the areas of vehicle performance and handling, vehicle-roadway interaction, highway pavement durability and efficacy, and roadside safety hardware and perimeter protective device evaluation. The sites selected for construction and testing are on an out-of-service apron/runway. The apron/runway consists of an unreinforced jointed-concrete pavement in 12.5-ft × 15-ft blocks nominally 6 inches deep. The aprons were built in 1942, and the joints have some displacement but are otherwise flat and level.

6.2. VEHICLE TOW AND GUIDANCE SYSTEM

For the testing utilizing the 1100C and 2270P vehicles, each was towed into the test installation using a steel cable guidance and reverse tow system. A steel cable for guiding the test vehicle was tensioned along the path, anchored at each end, and threaded through an attachment to the front wheel of the test vehicle. An additional steel cable was connected to the test vehicle, passed around a pulley near the impact point and through a pulley on the tow vehicle, and then anchored to the ground such that the tow vehicle moved away from the test site. A 2:1 speed ratio between the test and tow vehicle existed with this system. Just prior to impact with the installation, the test vehicle was released and ran unrestrained. The vehicle remained freewheeling (i.e., no steering or braking inputs) until it cleared the immediate area of the test site.

6.3. DATA ACQUISITION SYSTEMS

6.3.1. Vehicle Instrumentation and Data Processing

Each test vehicle was instrumented with a self-contained onboard data acquisition system. The signal conditioning and acquisition system is a multi-channel data acquisition system (DAS) produced by Diversified Technical Systems Inc. The accelerometers, which measure the x, y, and z axis of vehicle acceleration, are strain gauge type with linear millivolt output proportional to acceleration. Angular rate sensors, measuring vehicle roll, pitch, and yaw rates, are ultra-small, solid-state units designed for crash test service. The data acquisition hardware and software conform to the *MASH* recommended version of SAE J211, Instrumentation for Impact Test. Each of the channels is capable of providing precision amplification, scaling, and filtering based on transducer specifications and calibrations. During the test, data are recorded from each channel at a rate of 10,000 samples per second with a resolution of one part in 65,536. Once data are recorded, internal batteries back these up inside the unit in case the primary battery cable is severed. Initial contact of the pressure switch on the vehicle bumper provides a time zero mark and initiates the recording process. After each test, the data are downloaded from the DAS unit into a laptop computer at the test site. The Test Risk Assessment Program (TRAP) software then processes the raw data to produce detailed reports of the test results.

Each DAS is returned to the factory annually for complete recalibration and to ensure that all instrumentation used in the vehicle conforms to the specifications outlined by SAE J211. All accelerometers are calibrated annually by means of an ENDEVCO 2901 precision primary vibration standard. This standard and its support instruments are checked annually and receive a calibration traceable to the International System of Units (SI). Measurement Uncertainties have been determined for critical parameters involved in this testing, and are available upon request by the Sponsor.

TRAP uses the DAS-captured data to compute the occupant to vehicle contact impact velocities, time of occupant to vehicle contact after vehicle impact, and highest 10-millisecond (ms) average ridedown acceleration. TRAP calculates change in vehicle velocity at the end of a given impulse period. In addition, maximum average accelerations over 50-ms intervals in each of the three directions are computed. The data from the vehicle-mounted accelerometers are collected and filtered with an SAE Class 180 low-pass digital filter. Various filters to enhance readability are used for plotting acceleration versus time curves for the longitudinal, lateral, and vertical directions using TRAP.

TRAP uses the data from the yaw, pitch, and roll rate transducers to compute angular displacement in degrees at 0.0001-s intervals, and then plots yaw, pitch, and roll versus time. These displacements are in reference to the vehicle-fixed coordinate system with the initial position and orientation being initial impact. Measurement Uncertainties have been determined for critical parameters involved in this testing, and are available upon request by the Sponsor.

6.3.2. Anthropomorphic Dummy Instrumentation

An Alderson Research Laboratories Hybrid II, 50th percentile male anthropomorphic dummy, restrained with lap and shoulder belts, was placed in the front seat on the impact side of the 1100C vehicle. The dummy was not instrumented.

According to *MASH*, use of a dummy in the 2270P vehicle is optional, and no dummy was used in the test.

6.3.3. Photographic Instrumentation Data Processing

Photographic coverage of each test included 3 digital high-speed cameras:

- One placed overhead with a field of view perpendicular to the ground and directly over the impact point.
- One placed with a field of view parallel to and aligned with the installation at the downstream end.
- One placed at an oblique angle upstream from the installation on the field side.

A flashbulb on the impacting vehicle was activated by a pressure-sensitive tape switch to indicate the instant of contact with the Overlapping Precast Portable Concrete Barriers. The flashbulb was visible from each camera. The video files from these digital high-speed cameras were analyzed to observe phenomena occurring during the collision and to obtain time-event, displacement, and angular data. A digital camera recorded and documented conditions of each test vehicle and the installation before and after the test.

CHAPTER 7.

***MASH*TEST 3-10 (CRASH TEST 620281-01-1)**

7.1. CRITICAL IMPACT POINT LOCATION

The Critical Impact Point (CIP) for this test was 19.2 inches [1.6 feet] upstream from the downstream edge of barrier 16 at 25 degrees. The target CIP for this test was determined using the information provided in *MASH* Section 2.2.1 and *MASH* Section 2.3.2. Figure 7.1 **Error! Reference source not found.** shows the target CIP for test 620281-01-1. Figure 7.2 and Figure 7.3 depict the vehicle at the CIP prior to test 620281-01-1.

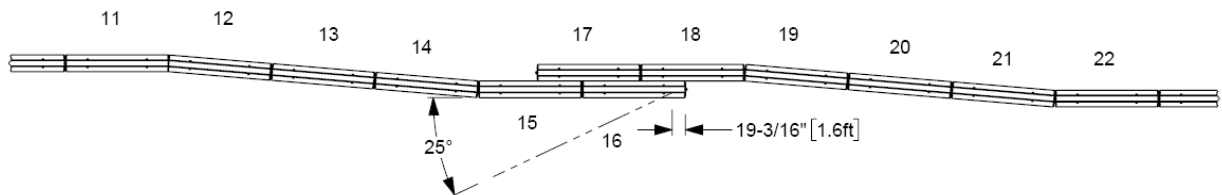


Figure 7.1. Target CIP for *MASH* Test 3-10 on Overlapping Precast Portable Concrete Barriers



Figure 7.2. Overlapping Precast Portable Concrete Barriers/Test Vehicle Geometrics for Test 620281-01-1.



Figure 7.3. Overlapping Precast Portable Concrete Barriers/Test Vehicle Impact Location 620281-01-1.

7.2. TEST VEHICLE DETAILS PRIOR TO IMPACT

Table 7.1 shows the vehicle measurements. Figure 7.4 and Figure 7.5 show the 2018 Nissan Versa used for the crash test. Figure E.1 in Appendix E.1 gives additional dimensions and information on the vehicle.

Table 7.1. Vehicle Measurements for Test 620281-01-1

Test Parameter	Specification	Tolerance	Measured
Dummy Mass (if applicable) ^a (lb)	165	N/A	165
Inertial Mass (lb)	2420	±55	2453
Gross Static ^a Mass (lb)	2585	±55	2618
Wheelbase (inches)	98	±5	102.4
Front Overhang (inches)	35	±4	32.5
Overall Length (inches)	169	±8	175.4
Overall Width (inches)	65	±3	66.7
Hood Height (inches)	28	±4	30.5
Track Width ^b (inches)	59	±2	58.4
CG aft of Front Axle ^c (inches)	39	±4	41.6
CG above Ground ^{c,d} (inches)	N/A	N/A	N/A

Note: N/A = not applicable; CG = center of gravity.

^a If a dummy is used, the gross static vehicle mass should be increased by the mass of the dummy.

^b Average of front and rear axles.

^c For test inertial mass.

^d 2270P vehicle must meet minimum CG height requirement.



Figure 7.4. Impact Side of Test Vehicle before Test 620281-01-1.



Figure 7.5. Opposite Impact Side of Test Vehicle before Test 620281-01-1.

7.3. TEST DESCRIPTION

7.3.1. Weather Conditions

Table 7.2 provides the weather conditions for 620281-01-1. Values for wind direction and vehicle travel are in reference to the degrees on a compass, with North being 0 degrees.

Table 7.2. Weather Conditions 620281-01-1

Date of Test	2025-10-16
Wind Speed	2 mi/h
Wind Direction	134°
Temperature	77°F
Relative Humidity	68 %
Vehicle Traveling	325°

7.3.2. Test Events

Table 7.3 lists events that occurred during Test 620281-01-1. The figures in Appendix E.2 present sequential photographs during the test.

Table 7.3. Events during Test 620281-01-1

Time (seconds)	Events
0.0000	Vehicle impacted the installation
0.0250	Vehicle began to redirect
0.0750	Vehicle contacted barrier 18, approximately 12 inches upstream from the joint of barriers 18 and 19
0.1100	Vehicle began to push barrier 19 toward the field-side
0.1470	Right front tire began to lift off the ground
0.1580	Right rear tire began to lift off the ground
0.2280	Vehicle was parallel with installation
0.3470	Concrete of upstream traffic-side of Barrier 19 began to spall
0.6140	Left front tire contacted the ground
0.8950	Left rear tire contacted the ground

7.4. TEST ACTUAL IMPACT CONDITIONS

Table 7.4 lists the details of the *MASH* impact conditions for this test and Table 7.5 lists the exit parameters.

Table 7.4. Impact Conditions for *MASH TEST 3-10*, Crash Test 620281-01-1

Test Parameter	Specification	Tolerance	Measured
Impact Speed (mi/h)	62	±2.5	62.2
Impact Angle (°)	25	±1.5	24.7
Impact Severity (kip-ft)	51	≥51	55.4
Impact Location	19.2 inches [1.6 feet] upstream from the downstream edge of barrier 16	±1 foot (12 inches)	17.0 inches [1.4 feet] upstream from the downstream edge of barrier 16

Table 7.5. Exit Parameters for *MASH TEST 3-10*, Crash Test 620281-01-1

Exit Parameter	Measured
Speed	Out of frame - Not measurable
Trajectory	Out of frame - Not measurable
Heading	Out of frame - Not measurable
Brakes applied post impact	Brakes not applied
Vehicle at rest position	190 ft downstream of impact point 45 ft to the traffic side
Comments:	Vehicle remained upright and stable. The vehicle met the exit box criteria ^a by crossing the exit box on the downstream end

^aPer the *MASH* guidelines in Section 5.2.3, the exit box for the 1100C used in this test was 15.1 ft toward the traffic side as measured from the traffic side toe of the barrier and 32.8 ft downstream from loss of contact.

7.5. DAMAGE TO TEST INSTALLATION

The downstream end of barrier 16 had abrasions and spalling, with a significant spall on the field side of barrier 16 at its base. Barrier 18 had some minor spalling on its upstream end. Barriers 18 and 19 at their joint had spalling at their base on the traffic side, and there was additional spalling on barrier 19 at its upper loop connection. Barriers 20 and 21 at their joint had spalling at their base on the traffic side. Table 7.6 describes the deflection and working width of the Overlapping Precast Portable Concrete Barriers. Figure 7.6 and Figure 7.7 show the damage to the Overlapping Precast Portable Concrete Barriers.

Table 7.6. Deflection and Working Width of the Overlapping Precast Portable Concrete Barriers for Test 620281-01-1

Test Parameter	Measured
Permanent Deflection/Location	29.0 inches toward field side, at the joint of barriers 18 and 19
Dynamic Deflection	29.4 inches toward field side at the top of the upstream field side corner of barrier 19
Working Width ^a and Height	53.5 inches, at a height of 0.0 inches at the field side toe of barrier 19 at the joint of barriers 18 and 19

^a Per *MASH*, "The working width is the maximum dynamic lateral position of any major part of the system or vehicle. These measurements are all relative to the pre-impact traffic face of the test article." In other words, working width is the total barrier width plus the maximum dynamic intrusion of any portion of the barrier or test vehicle past the field side edge of the barrier.



Figure 7.6. Overlapping Precast Portable Concrete Barriers at Impact Location after Test 620281-01-1.



Figure 7.7. Upstream View of the Overlapping Precast Portable Concrete Barriers after Test 620281-01-1.

7.6. DAMAGE TO TEST VEHICLE

Figure 7.8 and Figure 7.9 show the damage sustained by the vehicle. Figure 7.10 and Figure 7.11 show the interior of the test vehicle. Table 7.7 and Table 7.8 provide details on the occupant compartment deformation and exterior vehicle damage. Figure E.2 and Figure E.3 in Appendix E.1 provide exterior crush and occupant compartment measurements.



Figure 7.8. Impact Side of Test Vehicle after Test 620281-01-1.

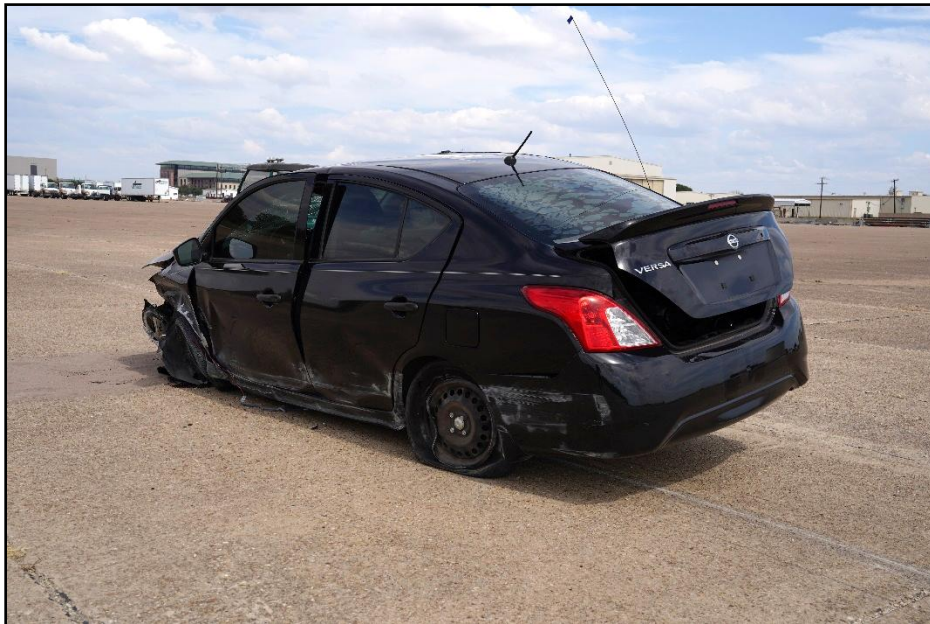


Figure 7.9. Rear Impact Side of Test Vehicle after Test 620281-01-1.



Figure 7.10. Overall Interior of Test Vehicle after Test 620281-01-1.



Figure 7.11. Interior of Test Vehicle on Impact Side after Test 620281-01-1.

Table 7.7. Occupant Compartment Deformation 620281-01-1

Test Parameter	Specification (inches)	Measured (inches)
Roof	≤4.0	0.0
Windshield	≤3.0	0.0
A and B Pillars	≤5.0 overall/≤3.0 lateral	0.0
Foot Well/Toe Pan	≤9.0	1.5
Floor Pan/Transmission Tunnel	≤12.0	0.5
Side Front Panel	≤12.0	1.5
Front Door (above Seat)	≤9.0	0.0
Front Door (below Seat)	≤12.0	0.0

Table 7.8. Exterior Vehicle Damage 620281-01-1

Test Parameter	Details
Side Windows	The side windows remained intact
Maximum Exterior Deformation	19 inches in the front plane at the left front corner at bumper height
VDS	11LFQ4
CDC	11FLAW3
Fuel Tank Damage	None
Description of Damage to Vehicle:	The front bumper, grill, and left headlight dislodged. The radiator and its support fractured. The left front fender, left front door, left rear door, and left rear quarter panel were deformed. The wheels on the left side deformed and their tires ruptured. The windshield was cracked on the left side, but there were no holes or tears in the laminate. The top of the left front door and left rear door separated from the body of the car creating openings of 3.5 inches and 0.5 inches respectively.

7.7. OCCUPANT RISK FACTORS

Data from the accelerometers were digitized for evaluation of occupant risk, and the results are shown in Table 7.9. Figure E.7 through Figure E.9 in Appendix E.3 show acceleration versus time traces.

Table 7.9. Occupant Risk Factors for Test 620281-01-1

Test Parameter	Specification ^a	Measured	Time
OIV, Longitudinal (ft/s)	≤40.0 ≤30.0	13.5	0.1282 seconds on left side of interior
OIV, Lateral (ft/s)	≤40.0 ≤30.0	17.6	0.1282 seconds on left side of interior
Ridedown, Longitudinal (g)	≤20.49 ≤15.0	9.3	0.1282 - 0.1382 seconds
Ridedown, Lateral (g)	≤20.49 ≤15.0	19.2	0.1307 - 0.1407 seconds
Theoretical Head Impact Velocity (THIV) (m/s)	N/A	5.7	0.1248 seconds on left side of interior
Acceleration Severity Index	N/A	1.6	0.1315 - 0.1815 seconds
50-ms Moving Avg. Accelerations (MA) Longitudinal (g)	N/A	-8.0	0.1135 - 0.1635 seconds
50-ms MA Lateral (g)	N/A	10.8	0.1148 - 0.1648 seconds
50-ms MA Vertical (g)	N/A	-4.5	0.1066 - 0.1566 seconds
Roll (°)	≤75	N/A	N/A
Pitch (°)	≤75	N/A	N/A
Yaw (°)	N/A	N/A	N/A

^a. *Values in italics are the preferred MASH values*

Note: N/A = Not Applicable

Due to equipment failure, accurate roll, pitch, and yaw angles could not be calculated. Visual inspection of the high-speed video indicates that roll and pitch never met or exceeded the specified maximum of 75 degrees.

7.8. TEST SUMMARY

Figure 7.12 summarizes the results of MASH Test 620281-01-1.



0.000 s



0.2000 s



0.4000 s



0.6000s

GENERAL INFORMATION

Test Agency:	Texas A&M Transportation Institute (TTI)
Test Standard/Test No.:	MASH 2016, Test 3-10
Project No.:	620281-01-1
Test Date:	2025-10-16

TEST ARTICLE

Type:	Longitudinal Barrier
Name:	Overlapping Precast Portable Concrete Barriers
Length:	383 feet 2 inches
Key Materials:	32 f-shape portable concrete barriers
Soil Type and Condition:	Concrete, dry

TEST VEHICLE

Type/Designation:	1100C
Year, Make and Model:	2018 Nissan Versa
Inertial Mass:	2453 lb
Dummy Mass:	165 lb
Gross Static Mass:	2618 lb

IMPACT CONDITIONS

Impact Speed:	62.2 mi/h
Impact Angle:	24.7°
Impact Location:	17.0 inches [1.4 feet] upstream from the downstream edge of barrier 16
Impact Severity:	55.4 kip-ft

EXIT CONDITIONS

Exit Speed:	Out of frame - Not measurable
Trajectory/Heading Angle:	Out of frame - Not measurable
Exit Box Criteria:	The vehicle met the exit box criteria

Stopping Distance:	190 ft downstream 45 ft to the traffic side
---------------------------	--

TEST ARTICLE DEFLECTIONS

Dynamic:	29.4 inches
Permanent:	29 inches
Working Width:	53.5 inches
Working Width Height:	0.0 inches

VEHICLE DAMAGE

VDS:	11LFQ4
CDC:	11FLAW3
Max Exterior Deformation:	19 inches in the front plane at the left front corner at bumper height
Max Occupant Compartment Deformation:	1.5 inches in the foot well/toe pan

OCCUPANT RISK VALUES

Longitudinal OIV:	13.5 ft/s
Lateral OIV:	17.6 ft/s
Longitudinal Ridedown:	9.3 g
Lateral Ridedown:	19.2 g
THIV:	5.7 m/s
ASI:	1.6
Max 50ms Longitudinal:	-8.0 g
Max 50ms Lateral:	10.8 g
Max 50ms Vertical:	-4.5 g
Max Roll:	Not measurable
Max Pitch:	Not measurable
Max Yaw:	Not measurable

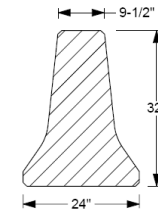
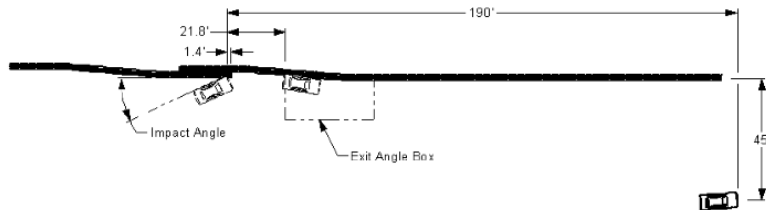


Figure 7.12. Summary of Results for MASH Test 3-10 on Overlapping Precast Portable Concrete Barriers.

CHAPTER 8.

***MASH*TEST 3-11 (CRASH TEST 620281-01-2)**

8.1. CRITICAL IMPACT POINT LOCATION

The Critical Impact Point (CIP) for this test was 51.6 inches [4.3 feet] upstream from the joint between barriers 14 and 15 at 25 degrees. The target CIP for this test was determined using the information provided in *MASH* Section 2.2.1 and *MASH* Section 2.3.2. Figure 8.1 shows the target CIP for test 620281-01-2. Figure 8.2 and Figure 8.3 depict the vehicle at the CIP prior to test 620281-01-2.

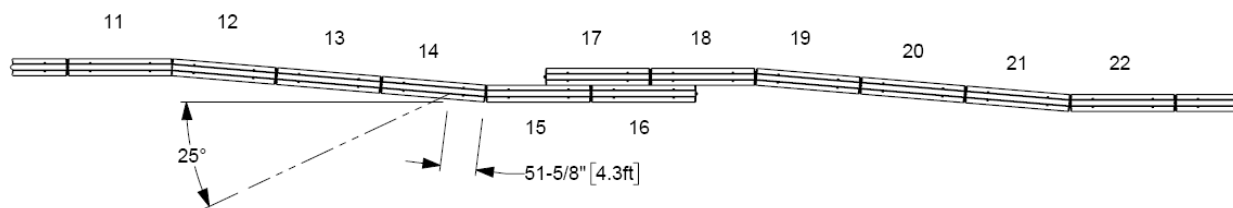


Figure 8.1. Target CIP for *MASH* Test 3-11 on Overlapping Precast Portable Concrete Barriers



Figure 8.2. Overlapping Precast Portable Concrete Barriers/Test Vehicle Geometrics for Test 620281-01-2.



Figure 8.3. Overlapping Precast Portable Concrete Barriers/Test Vehicle Impact Location 620281-01-2.

8.2. TEST VEHICLE DETAILS PRIOR TO IMPACT

Table 8.1 shows the vehicle measurements. Figure 8.4 and Figure 8.5 show the 2019 RAM 1500 used for the crash test. Figure F.1 in Appendix F.1 gives additional dimensions and information on the vehicle.

Table 8.1. Vehicle Measurements for Test 620281-01-2

Test Parameter	Specification	Tolerance	Measured
Dummy Mass (if applicable) ^a (lb)	165	N/A	N/A
Inertial Mass (lb)	5000	±110	5044
Gross Static ^a Mass (lb)	5000	±110	5044
Wheelbase (inches)	148	±12	140.5
Front Overhang (inches)	39	±3	40.0
Overall Length (inches)	237	±13	227.5
Overall Width (inches)	78	±2	78.5
Hood Height (inches)	43	±4	46.0
Track Width ^b (inches)	67	±1.5	68.3
CG aft of Front Axle ^c (inches)	63	±4	61.4
CG above Ground ^{c,d} (inches)	≥28	N/A	28.8

Note: N/A = not applicable; CG = center of gravity.

^a If a dummy is used, the gross static vehicle mass should be increased by the mass of the dummy.

^b Average of front and rear axles.

^c For test inertial mass.

^d 2270P vehicle must meet minimum CG height requirement.



Figure 8.4. Impact Side of Test Vehicle before Test 620281-01-2.



Figure 8.5. Opposite Impact Side of Test Vehicle before Test 620281-01-2.

8.3. TEST DESCRIPTION

8.3.1. Weather Conditions

Table 8.2 provides the weather conditions for 620281-01-2. Values for wind direction and vehicle travel are in reference to the degrees on a compass, with North being 0 degrees.

Table 8.2. Weather Conditions 620281-01-2

Date of Test	2025-10-23
Wind Speed	3 mi/h
Wind Direction	169°
Temperature	79°F
Relative Humidity	74 %
Vehicle Traveling	325°

8.3.2. Test Events

Table 8.3 lists events that occurred during Test 620281-01-2. The figures in Appendix F.2 present sequential photographs during the test.

Table 8.3. Events during Test 620281-01-2

Time (seconds)	Events
0.0000	Vehicle impacted the installation
0.0240	Barrier 14 began to lean toward the field-side.
0.0290	Vehicle began to redirect
0.0360	Barrier 15 began to move toward the field-side
0.0730	Barrier 17 began to slide toward the field-side
0.0810	Front right tire began to lift off the ground
0.2290	Vehicle was parallel with installation
0.2380	Rear right tire began to lift off the ground

8.4. TEST ACTUAL IMPACT CONDITIONS

Table 8.4 lists the details of the *MASH* impact conditions for this test and Table 8.5 lists the exit parameters.

Table 8.4. Impact Conditions for *MASH TEST 3-11*, Crash Test 620281-01-2

Test Parameter	Specification	Tolerance	Measured
Impact Speed (mi/h)	62	±2.5	62.1
Impact Angle (°)	25	±1.5	25.5
Impact Severity (kip-ft)	106	≥106	120.5
Impact Location	51.6 inches [4.3 feet] upstream from the joint between barriers 14 and 15	±1 foot (12 inches)	53.6 inches [4.5 feet] upstream from the joint between barriers 14 and 15

Table 8.5. Exit Parameters for *MASH TEST 3-11*, Crash Test 620281-01-2

Exit Parameter	Measured
Speed	Out of frame - Not measurable
Trajectory	Out of frame - Not measurable
Heading	Out of frame - Not measurable
Brakes applied post impact	Brakes not applied
Vehicle at rest position	120 ft downstream of impact point 41 ft to the traffic side
Comments:	Vehicle remained upright and stable. The vehicle met the exit box criteria ^a by crossing the exit box on the downstream end

^aPer the *MASH* guidelines in Section 5.2.3, the exit box for the 2270P used in this test was 16.8 ft toward the traffic side as measured from the traffic side toe of the barrier and 32.8 ft downstream from loss of contact.

8.5. DAMAGE TO TEST INSTALLATION

The field side base of the barriers at the joint of barriers 12 and 13, and 13 and 14 were spalled. The traffic side base of the barriers at the joint of barriers 14 and 15 had large spalls, and barrier 15 had cracks which extended through the barrier at 42 and 72 inches from its upstream end. The traffic and field side base of the barriers at the joint of barriers 15 and 16 were spalled. Barrier 16 had additional spalling on the field side 18 inches from its downstream end. Barrier 17 had spalling with exposed rebar on its traffic side near its downstream end. Barrier 18 had spalling on the field side at both ends, and barrier 19 had spalling on its field side on its upstream end. Table 8.6 describes the

deflection and working width of the Overlapping Precast Portable Concrete Barriers. Figure 8.6 and Figure 8.7 show the damage to the Overlapping Precast Portable Concrete Barriers.

Table 8.6. Deflection and Working Width of the Overlapping Precast Portable Concrete Barriers for Test 620281-01-2

Test Parameter	Measured
Permanent Deflection/Location	87.0 inches toward field side, at the joint of barriers 14 and 15
Dynamic Deflection (upstream half of the installation)	88.4 toward field side at the top of barrier 15 at the joint of barriers 14 and 15
Dynamic Deflection (downstream half of the installation)	94.7 inches toward field side at the upstream end of barrier 17
Working Width ^a and Height	159.8 inches, at a height of 0.0 inches at the toe of barrier 17 on the upstream end

^a Per *MASH*, "The working width is the maximum dynamic lateral position of any major part of the system or vehicle. These measurements are all relative to the pre-impact traffic face of the test article." In other words, working width is the total barrier width plus the maximum dynamic intrusion of any portion of the barrier or test vehicle past the field side edge of the barrier.



Figure 8.6. Overlapping Precast Portable Concrete Barriers at Impact Location after Test 620281-01-2.



Figure 8.7. Field-Side of the Overlapping Precast Portable Concrete Barriers at Impact after Test 620281-01-2.

8.6. DAMAGE TO TEST VEHICLE

Figure 8.8 and Figure 8.9 show the damage sustained by the vehicle. Figure 8.10 and Figure 8.11 show the interior of the test vehicle. Table 8.7 and Table 8.8 provide details on the occupant compartment deformation and exterior vehicle damage. Figure F.2 and Figure F.3 in Appendix F.1 provide exterior crush and occupant compartment measurements.



Figure 8.8. Impact Side of Test Vehicle after Test 620281-01-2.

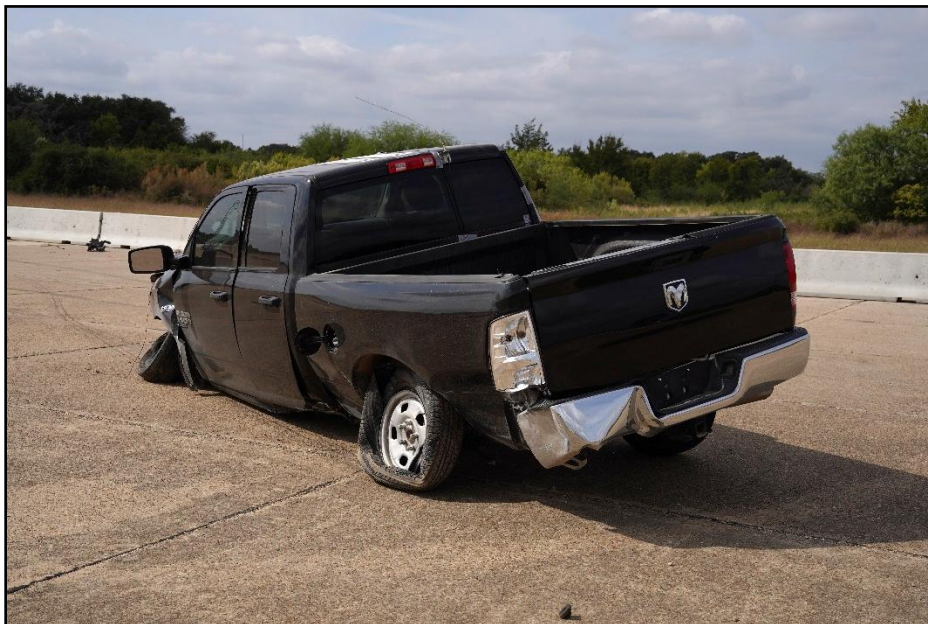


Figure 8.9. Rear Impact Side of Test Vehicle after Test 620281-01-2.



Figure 8.10. Overall Interior of Test Vehicle after Test 620281-01-2.



Figure 8.11. Interior of Test Vehicle on Impact Side after Test 620281-01-2.

Table 8.7. Occupant Compartment Deformation 620281-01-2

Test Parameter	Specification (inches)	Measured (inches)
Roof	≤4.0	0.0
Windshield	≤3.0	0.0
A and B Pillars	≤5.0 overall/≤3.0 lateral	0.0
Foot Well/Toe Pan	≤9.0	3.0
Floor Pan/Transmission Tunnel	≤12.0	0.0
Side Front Panel	≤12.0	0.5
Front Door (above Seat)	≤9.0	0.0
Front Door (below Seat)	≤12.0	0.0

Table 8.8. Exterior Vehicle Damage 620281-01-2

Test Parameter	Details
Side Windows	The side windows remained intact
Maximum Exterior Deformation	25 inches in the front plane at the left front corner at bumper height
VDS	11LFQ4
CDC	11FLAW3
Fuel Tank Damage	None
Description of Damage to Vehicle:	The front bumper, grill, hood, front left quarter panel, left side lower trim, left rear quarter panel, and rear bumper were deformed. The radiator and its support fractured. The wheels on the left side were deformed and their tires ruptured. The left front headlight released, and the left rear brake light fractured. The left front door deformed, causing a 1.3-inch gap at the top between it and the body of the vehicle, and the left rear door deformed, causing a 2.5-inch gap at its base between it and the body of the vehicle. The windshield had some cracking on the lower left side, due to the flexing of the vehicle during impact. There were no holes or tears in the laminate.

8.7. OCCUPANT RISK FACTORS

Data from the accelerometers were digitized for evaluation of occupant risk, and the results are shown in Table 8.9. Figure F.7 through Figure F.9 in Appendix F.3 show acceleration versus time traces.

Table 8.9. Occupant Risk Factors for Test 620281-01-2

Test Parameter	Specification ^a	Measured	Time
OIV, Longitudinal (ft/s)	≤ 40.0 <i>≤ 30.0</i>	19.3	0.1038 seconds on left side of interior
OIV, Lateral (ft/s)	≤ 40.0 <i>≤ 30.0</i>	19.3	0.1038 seconds on left side of interior
Ridedown, Longitudinal (g)	≤ 20.49 <i>≤ 15.0</i>	6.4	0.1673 - 0.1773 seconds
Ridedown, Lateral (g)	≤ 20.49 <i>≤ 15.0</i>	11.0	0.3456 - 0.3556 seconds
Theoretical Head Impact Velocity (THIV) (m/s)	N/A	8.4	0.1000 seconds on left side of interior
Acceleration Severity Index	N/A	1.6	0.0511 - 0.1011 seconds
50-ms Moving Avg. Accelerations (MA) Longitudinal (g)	N/A	-9.3	0.0399 - 0.0899 seconds
50-ms MA Lateral (g)	N/A	10.8	0.0231 - 0.0731 seconds
50-ms MA Vertical (g)	N/A	-3.9	0.9422 - 0.9922 seconds
Roll (°)	≤ 75	N/A	N/A
Pitch (°)	≤ 75	N/A	N/A
Yaw (°)	N/A	N/A	N/A

^a. *Values in italics are the preferred MASH values*

Note: N/A = Not Applicable

Due to equipment failure, accurate roll, pitch, and yaw angles could not be calculated. Visual inspection of the high-speed video indicates that roll and pitch never reached the specified maximum of 75 degrees.

8.8. TEST SUMMARY

Figure 2.1 summarizes the results of *MASH* Test 620281-01-2.



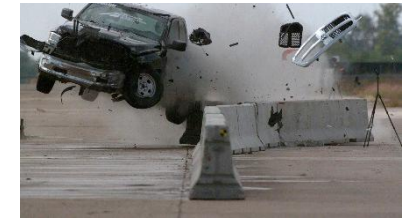
0.000 s



0.2000 s



0.4000 s



0.6000s

GENERAL INFORMATION

Test Agency:	Texas A&M Transportation Institute (TTI)
Test Standard/Test No.:	MASH 2016, Test 3-11
Project No.:	620281-01-2
Test Date:	2025-10-23

TEST ARTICLE

Type:	Longitudinal Barrier
Name:	Overlapping Precast Portable Concrete Barriers
Length:	383 feet 2 inches
Key Materials:	32 f-shape portable concrete barriers
Soil Type and Condition:	Concrete, dry

TEST VEHICLE

Type/Designation:	2270P
Year, Make and Model:	2019 RAM 1500
Inertial Mass:	5044 lb
Dummy Mass:	N/A lb
Gross Static Mass:	5044 lb

IMPACT CONDITIONS

Impact Speed:	62.1 mi/h
Impact Angle:	25.5°
Impact Location:	53.6 inches upstream from the joint between barriers 14 and 15
Impact Severity:	120.5 kip-ft

EXIT CONDITIONS

Exit Speed:	Out of frame - Not measurable
Trajectory/Heading Angle:	Out of frame - Not measurable
Exit Box Criteria:	The vehicle met the exit box criteria

Stopping Distance: 120 ft downstream
41 ft to the traffic side

TEST ARTICLE DEFLECTIONS

Dynamic:	88.4 / 94.7 inches
Permanent:	87 inches
Working Width:	159.8 inches
Working Width Height:	0.0 inches

VEHICLE DAMAGE

VDS:	11LFQ4
CDC:	11FLAW3
Max Exterior Deformation:	25 inches in the front plane at the left front corner at bumper height

Max Occupant Compartment Deformation: 3 inches in the foot well/toe pan

OCCUPANT RISK VALUES

Longitudinal OIV:	19.3 ft/s
Lateral OIV:	19.3 ft/s
Longitudinal Ridedown:	6.4 g
Lateral Ridedown:	11.0 g
THIV:	8.4 m/s
ASI:	1.6
Max 50ms Longitudinal:	-9.3 g
Max 50ms Lateral:	10.8 g
Max 50ms Vertical:	-3.9 g
Max Roll:	Not measurable
Max Pitch:	Not measurable
Max Yaw:	Not measurable

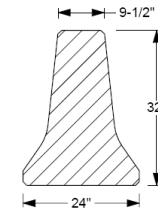
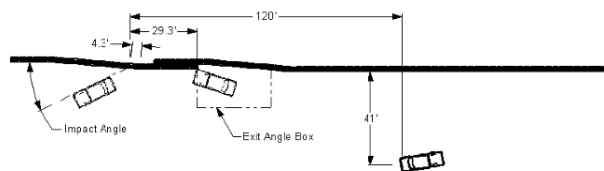


Figure 8.12. Summary of Results for MASH Test 3-11 on Overlapping Precast Portable Concrete Barriers.

CHAPTER 9.

RESULTS OF CRASH TESTING

The crash tests reported herein were performed in accordance with *MASH* TL-3, which involves two tests, on the Overlapping Precast Portable Concrete Barriers.

Table 9.1 shows that the Overlapping Precast Portable Concrete Barriers met the performance criteria for *MASH* TL-3 Longitudinal Barrier.

Table 9.1. Assessment Summary for *MASH* TL-3 Tests on Overlapping Precast Portable Concrete Barriers.

Evaluation Criteria	Description ¹	Test 620281-01-1 (<i>MASH</i> Test 3-10)	Test 620281-01-2 (<i>MASH</i> Test 3-11)
A	Contain, Redirect, or Controlled Stop	S	S
D	No Penetration into Occupant Compartment	S	S
F	Roll and Pitch Limit	S	S
H	OIV Threshold	S	S
I	Ridedown Threshold	S	S
Overall Evaluation		Pass	Pass

Note: S = Satisfactory; N/A = Not Applicable.

¹ See **Error! Reference source not found.** for details

CHAPTER 10.

SUMMARY, IMPLEMENTATION, AND FUTURE RESEARCH*

10.1. SUMMARY

This study addressed the lack of crash-tested guidance for overlapping free-standing portable concrete barriers used in work zone applications. Although overlapping barrier installations are commonly employed in practice, prior to this study there was no validated analytical or experimental basis to assess their safety performance under MASH criteria.

The study began with a literature review and survey of current practice, which confirmed that overlapping PCBs are widely used by transportation agencies. The survey of Roadside Safety Pooled Fund members indicated that F-shape barrier profiles with pin-and-loop connections and laterally offset overlapping configurations are most used in the field.

To address these knowledge gaps, finite element computer simulations were performed using LS-DYNA and executed on the High Performance Research Computing center at Texas A&M University. The FE models of the barrier and the vehicles were first validated using prior MASH TL-3 full-scale crash test results involving free-standing F-shape barriers impacted by the MASH 1100C small car (Test 3-10) and the 2270P pickup truck (Test 3-11). Validation demonstrated satisfactory agreement between simulated and experimental results in terms of vehicle kinematics and barrier deflection, with some discrepancies observed, including underprediction of longitudinal ridedown acceleration for MASH Test 3-10 with the small car.

Following validation, the researchers conducted an extensive parametric simulation study to evaluate the influence of overlap length, gap distance between the overlapping barrier segments, and impact location on system performance. A total of 82 simulations were performed, considering overlap lengths from 1.5 to 6 barrier segments, gap distance ranging from 0 to 2 ft, and seven impact points along the overlapping region. Results identified critical impact locations for the small car and pickup truck.

* The opinions/interpretations identified/expressed in this section of the report are outside the scope of TTI Proving Ground's A2LA Accreditation.

Simulation results showed that for MASH Test 3-10 with the small car, increasing the gap between overlapping barrier runs significantly increased ridedown acceleration, resulting in exceedance of the MASH allowable limit. Maintaining zero gap between barrier runs is needed to meet MASH occupant risk criteria. The simulations also indicated that shorter overlap lengths resulted in lower ridedown accelerations, making shorter overlaps both safer and more practical for work zone deployment.

For MASH Test 3-11 with the pickup-truck, the parametric simulations showed no vehicle stability concerns for the pickup truck across evaluated configurations. The pickup truck simulations controlled maximum barrier deflection and working width.

Based on the simulation results, the configuration consisting of 1.5 barrier segments of overlap with no gap between the overlapping barrier runs was selected for full-scale crash testing. MASH Tests 3-10 and 3-11 were conducted at the identified critical impact locations. Both crash tests were successfully completed and met the MASH Test Level 3 evaluation criteria for longitudinal barriers.

10.2. IMPLEMENTATION

Based on the results of this study, the following configuration is recommended for overlapping free-standing F-shape portable concrete barriers:

- 0-ft gap between overlapping barrier runs, and
- 1.5 barrier segments of overlap length.

MASH test level 3 crash testing of this configuration resulted in a maximum dynamic barrier deflection of 88.4 in. and a total working width of 159.8 in.

For the evaluated barrier segment length of 12 ft 6 in., this configuration results in an overlap length of approximately 18.8 ft. This provides transportation agencies a practical, cost-effective solution for overlapping portable barriers in work zones when circumstances dictate while maintaining compliance with MASH safety performance requirements.

For barriers with different segment lengths, different connection mechanisms, or alternative installation details, additional research is needed to determine the applicability of these recommendations. However, the researchers believe that for other barrier profiles of similar length, such as single-slope concrete barriers, the findings of this study are likely applicable.

10.3. FUTURE RESEARCH

To provide a complete guide for the overlapping practice of F-shape PCBs, further research is recommended to evaluate an overlap length of 2.5 barrier segments. Providing guidance for an overlapping range from 1.5 to 2.5 barrier segments would cover all

possible overlapping scenarios encountered in work zones based on the initial longitudinal gap that exists between the two barrier runs.

Crash testing conducted in this study demonstrated that the small car experienced a lateral ridedown acceleration of 19.2 g, which is close to the MASH allowable limit of 20.49 g. While parametric simulations showed only a small difference in ridedown acceleration between the 1.5-segment and 2.5-segment overlap configurations (only 0.6 g), the model validation indicated that ridedown acceleration tends to be underpredicted in simulations. As a result, definitive conclusions regarding the acceptability of the 2.5-segment overlap configuration cannot be drawn without physical testing.

The researchers believe that the 2.5-barrier overlap configuration is likely to meet MASH TL-3 criteria, but full-scale crash testing is recommended. Future research should conduct MASH Test 3-10 crash testing with the small car at the critical impact point defined in this study to evaluate MASH occupant risk criteria for this configuration.

REFERENCES

1. AASHTO. *Manual for Assessing Safety Hardware*, Second Edition. American Association of State Highway and Transportation Officials, Washington, DC, 2016.
2. Sheikh, N. M., Menges, W. L., and Kuhn, D. L. *MASH TL-3 Testing and Evaluation of Free-Standing Portable Concrete Barrier*. Test Report No. 607911-1&2. Texas A&M Transportation Institute, College Station, TX, May 2017.
3. Bremer, W., Noyce, D. A., Shaw, J. W., Chitturi, M. V., and Bill, A. *Guidelines for Work Zone Designers – Positive Protection*. Traffic Operations & Safety Laboratory, University of Wisconsin–Madison, Madison, WI, May 2019.
4. Minnesota Department of Transportation. *Temporary Barrier Guidance Manual*. MnDOT Office of Traffic Engineering, St. Paul, MN, December 2018.

APPENDIX A.

STANDARDS DRAWINGS

A.1.FDOT STANDARD DRAWINGS

GENERAL NOTES:

1. Temporary barrier systems may be any of the following:

A. Type K Temporary Concrete Barrier System (Index 102-110) installed as either Free-Standing or Anchored.

B. Proprietary Temporary Barrier Systems on the Approved Product List (APL).

a. Concrete Barrier (Free-Standing or Anchored)

b. Steel Barrier (Anchored)

c. Water Filled Barrier (Free-Standing)

2. Where existing flexible pavement is not present, construct a minimum 2" thick temporary Asphalt Pad using Miscellaneous Asphalt Pavement in accordance with Specification 339 with the exception that the use of a pre-emergent herbicide is not required.

3. For Barrier Delineators, see Specification 102. Mount on top of temporary barriers. Color must match adjacent longitudinal pavement marking.

4. Remove all grass debris, loose dirt, and sand for the pavement, bridge deck, or asphalt pad surface within the barrier footprint just prior to placement of the temporary barrier.

5. Ensure the setback distance is clear of any grass, construction debris, stockpiled materials, equipment, and objects.

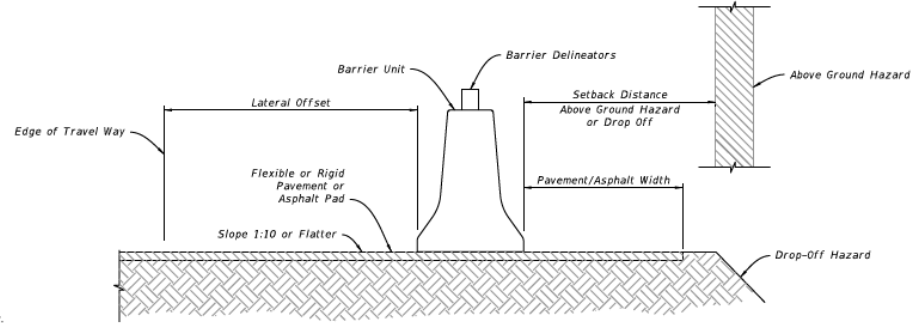
6. Transitions are required between Type K Barrier and free-standing, anchored, back-filled or other types of temporary barrier. See Index 102-110 for transitions between Type K Barrier and permanent bridge or traffic railing. Refer to the APL for transitions allowed for Proprietary Temporary Barrier Systems.

7. Anchoring (Bolting) of temporary barrier or crash cushions is not permitted on bridge superstructures that contain post-tensioned tendons within the concrete deck (top flange of concrete box girders) or on bridge superstructures consisting of longitudinally prestressed, transversely post-tensioned, solid or voided concrete slab units.

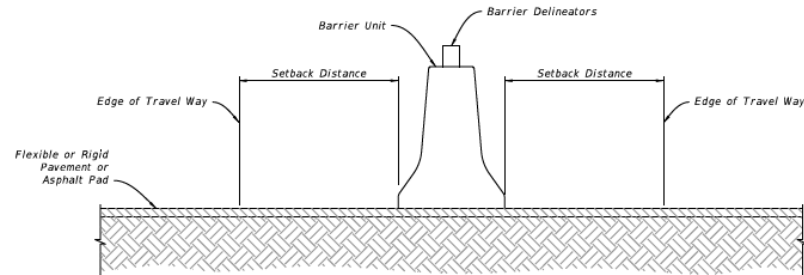
8. Anchor abutting segments of temporary barrier terminated with a Crash Cushion as shown in Index 102-110 or the APL.

9. The requirements of this Index do not apply to Temporary Low Profile Barrier. See Index 102-120.

10. Setback requirements below cover most Temporary Barrier options. Provide additional setback distance for APL products that require additional setback (deflection) space.



ROADSIDE INSTALLATION



MEDIAN INSTALLATION

INSTALLATION DATA

CONDITION	LATERAL OFFSET	SETBACK DISTANCE	PAVEMENT / ASPHALT WIDTH
Anchored	2' Min.	2' Min. (See Note)	1' Min.
Free-standing	2' Min.	4' Min.	4' Min.

NOTE: For Bridge Decks see Index 102-110 or APL.

LAST
REVISION
11/01/20

DESCRIPTION:

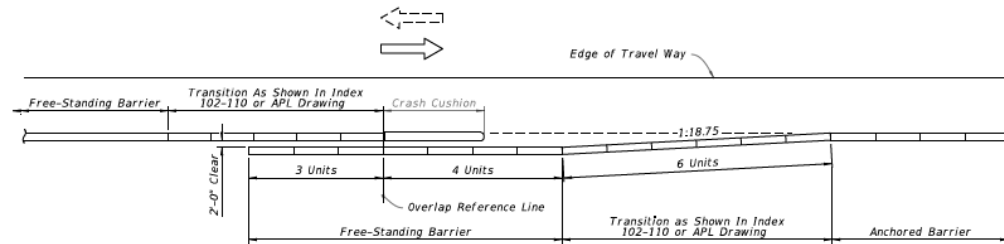


FY 2024-25
STANDARD PLANS

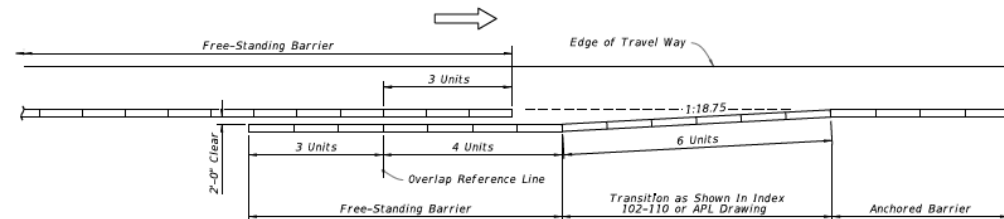
TEMPORARY BARRIER

INDEX
102-100

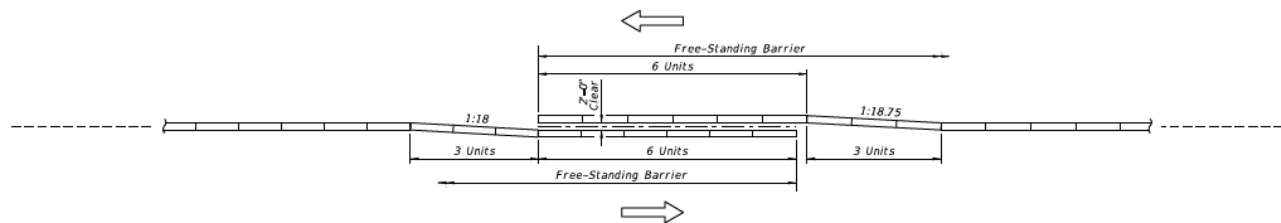
SHEET
1 of 4



APPROACH SHOULDER BARRIER TRANSITION ON UNDIVIDED FACILITIES



APPROACH SHOULDER BARRIER TRANSITION ON DIVIDED FACILITIES

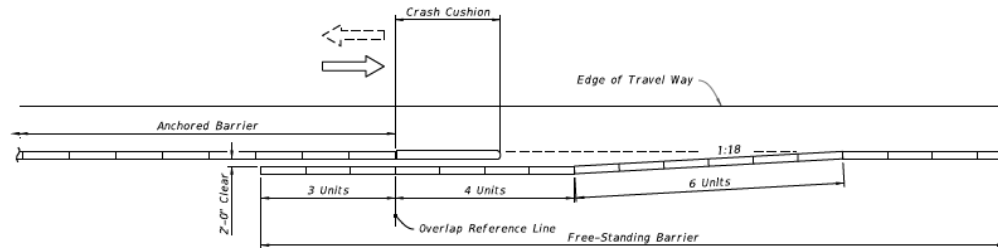


SYMBOL:

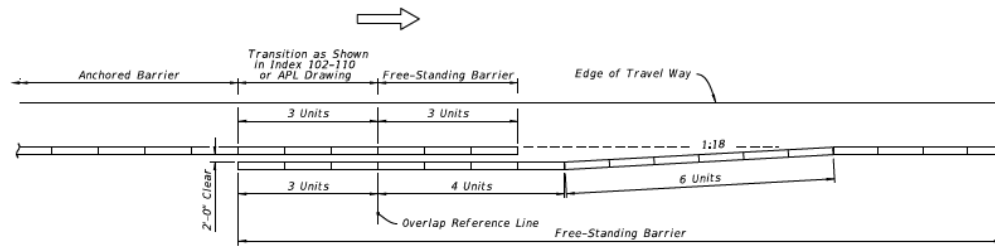
→ Direction of Traffic

MEDIAN BARRIER TRANSITION

LAST REVISION 11/01/20	DESCRIPTION:	FDOT FY 2024-25 STANDARD PLANS	TEMPORARY BARRIER	INDEX 102-100	SHEET 2 of 4
------------------------------	--------------	--------------------------------------	-------------------	------------------	-----------------



DEPARTURE SHOULDER BARRIER TRANSITION ON UNDIVIDED FACILITIES



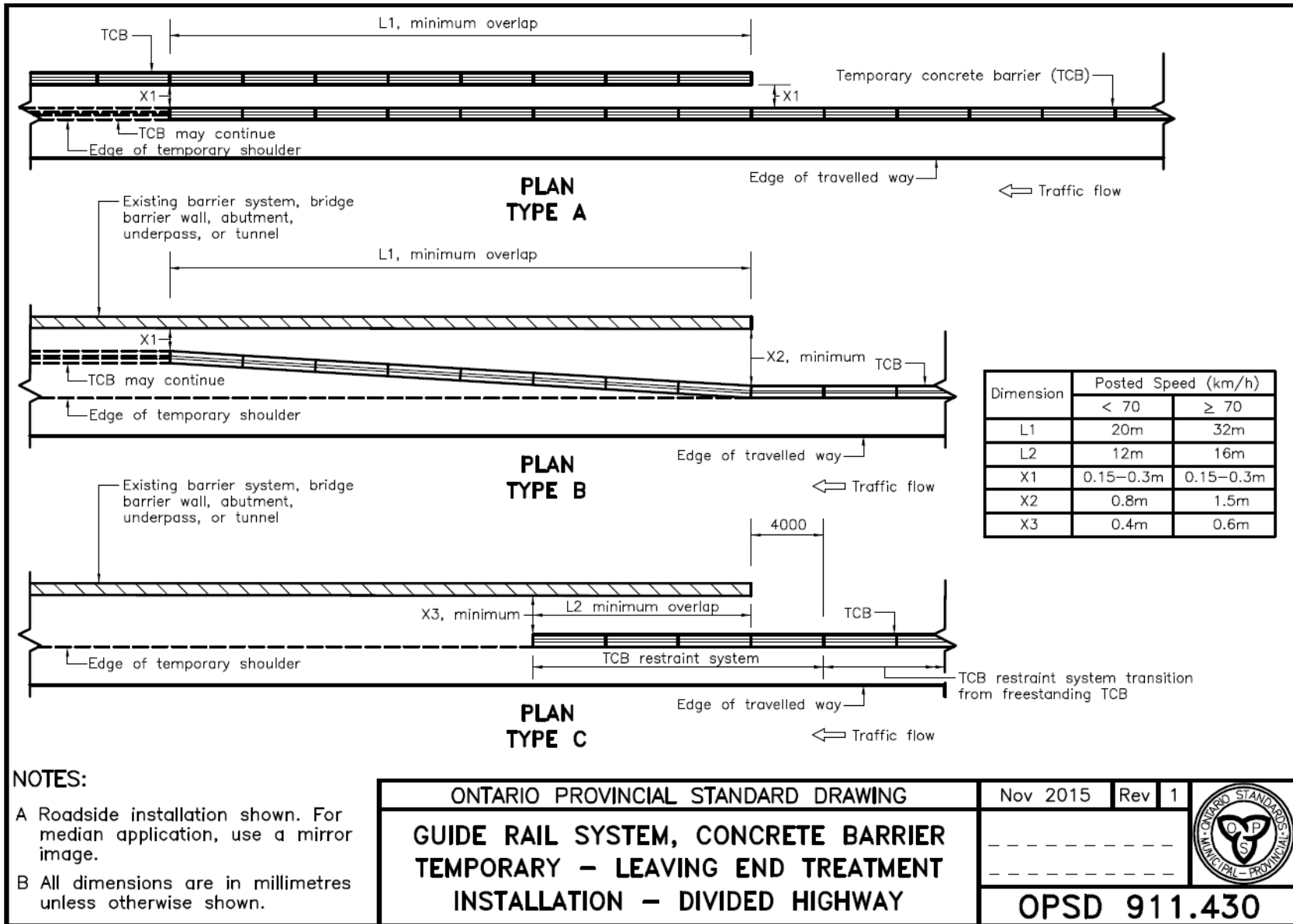
DEPARTURE (TRAILING) SHOULDER BARRIER TRANSITION ON DIVIDED FACILITIES

SYMBOL:

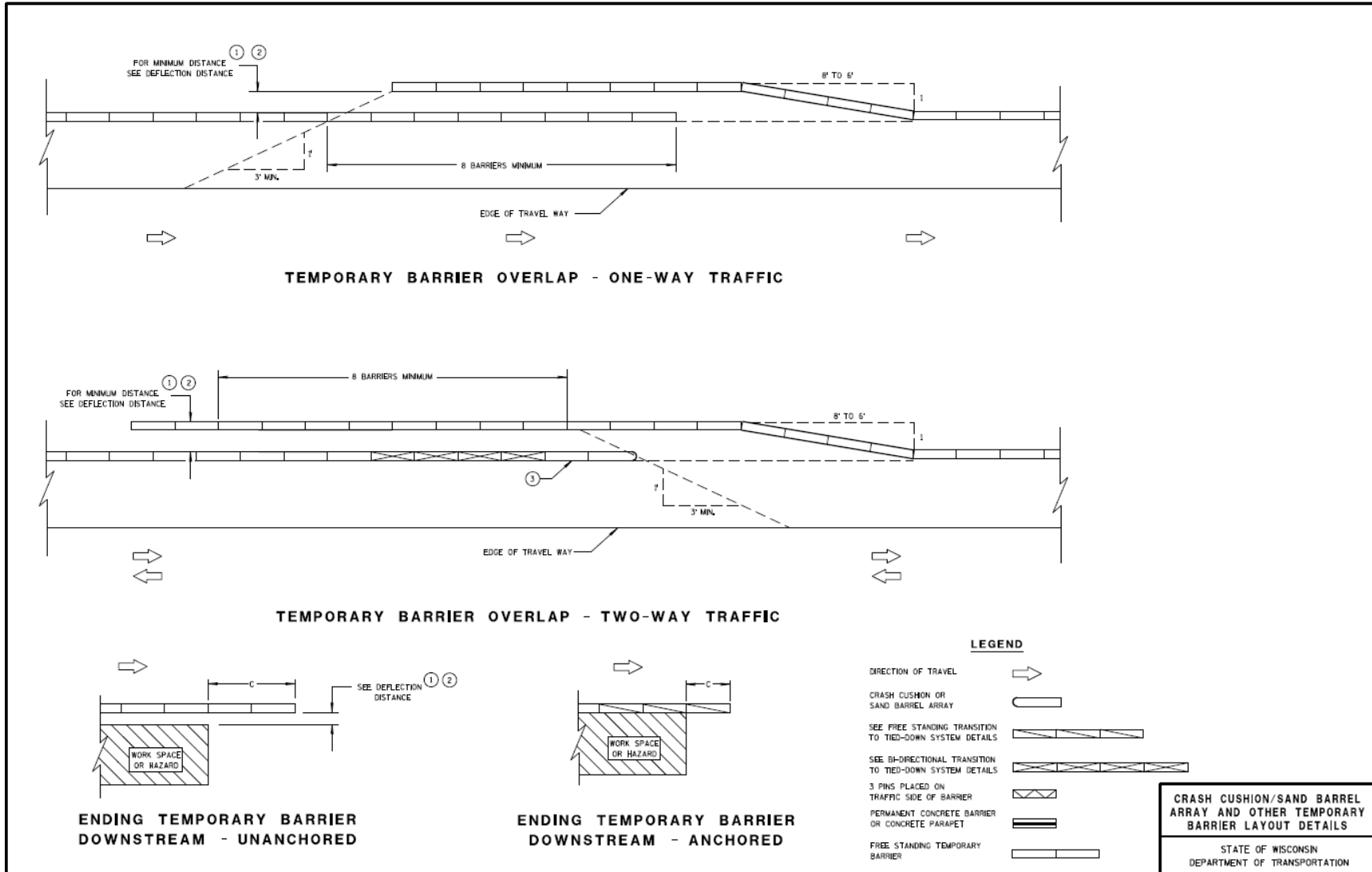
→ Direction of Traffic

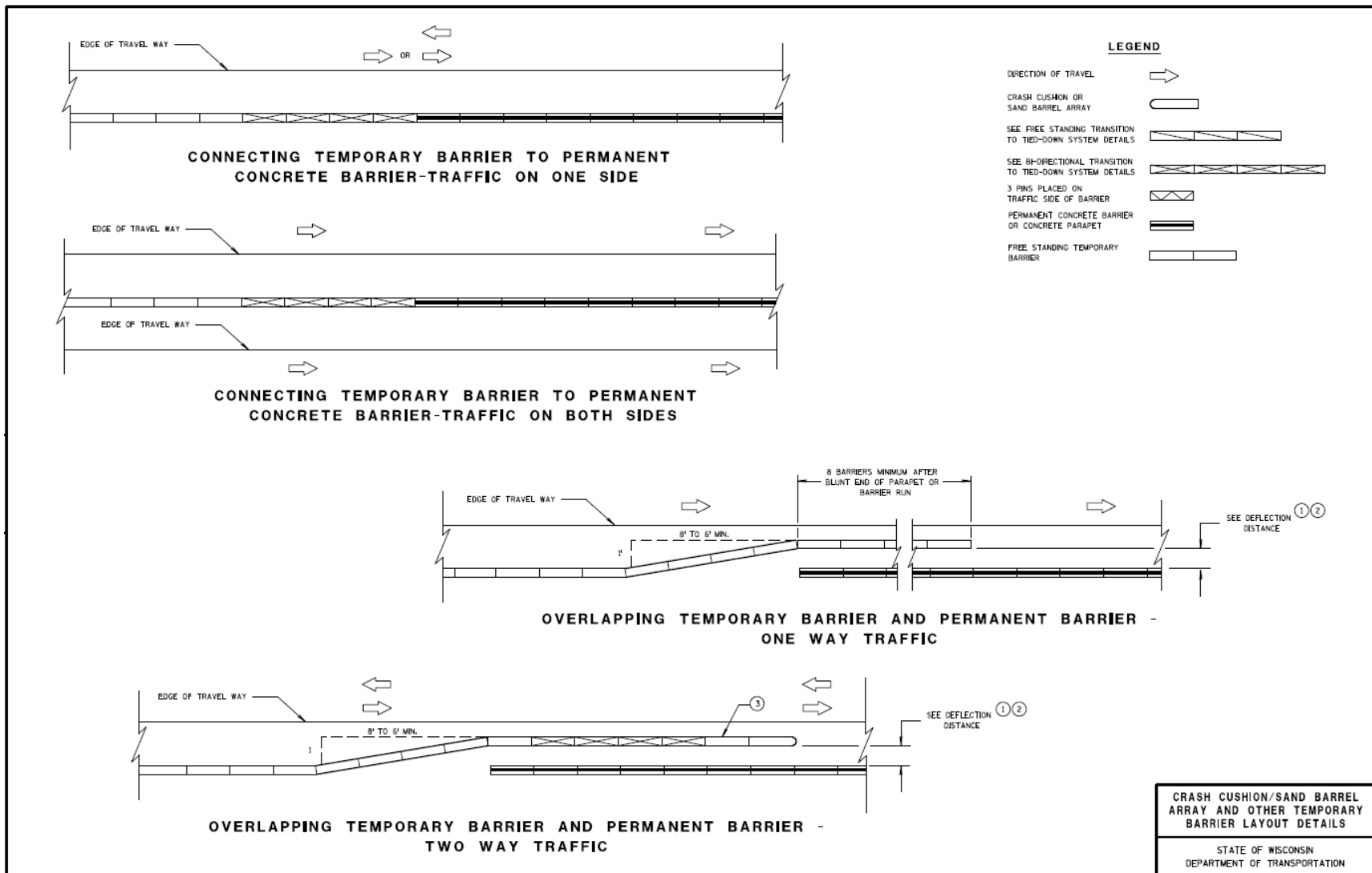
LAST REVISION 11/01/20	DESCRIPTION:	FDOT	FY 2024-25 STANDARD PLANS	TEMPORARY BARRIER	INDEX 102-100	SHEET 3 of 4
------------------------------	--------------	------	------------------------------	-------------------	------------------	-----------------

A.2. ONTARIO PROVINCIAL STANDARD DRAWING



A.3. WISDOT STANDARD DRAWINGS





APPENDIX B.

SURVEY TEMPLATE

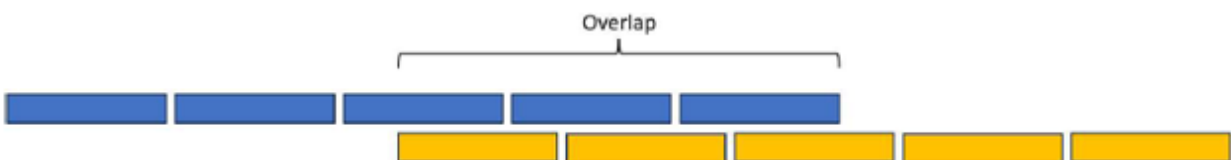
Introduction

Researching Guidelines for Overlapping Precast Concrete Portable Barriers

Overlapping of PCBs is a commonly used practice to terminate exposed barrier ends in work zones by many DOTs. Current practices and standards are not crash tested and not based in research. This survey aims to collect information about the current state of practice and use it to better address the research objectives. The goal of this project is to develop MASH compliant guidelines for overlapping precast concrete portable barriers.



The overlapping mentioned is as follows:



1.) Please enter your contact information below:

Name

DOT

Email

Phone

Questions

2.) Does your State DOT have standards, drawings or guidelines for the overlapping barriers practice?

No

Yes

3.) Please attach the standards, drawings, or guidelines of your State.

Attach additional files

Attach additional files

Attach additional files

4.) Which portable barrier profile does your State DOT typically use when overlapping is used?

F-shape

Single Slope Concrete Barrier (SSCB)

Other (please define):

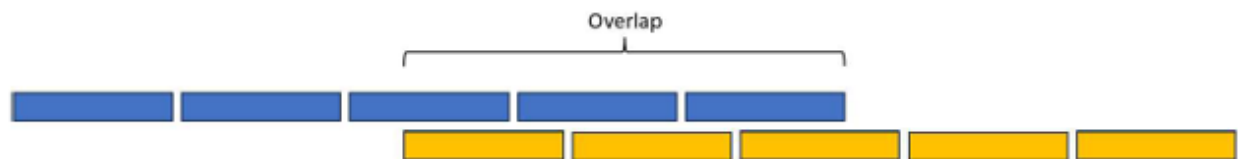
5.) Please attach the standards or drawings for the selected barrier profile.

Attach additional files

Attach additional files

Attach additional files

6.) What is the typical barriers overlapping length used by your State DOT? You may provide a range.



Length (or range) of overlap (ft):

7.) When overlapping is used, are the barrier runs initially in the same line and then offset to make the overlap, or do they initiate and remain in parallel?

Initiate and remain in parallel



Initiate in same line and offset to overlap

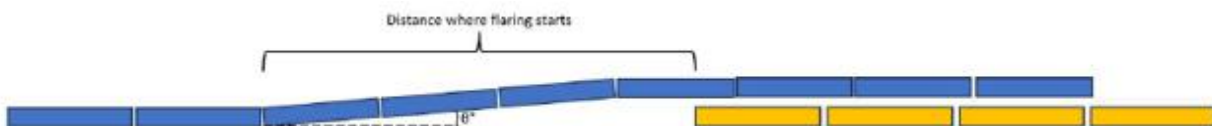


Initiate in same line and offset to overlap

Initiate and remain in parallel

Other: Please comment below

8.) In what distance to the barriers make the flare and at approximately what angle?



Distance where flaring starts (ft):

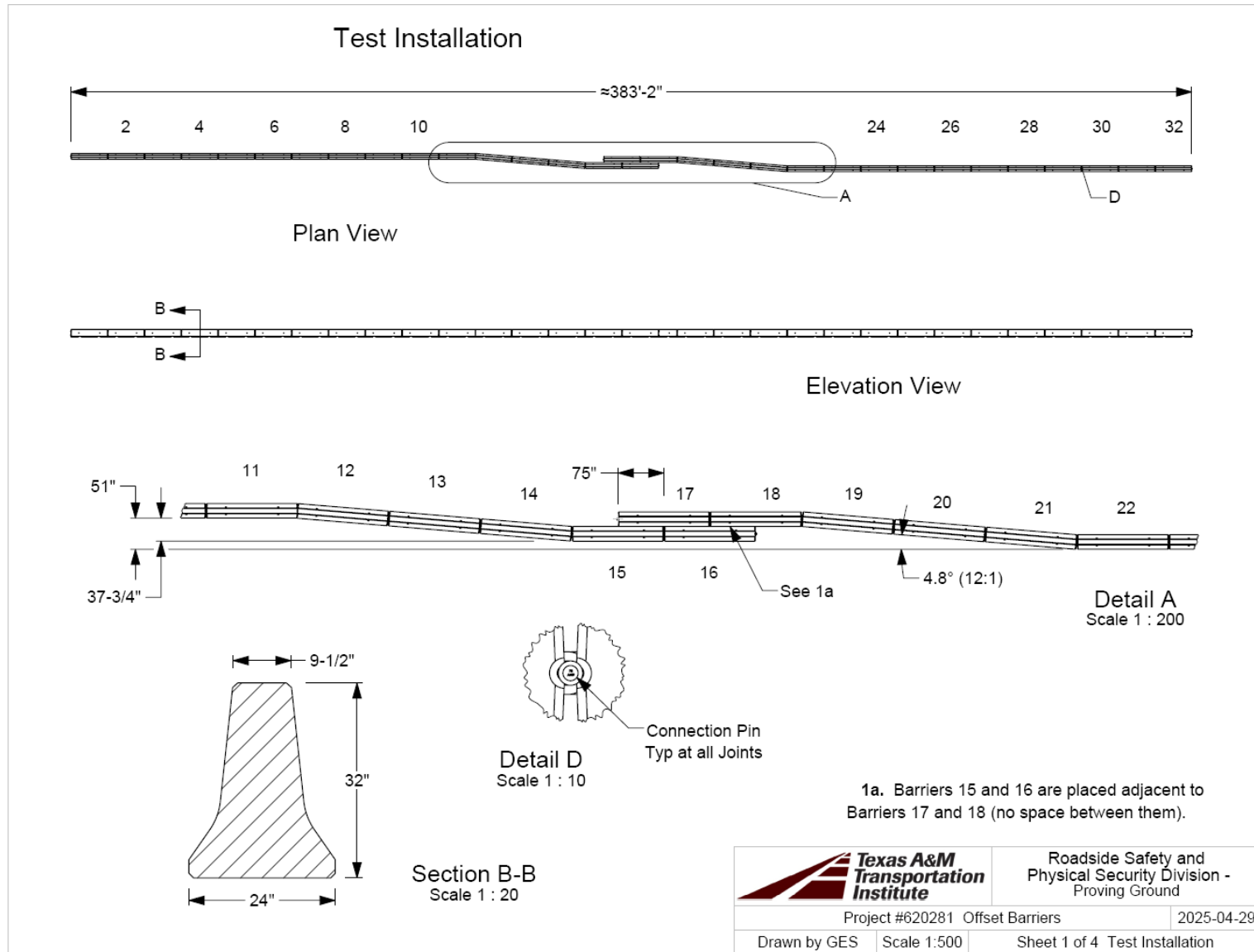
Angle (or rate) of flare:

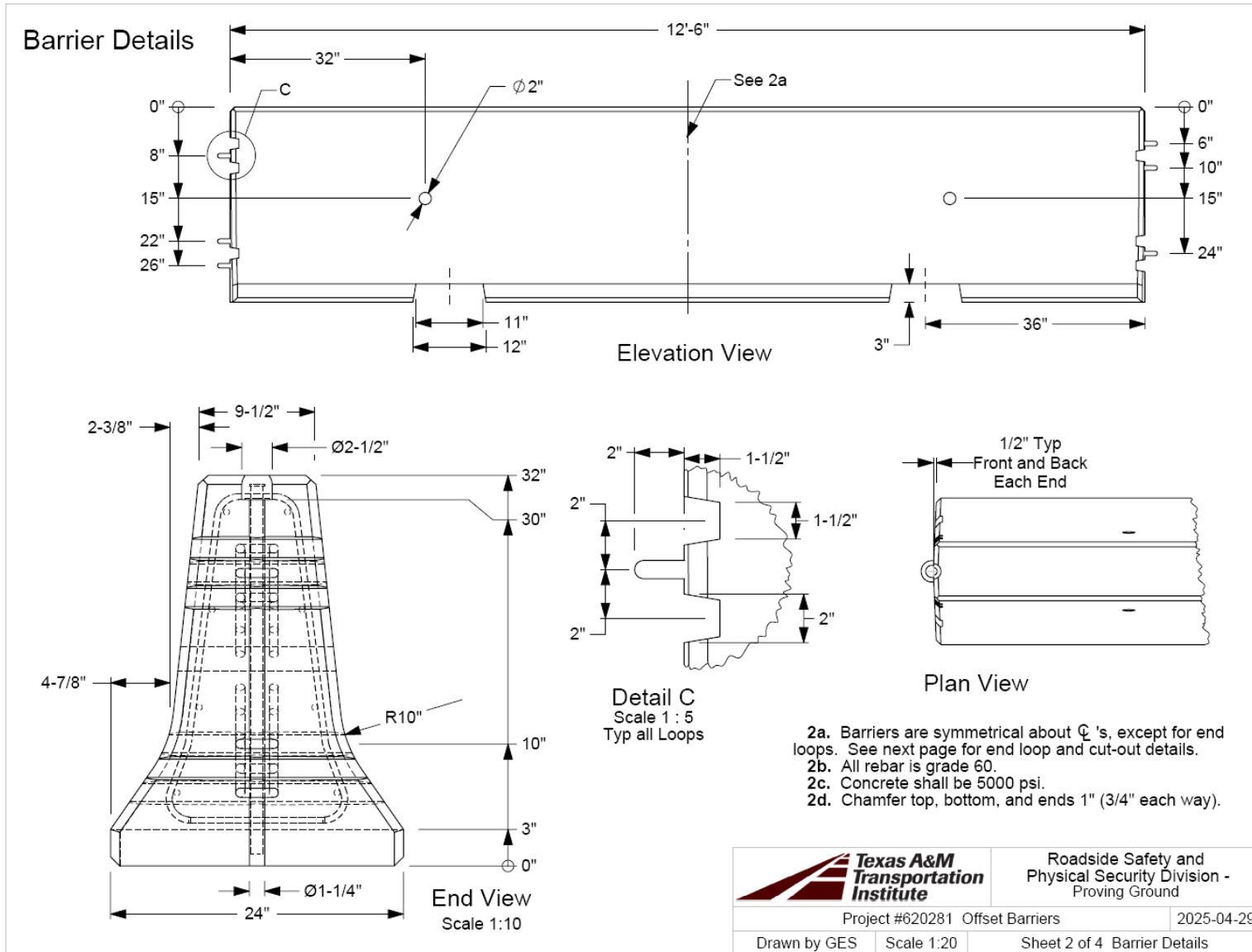
Other Comments:

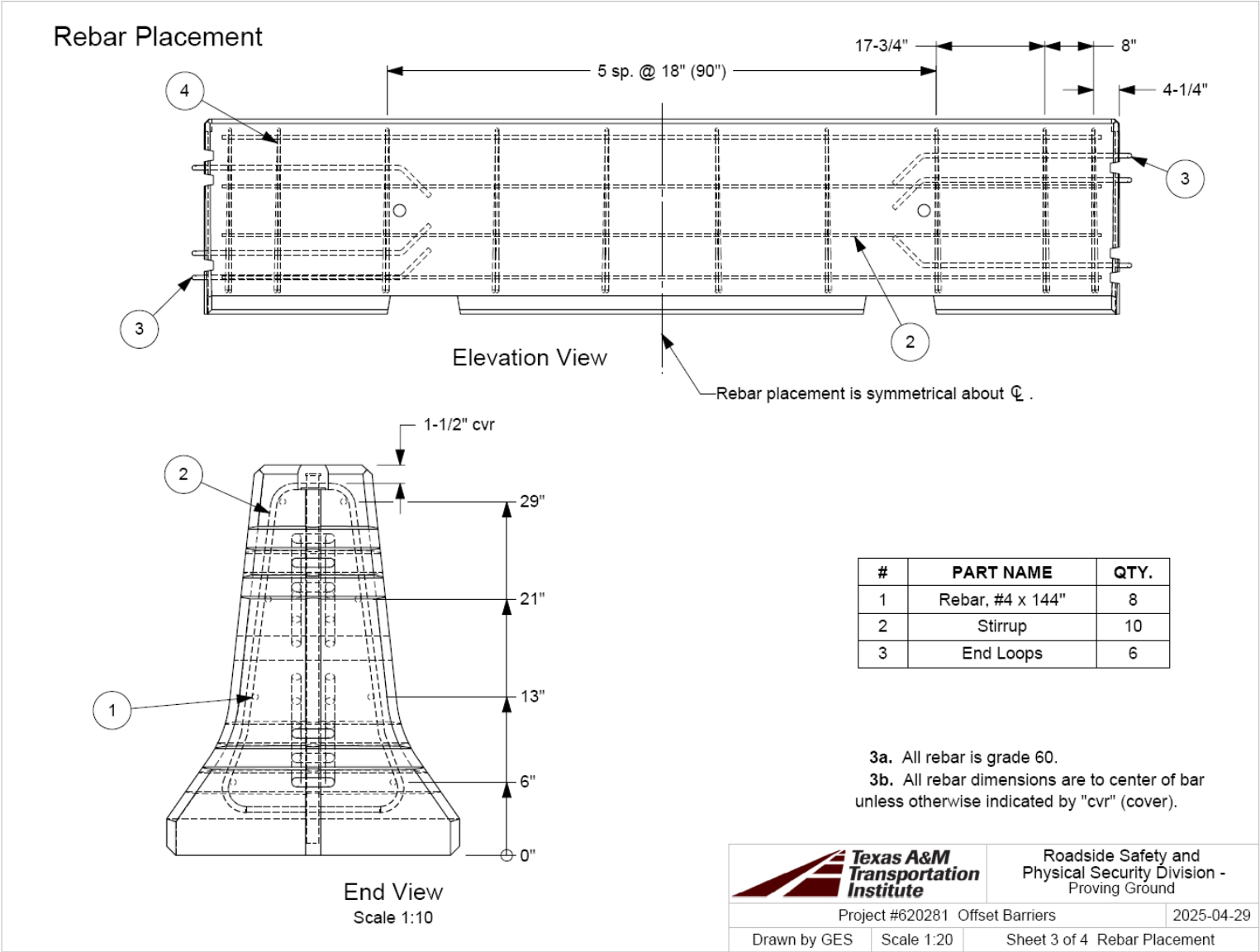
9.) In what other instances does your State use the overlapping barriers practice?

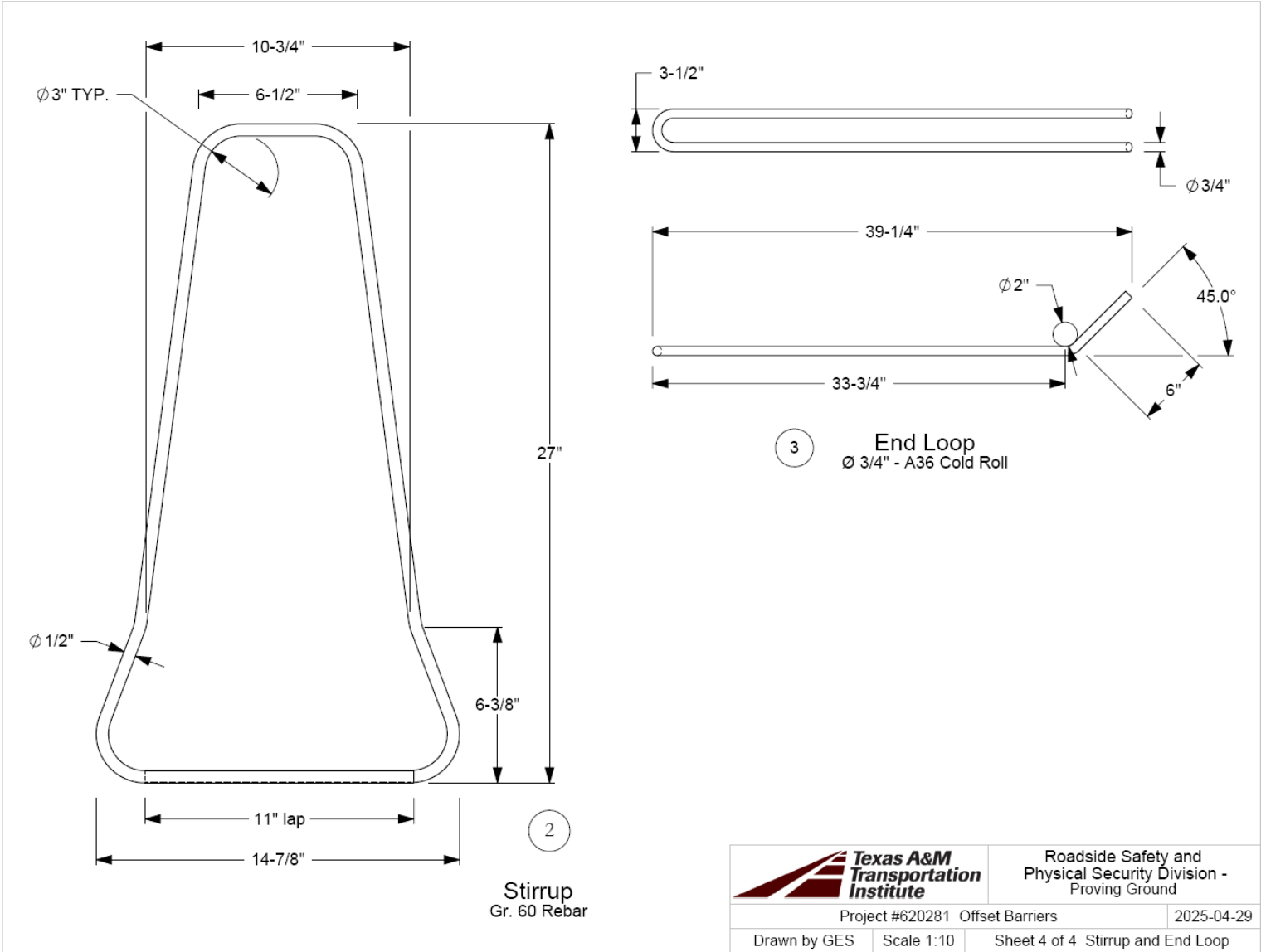
APPENDIX C.

**DETAILS OF OVERLAPPING PRECAST
PORTABLE CONCRETE BARRIERS**



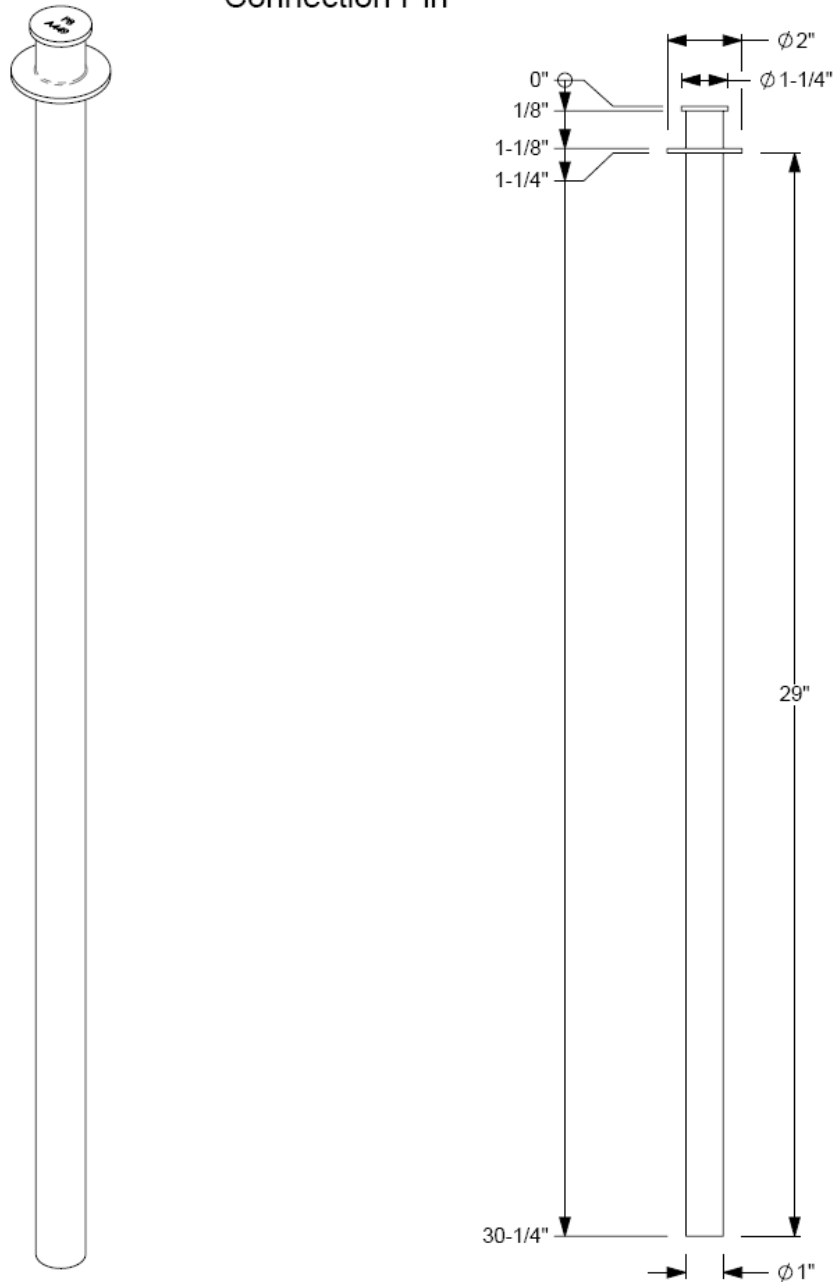






S:\Accreditation-17025-2017\EIR-000 Project Files\620281 - Overlapping PCB's - Cakalli\Drafting, 620281\620281 Drawing

Connection Pin



- 1a.** Pin is forged by Portland Bolt Company (Part #18241), with no welding, and galvanized per ASTM F2329 and A153.
1b. Material is ASTM A449.

		Roadside Safety and Physical Security Division - Proving Ground
Forged Connection Pin		2022-10-06
Drawn by GES	Scale 1:4	Sheet 1 of 1

S:\Accreditation-17025-2017\Drafting Department (Solidworks)\Standard Parts\Concrete Barriers\Forged Connection Pin

APPENDIX D.

SUPPORTING CERTIFICATION DOCUMENTS



2026-05-28



CERTIFIED MATERIAL TEST REPORT

Page 1 / 1

CUSTOMER SHIP TO REGAL METALS INTERNATIONAL INC 207 SENTRY DR MANSFIELD, TX 76063-3609 USA		CUSTOMER BILL TO REGAL METALS INTERNATIONAL INC 207 SENTRY DR MANSFIELD, TX 76063-3609 USA		GRADE 60 (420)	SHAPE / SIZE Rebar / #5 (16mm)	DOCUMENT ID: 0001248667
SALES ORDER 14965591000010		CUSTOMER MATERIAL N°		LENGTH 4000"	WEIGHT 23,781 LB	HEAT / BATCH S80483802
SPECIFICATION / DATE OF REVISION ASTM A615/A615M-24						
CUSTOMER PURCHASE ORDER NUMBER A4663		BILL OF LADING 1327-0000624394		DATE 04/25/2025		

CHEMICAL COMPOSITION									
C (%)	Mn (%)	P (%)	S (%)	Si (%)	Cu (%)	Ni (%)	Cr (%)	Mo (%)	Sn (%)
0.45	1.00	0.014	0.024	0.24	0.24	0.09	0.19	0.028	0.009
MECHANICAL PROPERTIES									
YS (PSI)	YS (MPa)	UTS (PSI)	UTS (MPa)	G/L (Inches)	G/L (mm)	Elong. (%)	BendTest		
71717	494	111968	772	8.000	200.0	11.50	OK		

MECHANICAL PROPERTIES									
YS (PSI)	YS (MPa)	UTS (PSI)	UTS (MPa)	G/L (Inches)	G/L (mm)	Elong. (%)	BendTest		
1.56									

COMMENTS / NOTES

Certified steel is 100% recyclable. Support the circular economy through our Metals Recycling Partnership. For details, visit www2.gerdau.com/metal-recycling, or contact metalrecycling@gerdau.com.

The above figures are certified chemical and physical test records as contained in the permanent records of the company. We certify that these data are correct and in compliance with specified requirements. No weld repair was performed on this material. The material has not been in contact with mercury while in Gerdau's possession. For all products other than billets or beam blanks, this material was Melting & Poured (via Electric Arc Furnace and Continuous Casting) and produced (Hot Rolled and, if applicable, Cold-Drawn) in the USA. For billets or beam blanks, this material was Melting & Poured (via Electric Arc Furnace and Continuous Casting) in the USA. CMTR complies with EN 10204 3.1.

Masakary
BHASKAR YALAMANCHILI
QUALITY DIRECTOR
Phone: (409) 267-1071 Email: Bhaskar.Yalamanchili@gerdau.com

Wade L. Lumpkins
WADE LUMPKINS
QUALITY ASSURANCE MGR.
Phone: 972-779-3118 Email: Wade.Lumpkins@gerdau.com

NUCOR

Mill Certification
06/16/2025

MTR#:2016295-3
Lot #:380005685820
3630 Fourth Street
Flowood, MS 39232 US
601 939-1623
Fax: 601 936-6202

Sold To: REGAL METALS
207 SENTRY DR
MANSFIELD, TX 76063 US

Ship To: REGAL METALS INTERNATIONAL
207 SENTRY DR
MANSFIELD, TX 76063 US

Customer PO	BRIAN YARD ORDER	Sales Order #	38031490 - 1.4
Product Group	Rebar	Product #	2110230
Grade	A615 Gr 60/AASHTO M31	Lot #	380005685820
Size	#5	Heat #	3800056858
BOL #	BOL-2065805	Load #	2016295
Description	Rebar #5/16mm A615 Gr 60/AASHTO M31 40' 0" [480"] 4001-8000 lbs	Customer Part #	
Production Date	06/05/2025	Qty Shipped LBS	20024
Product Country Of Origin	United States	Qty Shipped EA	480
Original Item Description		Original Item Number	

I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements.

Melt Country of Origin : United States

Melting Date: 05/23/2025

Roll Country of Origin : United States

Rolling Date: 06/05/2025

C (%)	Mn (%)	P (%)	S (%)	Si (%)	Ni (%)	Cr (%)	Mo (%)	Cu (%)	V (%)	Nb (%)
0.37	0.82	0.020	0.023	0.172	0.11	0.20	0.02	0.37	0.023	0.000

Mechanical

	<u>Average Deformation Height (IN)</u>	<u>Bend Test</u>
(1)	0.042	Pass

Tensile testing

	Yield (PSI)	Tensile (PSI)	Elongation in 8" (%)
(1)	70600	100100	15.6

Other Test Results

Weight Percent Variance (%) : -3.72

Tensile / Yield Ratio : 1.42

Comments:

Nucor Steel Jackson, Inc. is in compliance with and certified to: ISO 9001:2015, ISO 14001:2015, ABS Quality Assurance Program & AASHTO's NTPEP Reinforcing Steel and Wire (REBAR) Technical Committee Work Plan. All manufacturing processes for this product, including melting, casting, and hot rolling, were performed in the United States of America.

Mercury not intentionally added at any point during manufacturing or testing of this material. No weld repair was performed.

Material and Mill Certification are in full compliance with the American Iron and Steel requirement as mandated in EPA's State Revolving Fund Programs and complies with the Buy American Act, (FTA) Buy America Requirements (49 CFR part 661), and (FHWA) Buy America Requirements (23 CFR part 635.410)

This material was tested using full-section samples.

Nolan Guess

Nolan Guess, Quality Supervisor

Page 1 of 1

NUCOR

Mill Certification

06/12/2025

MTR#:2019965-2
Lot #:380005707120
3630 Fourth Street
Flowood, MS 39232 US
601 939-1623
Fax: 601 936-6202

Sold To: REGAL METALS
207 SENTRY DR
MANSFIELD, TX 76063 US

Ship To: REGAL METALS INTERNATIONAL
207 SENTRY DR
MANSFIELD, TX 76063 US

Customer PO	BRIAN 60' YARD	Sales Order #	38031545 - 1.3
Product Group	Rebar	Product #	2110206
Grade	A615 Gr 60/AASHTO M31	Lot #	380005707120
Size	#4	Heat #	3800057071
BOL #	BOL-2062986	Load #	2019965
Description	Rebar #4/13mm A615 Gr 60/AASHTO M31 60' 0" [720"] 6001-10000 lbs	Customer Part #	
Production Date	06/01/2025	Qty Shipped LBS	36072
Product Country Of Origin	United States	Qty Shipped EA	900
Original Item Description		Original Item Number	

I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements.

Melt Country of Origin : United States

Melting Date: 05/31/2025

Roll Country of Origin : United States

Rolling Date: 06/01/2025

C (%)	Mn (%)	P (%)	S (%)	Si (%)	Ni (%)	Cr (%)	Mo (%)	Cu (%)	V (%)	Nb (%)
0.38	0.80	0.013	0.030	0.220	0.12	0.17	0.04	0.31	0.023	0.000

Mechanical

	Average Deformation Height (in)	Bend Test
(1)	0.032	Pass

Tensile testing

	Yield (PSI)	Tensile (PSI)	Elongation in 8" (%)
(1)	69800	99700	12.5

Other Test Results

Weight Percent Variance (%) : -4.14

Tensile / Yield Ratio : 1.43

Comments:

Nucor Steel Jackson, Inc. is in compliance with and certified to: ISO 9001:2015, ISO 14001:2015, ABS Quality Assurance Program & AASHTO's NTPEP Reinforcing Steel and Wire (REBAR) Technical Committee Work Plan. All manufacturing processes for this product, including melting, casting, and hot rolling, were performed in the United States of America.
Mercury not intentionally added at any point during manufacturing or testing of this material. No weld repair was performed.
Material and Mill Certification are in full compliance with the American Iron and Steel requirement as mandated in EPA's State Revolving Fund Programs and complies with the Buy American Act, (FTA) Buy America Requirements (49 CFR part 661), and (FHWA) Buy America Requirements (23 CFR part 635.410)
This material was tested using full-section samples.

Nolan Guess

Nolan Guess, Quality Supervisor

Page 1 of 1

NUCOR®**Mill Certification**

06/03/2025

MTR#:1990406-1
Lot #:110006817020
8812 HWY 79 W
Jewett, TX 75846 US
903 626-4461
Fax: 903 626-6290Sold To: REGAL METALS INTERNATIONAL
207 SENTRY DR
MANSFIELD, TX 76063 USShip To: REGAL METALS INTERNATIONAL
207 SENTRY DR
MANSFIELD, TX 76063 US

Customer PO	YARD LOAD 5/16	Sales Order #	11086983 - 3.5
Product Group	Rebar	Product #	2110200
Grade	A615 Gr 60/AASHTO M31	Lot #	110006817020
Size	#4	Heat #	1100068170
BOL #	BOL-2050229	Load #	1990406
Description	Rebar #4/13mm A615 Gr 60/AASHTO M31 40' 0" [480"] 2001-4000 lbs	Customer Part #	
Production Date	04/15/2025	Qty Shipped LBS	48096
Product Country Of Origin	United States	Qty Shipped EA	1800
Original Item Description		Original Item Number	

I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements.

Melt Country of Origin : United States

Melting Date: 04/12/2025

Roll Country of Origin : United States

Rolling Date: 04/15/2025

C (%)	Mn (%)	P (%)	S (%)	Si (%)	Ni (%)	Cr (%)	Mo (%)	Cu (%)	V (%)	Nb (%)
0.38	1.03	0.017	0.019	0.212	0.11	0.22	0.03	0.28	0.005	0.003

Mechanical**Bend Test**

(1) Pass

Tensile testing

	Yield (PSI)	Tensile (PSI)	Elongation in 8" (%)
(1)	68300	104900	10.0

Other Test Results

Tensile / Yield Ratio : 1.54

Comments:

1. All manufacturing processes of the steel, including melting, casting & hot rolling, have been performed in U.S.A
2. Mercury not intentionally added at any point during manufacturing or testing of this material.
3. Welding or weld repair was not performed on this material.
4. This material conforms to the specifications described on this document and may not be reproduced, except in full, without written approval of Nucor Corporation.
5. Results reported ASTM E45 (Inclusion content) and ASTM E881 (Macro-etch) are provided as interpretation of ASTM procedures.

Ramon Vigil, Quality Supervisor

Page 1 of 1

NUCOR

Mill Certification
06/12/2025

MTR#:2019968-2
Lot #:380005692420
3630 Fourth Street
Flowood, MS 39232 US
601 939-1623
Fax: 601 936-6202

Sold To: REGAL METALS
207 SENTRY DR
MANSFIELD, TX 76063 US

Ship To: REGAL METALS INTERNATIONAL
207 SENTRY DR
MANSFIELD, TX 76063 US

Customer PO	BRIAN 60' YARD	Sales Order #	38031545 - 1.2
Product Group	Rebar	Product #	2110206
Grade	A615 Gr 60/AASHTO M31	Lot #	380005692420
Size	#4	Heat #	3800056924
BOL #	BOL-2061592	Load #	2019968
Description	Rebar #4/13mm A615 Gr 60/AASHTO M31 60' 0" [720"] 6001-10000 lbs	Customer Part #	
Production Date	06/01/2025	Qty Shipped LBS	27054
Product Country Of Origin	United States	Qty Shipped EA	675
Original Item Description		Original Item Number	

I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements.

Melt Country of Origin : United States

Melting Date: 05/25/2025

Roll Country of Origin : United States

Rolling Date: 06/01/2025

C (%)	Mn (%)	P (%)	S (%)	Si (%)	Ni (%)	Cr (%)	Mo (%)	Cu (%)	V (%)	Nb (%)
0.40	0.83	0.007	0.023	0.185	0.13	0.12	0.03	0.33	0.023	0.001

Mechanical

	Average Deformation Height (IN)	Bend Test
(1)	0.034	Pass

Tensile testing

	Yield (PSI)	Tensile (PSI)	Elongation in 8" (%)
(1)	71300	102500	12.5

Other Test Results

Weight Percent Variance (%) : -1.81

Tensile / Yield Ratio : 1.44

Comments:

Nucor Steel Jackson, Inc. is in compliance with and certified to: ISO 9001:2015, ISO 14001:2015, ABS Quality Assurance Program & AASHTO's NTPEP Reinforcing Steel and Wire (REBAR) Technical Committee Work Plan. All manufacturing processes for this product, including melting, casting, and hot rolling, were performed in the United States of America.

Mercury not intentionally added at any point during manufacturing or testing of this material. No weld repair was performed.

Material and Mill Certification are in full compliance with the American iron and Steel requirement as mandated in EPA's State Revolving Fund Programs and complies with the Buy American Act, (FTA) Buy America Requirements (49 CFR part 661), and (FHWA) Buy America Requirements (23 CFR part 635.410)

This material was tested using full-section samples.

Nolan Guess

Nolan Guess, Quality Supervisor

Page 1 of 1



US-ML-MIDLOTIHAN
300 WARD ROAD
MIDLOTIHAN, TX 76065
USA

CERTIFIED MATERIAL TEST REPORT

Page 1 / 1

CUSTOMER SENT TO REGAL METALS INTERNATIONAL INC 207 SENTRY DR MANSFIELD, TX 76063-3609 USA	CUSTOMER BILL TO REGAL METALS INTERNATIONAL INC 207 SENTRY DR MANSFIELD, TX 76063-3609 USA	GRADE 60 (420)	SHAPE / SIZE Rebar / #4 (13MM)	DOCUMENT ID: 0001216063
SALES ORDER 14783780000030	CUSTOMER MATERIAL N°	LENGTH 6000"	WEIGHT 24,048 LB	HEAT / BATCH S806407702
CUSTOMER PURCHASE ORDER NUMBER Yard 021725		BILL OF LADING 1327-0000614176		DATE 02/20/2025
SPECIFICATION / DATE OF REVISION ASTM A615/A615M-24				

CHEMICAL COMPOSITION										
C (%)	Mn (%)	P (%)	S (%)	Si (%)	Cu (%)	Ni (%)	Cr (%)	Mo (%)	Sn (%)	V (%)
0.45	0.97	0.010	0.026	0.22	0.24	0.11	0.17	0.028	0.005	0.003
MECHANICAL PROPERTIES										
YS (PSI) 74452	YS (MPa) 513	UTS (PSI) 114450	UTS (MPa) 789	G/L (Inches) 8.000	G/L (mm) 200.0	Nb (%) 0.001	Al (%) 0.001	CE _{req} (%) 0.64	CH _{req} (%) 0.64	CH _{req} (%) 0.64
MECHANICAL PROPERTIES										
UTS / YS 1.54										

COMMENTS / NOTES

Certified steel is 100% recyclable. Support the circular economy through our Metals Recycling Partnership. For details, visit www2.gerdau.com/articles-recycling or contact metalrecycling@gerdau.com.

The above figures are certified chemical and physical test records as contained in the permanent records of the company. We certify that these data are correct and in compliance with specified requirements. No weld repair was performed on this material. The material has not been in contact with mercury while in Gerdau's possession. For all products other than billets or beam blanks, this material was Melted & Poured (via Electric Arc Furnace and Continuous Casting) and produced (Hot Rolled and, if applicable, Cold Drawn) in the USA. For billets or beam blanks, this material was Melted & Poured (via Electric Arc Furnace and Continuous Casting) in the USA. CMTR complies with EN 10204 3.1.

Maskey
BHASKAR YALAMANCHI
QUALITY DIRECTOR
Phone: (409) 267-1071 Email: Bhaskar.Yalamanchi@gerdau.com

De A. Jr.
WADE LAMPENS
QUALITY ASSURANCE MGR.
Phone: 972-779-3118 Email: Wade.Lampens@gerdau.com

NUCOR

Mill Certification

06/16/2025

MTR#:2019971-2
Lot #:380005688920
3630 Fourth Street
Flowood, MS 39232 US
601 939-1623
Fax: 601 936-6202

Sold To: REGAL METALS
207 SENTRY DR
MANSFIELD, TX 76063 US

Ship To: REGAL METALS INTERNATIONAL
207 SENTRY DR
MANSFIELD, TX 76063 US

Customer PO	BRIAN 60' YARD	Sales Order #	38031545 - 2.6
Product Group	Rebar	Product #	3019447
Grade	A615 Gr 60/AASHTO M31	Lot #	380005688920
Size	#5	Heat #	3800056889
BOL #	BOL-2066549	Load #	2019971
Description	Rebar #5/16mm A615 Gr 60/AASHTO M31 60' 0" [720"] 6001-10000 lbs	Customer Part #	
Production Date	05/29/2025	Qty Shipped LBS	36048
Product Country Of Origin	United States	Qty Shipped EA	576
Original Item Description		Original Item Number	

I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements.

Melt Country of Origin : United States

Melting Date: 05/24/2025

Roll Country of Origin : United States

Rolling Date: 05/29/2025

C (%)	Mn (%)	P (%)	S (%)	Si (%)	Ni (%)	Cr (%)	Mo (%)	Cu (%)	V (%)	Nb (%)
0.40	0.85	0.009	0.026	0.206	0.10	0.13	0.02	0.31	0.023	0.001

Mechanical

	Average Deformation Height (IN)	Bend Test
(1)	0.039	Pass

Tensile testing

	Yield (PSI)	Tensile (PSI)	Elongation in 8" (%)
(1)	66400	99200	21.2

Other Test Results

Weight Percent Variance (%) : -3.79

Tensile / Yield Ratio : 1.50

Comments:

Nucor Steel Jackson, Inc. is in compliance with and certified to: ISO 9001:2015, ISO 14001:2015, ABS Quality Assurance Program & AASHTO's NTPEP Reinforcing Steel and Wire (REBAR) Technical Committee Work Plan. All manufacturing processes for this product, including melting, casting, and hot rolling, were performed in the United States of America.

Mercury not intentionally added at any point during manufacturing or testing of this material. No weld repair was performed.

Material and Mill Certification are in full compliance with the American Iron and Steel requirement as mandated in EPA's State Revolving Fund Programs and complies with the Buy American Act, (FTA) Buy America Requirements (49 CFR part 661), and (FHWA) Buy America Requirements (23 CFR part 635.410)

This material was tested using full-section samples.

Nolan Guess

Nolan Guess, Quality Supervisor

Page 1 of 1

Mi

NUCOR**Mill Certification**

02/18/2025

MTR#:1889269-2
Lot #:110006605720
8812 HWY 79 W
Jewett, TX 75846 US
903 626-4461
Fax: 903 626-6290Sold To: REGAL METALS INTERNATIONAL
207 SENTRY DR
MANSFIELD, TX 76063 USShip To: REGAL METALS INTERNATIONAL
207 SENTRY DR
MANSFIELD, TX 76063 US

Customer PO	YARD LOAD 2/10	Sales Order #	11080199 - 7.9
Product Group	Rebar	Product #	2110320
Grade	A615 Gr 60/AASHTO M31	Lot #	110006605720
Size	#8	Heat #	1100066057
BOL #	BOL-1939407	Load #	1889269
Description	Rebar #8/25mm A615 Gr 60/AASHTO M31 40' 0" [480"] 2001-6000 lbs	Customer Part #	
Production Date	02/11/2025	Qty Shipped LBS	12816
Product Country Of Origin	United States	Qty Shipped EA	120
Original Item Description		Original Item Number	

I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements.

Melt Country of Origin : United States

Melting Date: 02/09/2025

Roll Country of Origin : United States

Rolling Date: 02/11/2025

C (%)	Mn (%)	P (%)	S (%)	Si (%)	Ni (%)	Cr (%)	Mo (%)	Cu (%)	V (%)	Nb (%)
0.36	0.97	0.017	0.014	0.201	0.16	0.28	0.05	0.23	0.004	0.022

Mechanical**Bend Test**

(1) Pass

Tensile testing

	Yield (PSI)	Tensile (PSI)	Elongation in 8" (%)
(1)	70300	104800	11.0

Other Test Results

Tensile / Yield Ratio : 1.49

Comments:

1. All manufacturing processes of the steel, including melting, casting & hot rolling, have been performed in U.S.A
2. Mercury not intentionally added at any point during manufacturing or testing of this material.
3. Welding or weld repair was not performed on this material.
4. This material conforms to the specifications described on this document and may not be reproduced, except in full, without written approval of Nucor Corporation.
5. Results reported ASTM E45 (Inclusion content) and ASTM E381 (Macro-etch) are provided as interpretation of ASTM procedures.

Robert E. Fortson, Quality Assurance

NUCOR

Mill Certification

05/30/2025

MTR#:2005651-2
Lot #:380005631820
3630 Fourth Street
Flowood, MS 39232 US
601 939-1623
Fax: 601 936-6202

Sold To: REGAL METALS
207 SENTRY DR
MANSFIELD, TX 76063 US

Ship To: REGAL METALS INTERNATIONAL
207 SENTRY DR
MANSFIELD, TX 76063 US

Customer PO	BRIAN 2 NOW 2 LATER	Sales Order #	38031249 - 1.3
Product Group	Rebar	Product #	2110265
Grade	A615 Gr 60/AASHTO M31	Lot #	380005631820
Size	#6	Heat #	3800056318
BOL #	BOL-2047185	Load #	2005651
Description	Rebar #6/19mm A615 Gr 60/AASHTO M31 40' 0" [480"] 2001-6000 lbs	Customer Part #	
Production Date	05/06/2025	Qty Shipped LBS	30282
Product Country Of Origin	United States	Qty Shipped EA	504
Original Item Description		Original Item Number	

I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements.

Melt Country of Origin : United States

Melting Date: 05/01/2025

Roll Country of Origin : United States

Rolling Date: 05/06/2025

C (%)	Mn (%)	P (%)	S (%)	Si (%)	Ni (%)	Cr (%)	Mo (%)	Cu (%)	V (%)	Nb (%)	Sn (%)
0.36	0.79	0.014	0.028	0.227	0.22	0.23	0.05	0.33	0.021	0.002	0.012

Mechanical

	Average Deformation Height (IN)	Bend Test
(1)	0.049	Pass

Tensile testing

	Yield (PSI)	Tensile (PSI)	Elongation in 8" (%)
(1)	69900	106500	13.8

Other Test Results

Weight Percent Variance (%) : -3.40

Tensile / Yield Ratio : 1.52

Comments:

Nucor Steel Jackson, Inc. is in compliance with and certified to: ISO 9001:2015, ISO 14001:2015, ABS Quality Assurance Program & AASHTO's NYTEP Reinforcing Steel and Wire (REBAR) Technical Committee Work Plan. All manufacturing processes for this product, including melting, casting, and hot rolling, were performed in the United States of America.

Mercury not intentionally added at any point during manufacturing or testing of this material. No weld repair was performed.

Material and Mill Certification are in full compliance with the American Iron and Steel requirement as mandated in EPA's State Revolving Fund Programs and complies with the Buy American Act, (FTA) Buy America Requirements (49 CFR part 661), and (FHWA) Buy America Requirements (23 CFR part 635.410)

This material was tested using full-section samples.

Nolan Guess

Nolan Guess, Quality Supervisor

Page 1 of 1

NUCOR

Mill Certification
06/16/2025

MTR#:2018971-2
Lot #:380005688920
3630 Fourth Street
Flowood, MS 39232 US
601 939-1623
Fax: 601 936-6202

Sold To: REGAL METALS
207 SENTRY DR
MANSFIELD, TX 76063 US

Ship To: REGAL METALS INTERNATIONAL
207 SENTRY DR
MANSFIELD, TX 76063 US

Customer PO	BRIAN 60' YARD	Sales Order #	38031545 - 2.6
Product Group	Rebar	Product #	3019447
Grade	A615 Gr 60/AASHTO M31	Lot #	380005688920
Size	#5	Heat #	3800056889
BOL #	BOL-2066549	Load #	2019971
Description	Rebar #5/16mm A615 Gr 60/AASHTO M31 60' 0" [720"] 6001-10000 lbs	Customer Part #	
Production Date	05/29/2025	Qty Shipped LBS	36048
Product Country Of Origin	United States	Qty Shipped EA	576
Original Item Description		Original Item Number	

I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements.

Melt Country of Origin : United States

Melting Date: 05/24/2025

Roll Country of Origin : United States

Rolling Date: 05/29/2025

C (%)	Mn (%)	P (%)	S (%)	Si (%)	Ni (%)	Cr (%)	Mo (%)	Cu (%)	V (%)	Nb (%)
0.40	0.85	0.009	0.026	0.206	0.10	0.13	0.02	0.31	0.023	0.001

Mechanical

	Average Deformation Height (IN)	Band Test
(1)	0.039	Pass

Tensile testing

	Yield (PSI)	Tensile (PSI)	Elongation in 8" (%)
(1)	66400	99200	21.2

Other Test Results

Weight Percent Variance (%) : -3.79

Tensile / Yield Ratio : 1.50

Comments:

Nucor Steel Jackson, Inc. is in compliance with and certified to: ISO 9001:2015, ISO 14001:2015, ABS Quality Assurance Program & AASHTO's NTPEP Reinforcing Steel and Wire (REBAR) Technical Committee Work Plan. All manufacturing processes for this product, including melting, casting, and hot rolling, were performed in the United States of America.
Mercury not intentionally added at any point during manufacturing or testing of this material. No weld repair was performed.
Material and Mill Certification are in full compliance with the American Iron and Steel requirement as mandated in EPA's State Revolving Fund Programs and complies with the Buy American Act, (FTA) Buy America Requirements (49 CFR part 661), and (FHWA) Buy America Requirements (23 CFR part 635.410)
This material was tested using full-section samples.

Nolan Guess

Nolan Guess, Quality Supervisor

Page 1 of 1

NUCOR

Mill Certification

06/05/2025

MTR#:2011246-2
Lot #:38000568820
3630 Fourth Street
Flowood, MS 39232 US
601 939-1623
Fax: 601 936-6202

Sold To: REGAL METALS
207 SENTRY DR
MANSFIELD, TX 76063 US

Ship To: REGAL METALS INTERNATIONAL
207 SENTRY DR
MANSFIELD, TX 76063 US

Customer PO	YARD LOADS	Sales Order #	38031356 - 1.3
Product Group	Rebar	Product #	3019447
Grade	A615 Gr 60/AASHTO M31	Lot #	380005688820
Size	#5	Heat #	3800056888
BOL #	BOL-2053669	Load #	2011246
Description	Rebar #5/16mm A615 Gr 60/AASHTO M31 60' 0" [720"] 6001-10000 lbs	Customer Part #	
Production Date	05/29/2025	Qty Shipped LBS	36048
Product Country Of Origin	United States	Qty Shipped EA	576
Original Item Description		Original Item Number	

I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements.

Melt Country of Origin : United States

Melting Date: 05/24/2025

Roll Country of Origin : United States

Rolling Date: 05/29/2025

C (%)	Mn (%)	P (%)	S (%)	Si (%)	Ni (%)	Cr (%)	Mo (%)	Cu (%)	V (%)	Nb (%)
0.40	0.76	0.010	0.026	0.199	0.10	0.13	0.02	0.29	0.022	0.002

Mechanical

	Average Deformation Height (IN)	Bend Test
(1)	0.038	Pass

Tensile testing

	Yield (PSI)	Tensile (PSI)	Elongation in 8" (%)
(1)	64200	96400	17.5

Other Test Results

Weight Percent Variance (%) : -3.16

Tensile / Yield Ratio : 1.50

Comments:

Nucor Steel Jackson, Inc. is in compliance with and certified to: ISO 9001:2015, ISO 14001:2015, ABS Quality Assurance Program & AASHTO's NTPEP Reinforcing Steel and Wire (REBAR) Technical Committee Work Plan. All manufacturing processes for this product, including melting, casting, and hot rolling, were performed in the United States of America.

Mercury not intentionally added at any point during manufacturing or testing of this material. No weld repair was performed.

Material and Mill Certification are in full compliance with the American Iron and Steel requirement as mandated in EPA's State Revolving Fund Programs and complies with the Buy American Act, (FTA) Buy America Requirements (49 CFR part 661), and (FHWA) Buy America Requirements (23 CFR part 635.410)

This material was tested using full-section samples.

Nolan Guess

Nolan Guess, Quality Supervisor

Page 1 of 1

NUCOR**Mill Certification**

06/18/2025

MTR#:2027805-2
 Lot #:110006976920
 8812 HWY 79 W
 Jewett, TX 75846 US
 903 626-4461
 Fax: 903 626-6290

Sold To: REGAL METALS INTERNATIONAL
 207 SENTRY DR
 MANSFIELD, TX 76063 US

Ship To: REGAL METALS INTERNATIONAL
 207 SENTRY DR
 MANSFIELD, TX 76063 US

Customer PO	YARD LOAD 6/16	Sales Order #	11088570 - 2.2
Product Group	Rebar	Product #	2110230
Grade	A615 Gr 60/AASHTO M31	Lot #	110006976920
Size	#5	Heat #	1100069769
BOL #	BOL-2069005	Load #	2027805
Description	Rebar #5/16mm A615 Gr 60/AASHTO M31 40' 0" [480"] 4001-8000 lbs	Customer Part #	
Production Date	06/01/2025	Qty Shipped LBS	40050
Product Country Of Origin	United States	Qty Shipped EA	960
Original Item Description		Original Item Number	

I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements.

Melt Country of Origin : United States

Melting Date: 05/30/2025

Roll Country of Origin : United States

Rolling Date: 06/01/2025

C (%)	Mn (%)	P (%)	S (%)	Si (%)	Ni (%)	Cr (%)	Mo (%)	Cu (%)	V (%)	Nb (%)
0.35	1.08	0.019	0.017	0.197	0.16	0.30	0.04	0.31	0.004	0.001

Mechanical**Bend Test**

(1) Pass

Tensile testing

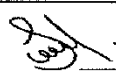
	Yield (PSI)	Tensile (PSI)	Elongation in 8" (%)
(1)	65000	101700	12.0

Other Test Results

Tensile / Yield Ratio : 1.56

Comments:

1. All manufacturing processes of the steel, including melting, casting & hot rolling, have been performed in U.S.A
2. Mercury not intentionally added at any point during manufacturing or testing of this material.
3. Welding or weld repair was not performed on this material.
4. This material conforms to the specifications described on this document and may not be reproduced, except in full, without written approval of Nucor Corporation.
5. Results reported ASTM E45 (inclusion content) and ASTM E381 (Macro-etch) are provided as interpretation of ASTM procedures.


 Ramon Vigil, Quality Supervisor

Page 1 of 1



CERTIFIED MATERIAL TEST REPORT

Page 1/1

CUSTOMER SHIP TO		CUSTOMER BILT TO		GRADE	SHAPE / SIZE	DOCUMENT ID:
REGAL METALS INTERNATIONAL INC.		REGAL METALS INTERNATIONAL INC.		60 (420)	Rebar / #4 (13MM)	0001216063
207 SENTRY DR. MANSFIELD, TX 76063-3609 USA		207 SENTRY DR. MANSFIELD, TX 76063-3609 USA		LENGTH 600"	WEIGHT 24.045 LB	HEAT / BATCH 5806407702
SALES ORDER 14783780000039		CUSTOMER MATERIAL N°		SPECIFICATION / DATE OF REVISION ASTM A615/A615M-24		

US-MT-MIDLOTHIAN
300 WARD ROAD
MIDLOTHIAN, TX 76065
USA

CUSTOMER PURCHASE ORDER NUMBER Yard 021725	BILL OF LADING 1327-0000614176	DATE 02/20/2025
---	-----------------------------------	--------------------

CHEMICAL COMPOSITION										
C (%)	Mn (%)	P (%)	S (%)	Si (%)	Ca (%)	Ni (%)	Cr (%)	Mo (%)	Sn (%)	V (%)
0.45	0.97	0.010	0.026	0.22	0.24	0.11	0.17	0.028	0.005	0.003
MECHANICAL PROPERTIES										
YS (ksi)	YS (MPa)	UTS (ksi)	UTS (MPa)	UTS (ksi)	UTS (MPa)	G/L (inches)	G/L (mm)	Elong. (%)	Bend Test	
74.532	513	114.510	789	8.000	200.0	16.50	OK			
MECHANICAL PROPERTIES										
UTS / YS										
1.54										

COMMENTS / NOTES

Gerda's steel is 100% recyclable. Support the circular economy through our Metals Recycling Partnership. For details, visit www2.gerdau.com/metal-recycling, or contact metalrecycling@gerdau.com.

The above figures are certified chemical and physical test records as contained in the permanent records of the company. We certify that these data are correct and in compliance with specified requirements. No weld repair was performed on this material. The material has not been in contact with mercury while in Gerda's possession. For all products other than billets or beam blanks, this material was Melting & Poured (via Electric Arc Furnace and Continuous Casting) and produced (Hot Rolled and, if applicable, Cold-Drawn) in the USA. For billets or beam blanks, this material was Melting & Poured (via Electric Arc Furnace and Continuous Casting) in the USA. CMTR complies with EN 10204 3.1.

Shackley
BHASKAR YALAMANCHILI
QUALITY DIRECTOR
Phone: (409) 267-1071 Email: Bhaskar.Yalamanchili@gerdau.com

De A. Jr.
WADE LAMPSON
QUALITY ASSURANCE MGR.
Phone: 972-779-3118 Email: Wade.Lampson@gerdau.com

Sentry 25-186

NUCOR

Mill Certification
06/12/2025

MTR# 2019969-3
Lot #: 380005692320
3630 Fourth Street
Flowood, MS 39232 US
601 939-1623
Fax: 601 936-6202

Sold To: REGAL METALS
207 SENTRY DR
MANSFIELD, TX 76063 US

Ship To: REGAL METALS INTERNATIONAL
207 SENTRY DR
MANSFIELD, TX 76063 US

Customer PO	BRIAN 60' YARD	Sales Order #	38031545 - 1.4
Product Group	Rebar	Product #	2110206
Grade	A615 Gr 60/AASHTO M31	Lot #	380005692320
Size	#4	Heat #	3800056923
BOL #	BOL-2062325	Load #	2019969
Description	Rebar #4/13mm A615 Gr 60/AASHTO M31 60' 0" [720"] 6001-10000 lbs	Customer Part #	
Production Date	06/01/2025	Qty Shipped LBS	27054
Product Country Of Origin	United States	Qty Shipped EA	675
Original Item Description		Original Item Number	

I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements.

Melt Country of Origin : United States

Melting Date: 05/25/2025

Roll Country of Origin : United States

Rolling Date: 06/01/2025

C (%)	Mn (%)	P (%)	S (%)	Si (%)	Ni (%)	Cr (%)	Mo (%)	Cu (%)	V (%)	Nb (%)
0.41	0.79	0.008	0.028	0.203	0.12	0.13	0.02	0.34	0.027	0.002

Mechanical

	Average Deformation Height (IN)	Bend Test
(1)	0.024	Pass

Tensile testing

	Yield (PSI)	Tensile (PSI)	Elongation in 8" (%)
(1)	68300	101100	15.0

Other Test Results

Weight Percent Variance (%) : -4.43

Tensile / Yield Ratio : 1.48

Comments:

Nucor Steel Jackson, Inc. is in compliance with and certified to: ISO 9001:2015, ISO 14001:2015, ABS Quality Assurance Program & AASHTO's NTPEP Reinforcing Steel and Wire (REBAR) Technical Committee Work Plan. All manufacturing processes for this product, including melting, casting, and hot rolling, were performed in the United States of America.

Mercury not intentionally added at any point during manufacturing or testing of this material. No weld repair was performed.

Material and Mill Certification are in full compliance with the American Iron and Steel requirement as mandated in EPA's State Revolving Fund Programs and complies with the Buy American Act, (FTA) Buy America Requirements (49 CFR part 661), and (FHWA) Buy America Requirements (23 CFR part 635.410)

This material was tested using full-section samples.

Nolan Guess

Nolan Guess, Quality Supervisor

Page 1 of 1



CMC STEEL TEXAS
1 STEEL MILL DRIVE
SEGUIN TX 78155-7510

1 SERIES-BPS®

EAT NO.: 3137924
SECTION: ROUND 3/4 x 20" A36/52950
GRADE: ASTM A36-19/A529-19 Gr 50 RD
MILL DATE: 04/04/2025
ELT DATE: 03/20/2025
Mfr. No.: 86392384 / 137924A457

CERTIFIED MILL TEST REPORT
For additional copies call
800-227-6489

We hereby certify that the test results presented here,
are accurate and conform to the reported grade specification

Drawn
Drawn M Fischer
Quality Assurance Manager

Triple S Steel Supply Co		Triple S Steel- Jensen		Delivery#: 86392384	
S	O	S	H	BOL#: 76682884	
L	D	I	I	CUST PO#: HOU-213284	
D	T	P	P	CUST P/N:	
T	O	US 77026-1113	US 77026-1113	DLVRY LBS / HEAT: 22830.000 LB	
		7136977105	7136977105	DLVRY PCS / HEAT: 760 EA	

Characteristic	Value	Characteristic	Value
C	0.10%	Elongation Gage Lgth test 1	8IN
Mn	1.09%	Reduction of Area test 1	61%
P	0.014%	Yield to tensile ratio test 1	0.74
S	0.024%	Yield Strength test 2	55.6ksi
Si	0.19%	Tensile Strength test 2	75.6ksi
Cu	0.26%	Elongation test 2	46%
Cr	0.06%	Elongation Gage Lgth test 2	2IN
Ni	0.08%	Reduction of Area test 2	57%
Mo	0.019%	Yield to tensile ratio test 2	0.74
V	0.000%	BHN @ Surface test 1	0BHN
Co	0.009%		
Sn	0.009%		
Al	0.002%		
N	0.0106%		
Carbon Eq F1554	0.30%		
Carbon Eq A529	0.35%		
Yield Strength test 1	55.2ksi		
Tensile Strength test 1	74.6ksi		
Elongation test 1	28%		

The Following is true of the material represented by this MTR:

- *Material is fully killed and is Hot Rolled Steel
- *100% melted, rolled, and manufactured in the USA
- *EN10204:2004 3.1 compliant *Contains no weld repair
- *Contains no Mercury contamination
- *Manufactured in accordance with the latest version of the plant quality manual
- *Meets the "Buy America" requirements of 23 CFR 635.410, 49 CFR 661
- *Warning: This product can expose you to chemicals which are known to the State of California to cause cancer, birth defects or other reproductive harm. For more information go to www.P65Warnings.ca.gov
- *THE RECORDING OF FALSE, FICTITIOUS OR FRAUDULENT STATEMENTS OR ENTRIES ON THIS DOCUMENT MAY BE PUNISHABLE AS A FELONY UNDER FEDERAL STATUTE

ARKS : ALSO MEETS ASTM GRADE A36, A529-50, A572-50, A709-36, A709-50, A992, AASHTO M270-36, M270-50, CSA G40.21-04 44W, 50W

IT MEETS THE REQUIREMENTS OF F1554, A529-50, A572-50, A709-36, A709-50, A992, AASHTO M270-36, M270-50, CSA G40.21-04 44W, 50W

SUMMIT PRECAST CONCRETE
PO: 25-188
PART: 250548 TTI LOOP CONN
END LOOPS HDG

UFLD



CMC STEEL TEXAS
1 STEEL MILL DRIVE
SEGUIN TX 78155-7510

CERTIFIED MILL TEST REPORT
For additional copies call
800-227-6489

We hereby certify that the test results presented here
are accurate and conform to the reported grade specification

Drew M. Fisher
Drew M. Fisher
Quality Assurance Manager

1SERIES-BPS®

AT NO.: 3133243
CTION: ROUND 3/4 x 20"0" A36/52950
ADE: ASTM A36-19/A529-19 Gr 50 RD
LL DATE: 04/04/2025
LT DATE: 08/26/2024
L No.: 86279742 / 133243A457

S O'Neal Steel Inc
O
L 4530 MESSER AIRPORT HWY
D BIRMINGHAM AL
US 35222-1627
T 2055998000
O

S O'Neal Steel
H
I 4005 Grand Lakes Way
P Grand Prairie TX
US 75050-0000
T 9724027945
O

Delivery#: 86279742
BOL#: 76567623
CUST PO#: 722550
CUST P/N: 834718
DLVRY LBS / HEAT: 4566.000 LB
DLVRY PCS / HEAT: 152 EA

Characteristic	Value	Characteristic	Value	Characteristic	Value
C	0.16%	Elongation Gage Lgth test 1	8IN	The Following is true of the material represented by this MTR: *Material is fully killed and is Hot Rolled Steel *100% melted, rolled, and manufactured in the USA *EN10204:2004 3.1 compliant *Contains no weld repair *Contains no Mercury contamination *Manufactured in accordance with the latest version of the plant quality manual *Meets the "Buy America" requirements of 23 CFR635.410, 46 CFR 661 *Warning: This product can expose you to chemicals which are known to the State of California to cause cancer, birth defects or other reproductive harm. For more information go to www.P65Warnings.ca.gov *THE RECORDING OF FALSE, FICTITIOUS OR FRAUDULENT STATEMENTS OR ENTRIES ON THIS DOCUMENT MAY BE PUNISHABLE AS A FELONY UNDER FEDERAL STATUTE	
Mn	0.75%	Reduction of Area test 1	51%		
P	0.009%	Yield to tensile ratio test1	0.72		
S	0.023%	Yield Strength test 2	62.4ksi		
Si	0.21%	Tensile Strength test 2	73.4ksi		
Cu	0.41%	Elongation test 2	50%		
Cr	0.05%	Elongation Gage Lgth test 2	2IN		
Ni	0.09%	Reduction of Area test 2	57%		
Mo	0.020%	Yield to tensile ratio test2	0.71		
V	0.014%	BHN @ Surface test 1	149BHN		
Cb	0.001%				
Sn	0.010%				
Al	0.005%				
N	0.0154%				
Carbon Eq F1554	0.30%				
Carbon Eq A529	0.37%				
Yield Strength test 1	52.6ksi				
Tensile Strength test 1	72.8ksi				
Elongation test 1	26%				

ALSO MEETS ASTM GRADE A36, A529-50, A572-50, A709-36, A709-50, A992, AASHTO M270-36, M270-50, CSA G40.21-04 44W, 50W
MEETS THE REQUIREMENTS OF F1554 GRADE 36 SUPPLEMENT S1

SUMMIT PRECAST CONCRETE
PO: 25-188
PART: 250548 TTI LOOP CONN
END LOOPS HDG

UF4547



UNI-FAB
CERTIFICATE OF MATERIAL
SPECIFICATIONS AND WORKMANSHIP

DATE: 8/6/25

PO# 144173

JOB: 73592

PART NUMBER: 250548 TTI LOOP CONN

PART DESCRIPTION: END LOOPS HDG

CUST PO: 25-188 LINE 1

S/N: TRACER 1 -210

Material: A36

HL: UF4547 /HT# 3133243, UF4610 /HT# 3137924

QUANTITY: 210

SPECIAL PROCESS: MANUFACTURED PER PRINT

COUNTRY OF ORIGIN: United States of America

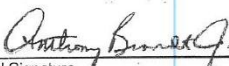
The materials, processes, and workmanship all conform to the requirements of all applicable specifications, drawings, and the purchase order supplied to Uni-Fab. The appropriate documentation providing traceability is on file at Uni-Fab. It is available for review by authorized customer representatives.

Serial No.	25-188-1-71, 25-188-1-72, 25-188-1-73, 25-188-1-74, 25-188-1-75
Serial No.	25-188-1-76, 25-188-1-77, 25-188-1-78, 25-188-1-79, 25-188-1-80
Serial No.	25-188-1-81, 25-188-1-82, 25-188-1-83, 25-188-1-84, 25-188-1-85
Serial No.	25-188-1-86, 25-188-1-87, 25-188-1-88, 25-188-1-89, 25-188-1-90
Serial No.	25-188-1-91, 25-188-1-92, 25-188-1-93, 25-188-1-94, 25-188-1-95
Serial No.	25-188-1-96, 25-188-1-97, 25-188-1-98, 25-188-1-99, 25-188-1-100
Serial No.	25-188-1-101, 25-188-1-102, 25-188-1-103, 25-188-1-104, 25-188-1-105
Serial No.	25-188-1-106, 25-188-1-107, 25-188-1-108, 25-188-1-109, 25-188-1-110
Serial No.	25-188-1-111, 25-188-1-112, 25-188-1-113, 25-188-1-114, 25-188-1-115
Serial No.	25-188-1-116, 25-188-1-117, 25-188-1-118, 25-188-1-119, 25-188-1-120
Serial No.	25-188-1-121, 25-188-1-122, 25-188-1-123, 25-188-1-124, 25-188-1-125
Serial No.	25-188-1-126, 25-188-1-127, 25-188-1-128, 25-188-1-129, 25-188-1-130
Serial No.	25-188-1-131, 25-188-1-132, 25-188-1-133, 25-188-1-134, 25-188-1-135
Serial No.	25-188-1-136, 25-188-1-137, 25-188-1-138, 25-188-1-139, 25-188-1-140
Serial No.	25-188-1-141, 25-188-1-142, 25-188-1-143, 25-188-1-144, 25-188-1-145
Serial No.	25-188-1-146, 25-188-1-147, 25-188-1-148, 25-188-1-149, 25-188-1-150
Serial No.	25-188-1-151, 25-188-1-152, 25-188-1-153, 25-188-1-154, 25-188-1-155
Serial No.	25-188-1-156, 25-188-1-157, 25-188-1-158, 25-188-1-159, 25-188-1-160
Serial No.	25-188-1-161, 25-188-1-162, 25-188-1-163, 25-188-1-164, 25-188-1-165
Serial No.	25-188-1-166, 25-188-1-167, 25-188-1-168, 25-188-1-169, 25-188-1-170
Serial No.	25-188-1-171, 25-188-1-172, 25-188-1-173, 25-188-1-174, 25-188-1-175
Serial No.	25-188-1-176, 25-188-1-177, 25-188-1-178, 25-188-1-179, 25-188-1-180
Serial No.	25-188-1-181, 25-188-1-182, 25-188-1-183, 25-188-1-184, 25-188-1-185
Serial No.	25-188-1-186, 25-188-1-187, 25-188-1-188, 25-188-1-189, 25-188-1-190
Serial No.	25-188-1-191, 25-188-1-192, 25-188-1-193, 25-188-1-194, 25-188-1-195
Serial No.	25-188-1-196, 25-188-1-197, 25-188-1-198, 25-188-1-199, 25-188-1-200
Serial No.	25-188-1-201, 25-188-1-202, 25-188-1-203, 25-188-1-204, 25-188-1-205
Serial No.	25-188-1-206, 25-188-1-207, 25-188-1-208, 25-188-1-209, 25-188-1-210

CERT ENVELOPE

COUNTRY OF ORIGIN: USA

The materials, processes, and workmanship all conform to the requirements of all applicable specifications, drawings, and the purchase order supplied to Craig Godwin, Inc. dba. The appropriate documentation providing traceability is on file at Craig Godwin, Inc. dba. It is available for review by authorized customer representatives.


 Authorized Signature
 Craig Godwin, Inc. dba

UMW PO 25-188



United Machine Works

Craig Godwin, Inc. dba

Certificate of Conformance

To: SUMMIT PRECAST CONCRETE, LP
9930 INDUSTRIAL DR
Navasota, TX 77868
USA

From: United Machine Works
P O Box 525
New Waverly, TX 77358
USA

Packing List No: 146058
Shipping Date: 08/06/2025

Today's Date: 08/06/2025
PO Number: 25-188

CERTIFICATION DOCUMENTS

<u>PO Line No.</u>	<u>Number</u>	<u>Revision</u>	<u>Description</u>	<u>Job No.</u>	<u>Unit</u>	<u>Shipped</u>	<u>Ordered</u>	<u>Back Ordered</u>
1	250548 TTI LOOP		END LOOPS HDG	73592	EA	210	210	0
	CONN							
	Serial No.	25-188-1-1, 25-188-1-2, 25-188-1-3, 25-188-1-4, 25-188-1-5						
	Serial No.	25-188-1-6, 25-188-1-7, 25-188-1-8, 25-188-1-9, 25-188-1-10						
	Serial No.	25-188-1-11, 25-188-1-12, 25-188-1-13, 25-188-1-14, 25-188-1-15						
	Serial No.	25-188-1-16, 25-188-1-17, 25-188-1-18, 25-188-1-19, 25-188-1-20						
	Serial No.	25-188-1-21, 25-188-1-22, 25-188-1-23, 25-188-1-24, 25-188-1-25						
	Serial No.	25-188-1-26, 25-188-1-27, 25-188-1-28, 25-188-1-29, 25-188-1-30						
	Serial No.	25-188-1-31, 25-188-1-32, 25-188-1-33, 25-188-1-34, 25-188-1-35						
	Serial No.	25-188-1-36, 25-188-1-37, 25-188-1-38, 25-188-1-39, 25-188-1-40						
	Serial No.	25-188-1-41, 25-188-1-42, 25-188-1-43, 25-188-1-44, 25-188-1-45						
	Serial No.	25-188-1-46, 25-188-1-47, 25-188-1-48, 25-188-1-49, 25-188-1-50						
	Serial No.	25-188-1-51, 25-188-1-52, 25-188-1-53, 25-188-1-54, 25-188-1-55						
	Serial No.	25-188-1-56, 25-188-1-57, 25-188-1-58, 25-188-1-59, 25-188-1-60						
	Serial No.	25-188-1-61, 25-188-1-62, 25-188-1-63, 25-188-1-64, 25-188-1-65						
	Serial No.	25-188-1-66, 25-188-1-67, 25-188-1-68, 25-188-1-69, 25-188-1-70						



www.portlandbolt.com
sales@portlandbolt.com

Sales Order No. 185017

Date 6/24/2025
Salesperson Dan Karpan
Email dan@portlandbolt.com
Phone 800.599.0538

PB Northwest 800.547.6758 3441 NW Guam St. Portland, OR 97210	PB Southeast 800.631.2076 890 W Five Notch Rd. North Augusta, SC 29860	PB Northeast 833.701.4125 12 Elbridge St. Jordan, NY 13080
---	--	--

Sold To
936.701.1977
SUMMIT PRECAST CONCRETE
15349 SUMMIT PARK DR.
SUITE 101
MONTGOMERY, TX 77356

Ship To
SUMMIT PRECAST CONCRETE
9930 Industrial Drive
Navasota, TX 77868

Attention Toby<toby@summitprecast.com>	Terms Full Payment Before shipping	Customer PO Credit Card
--	--	-----------------------------------

Ship Date (scheduled) 7/30/2025	Delivery Best Way (Prepaid)	Certs Emailed Mill Test Reports
---	---------------------------------------	---

Comments

No.	Qty	UOM	Description
1	34	EA	1 X 29 galv. A449 [OR] barrier pin with 2" ring
2	0	EA	FREIGHT CHARGES

Total Weight (lbs.) 236.66



CERTIFIED MATERIAL TEST REPORT

Page 2 / 2

CUSTOMER SHIP TO PLAINFIELD 14636 S DEPOT DRIVE PLAINFIELD, IL 60544 USA		CUSTOMER DEL TO R L PERLOW CORPORATION 14636 S DEPOT DRIVE PLAINFIELD, IL 60544-7709 USA		GRADE 4140HR2	SHAPE / SIZE Round Bar / 1"	DOCUMENT ID: 0001220752
SALES ORDER 146133904000010		CUSTOMER MATERIAL N° A1.0904140GAS A		LENGTH 2106"	WEIGHT 6.659 LB	HEAT / BATCH 58064340006
CUSTOMER PURCHASE ORDER NUMBER P5454		BILL OF LADING 1327-0000615677		DATE 03/01/2025		SPECIFICATION / DATE OF REVISION ASTM A29-23 ASTM A304-20 ASTM A322-18

COMMENTS / NOTES

Metals or exceeds SAE 1422, S-S, O-S

GerdaU steel is 100% recyclable. Support the circular economy through our Metals Recycling Partnership. For details, visit www2.gerdau.com/metals-recycling, or contact metalsrecycling@gerdau.com.

The above figures are certified chemical and physical test records as contained in the permanent records of the company. We certify that these data are correct and in compliance with specified requirements. No weld repair was performed on this material. The material has not been in contact with mercury while in GerdaU's possession. For all products other than billets or beam blanks, this material was Melbed & Powder (via Electric Arc Furnace and Continuous Cast) and produced (Hot Rolled and, if applicable, Cold-Drawn) in the USA. For billets or beam blanks, this material was Melbed & Powder (via Electric Arc Furnace and Continuous Cast) in the USA. CMTR complies with EN 10204 3.1.

Maskey
BRASCAK YALAMANCHIL
QUALITY DIRECTOR
Phone: (409) 367-1071 Email: Brasack.Yalamanchil@gerdau.com

Wade A. Hie
WADE LUMPKENS
QUALITY ASSURANCE MGR.
Phone: 972-779-3118 Email: Wade.Lumpkins@gerdau.com



US-MI-MIDLOTHIAN
300 WARD ROAD
MIDLOTHIAN, TX 76065
USA

CUSTOMER SHIP TO
PLAINFIELD
14636 S DEPOT DRIVE
PLAINFIELD, NJ 08044
USA

CUSTOMER BIL TO
R L PERLOW CORPORATION
14636 S DEPOT DRIVE
PLAINFIELD, NJ 08044-7709
USA

GRADE
4140HR2

SHAPE / SIZE
Round Bar / 1"

DOCUMENT ID:
0001220752

LENGTH
21'06"

WEIGHT
6,659 LB

HEAT / BATCH
58064340/06

CERTIFIED MATERIAL TEST REPORT

18173 2837575

Page 1 / 2

CUSTOMER PURCHASE ORDER NUMBER
P5454

BILL OF LADING
1327-0000615677

DATE
03/01/2025

SALES ORDER
14613390/000010

CUSTOMER MATERIAL N°
A1.0004140GAS A

SPECIFICATION / DATE OF REVISION
ASTM A29-23
ASTM A304-20
ASTM A322-18

CHEMICAL COMPOSITION		P (%)	S (%)	Si (%)	Cu (%)	Ni (%)	Cr (%)	Mo (%)	Sn (%)	V (%)	Nb (%)	Al (%)	Ti (%)	B (%)
C (%)	Mn (%)	0.009	0.028	0.24	0.30	0.09	0.92	0.228	0.008	0.028	0.000	0.001	0.003	0.0000
0.41	0.88													

GEOMETRIC CHARACTERISTICS
R/R
33.8

METALLURGICAL CHARACTERISTICS		ESR1 S	ESR1 R	ESR1 C
Linea:	OK	1	1	1

HARDENABILITY		H (HRC)	J (HRC)	K (HRC)	L (HRC)	M (HRC)	N (HRC)	O (HRC)	P (HRC)	Q (HRC)	R (HRC)	S (HRC)	T (HRC)	U (HRC)	V (HRC)	W (HRC)	X (HRC)	Y (HRC)	Z (HRC)
DI A555 (Inches)	6.02	56	56	56	56	56	56	56	56	56	56	56	56	56	56	56	56	56	56

HARDENABILITY		J16 (HRC)	J18 (HRC)	J20 (HRC)	J24 (HRC)	J28 (HRC)	J32 (HRC)
50	50	49	46	45	42		

The above figures are certified chemical and physical test records as contained in the permanent records of the company. We certify that these data are correct and in compliance with specified requirements. No weld repair was performed on this material. The material has not been in contact with mercury while in Gerda's possession. For all products other than billets or beam blanks, this material was Melled & Poured (via Electric Arc Furnace and Continuous Cast) and produced (Hot Rolled and, if applicable, Cold Drawn) in the USA. For billets or beam blanks, this material was Melled & Poured (via Electric Arc Furnace and Continuous Cast) in the USA. CMTR complies with EN 10204 3.1.

Maskey
BHASIKAR VALAVANTH
QUALITY DIRECTOR

Phone: (409) 267-1071 Email: Bhasikar.Valavanth@gerdau.com

Wade A. Lunsford
WADE LUNSFORD
QUALITY ASSURANCE MGR.

Phone: 972-779-3118 Email: Wade.Lunsford@gerdau.com



FOR	SUMMIT PRECAST CONCRETE
PB INVOICE	185017
CUSTOMER PO	Credit Card
SHIP DATE	07/29/2025

Certificate of Conformance

We certify that the following items were manufactured and tested in accordance with the chemical, mechanical, dimensional and thread fit requirements of the specifications referenced.

1 X 29 GALV. A449 [OR] BARRIER PIN WITH 2" RING

HEAT	58064340	BASE STEEL	4140AR	DIAMETER	1.000	SOURCE	PERLOW STEEL CORP	
C	CR	CU	MN	MO	NI	P	S	SI
0.410	0.920	0.300	0.880	0.228	0.090	0.009	0.028	0.240

Coatings

- ASTM F2329 and A153 cl.C Hot Dip Galvanizing

Certification Department Quality Assurance
Dane McKinnon

APPENDIX E.

MASH TEST 3-10 (CRASH TEST 620281-01-1)

E.1. VEHICLE PROPERTIES AND INFORMATION

Date: 2025-10-16 Test No.: 620281-01-1 VIN No.: 3N1CN7AP2JL818260

Year: 2018 Make: Nissan Model: Versa

Tire Inflation Pressure: 36 PSI Odometer: 46,373 Tire Size: P185/65R15

Describe any damage to the vehicle prior to test: None

- Denotes accelerometer location.

NOTES: None

Engine Type: 4 CYL

Engine CID: 1.6 L

Transmission Type:

☒ Auto or ☐ Manual
☒ FWD ☐ RWD ☐ 4WD

Optional Equipment:

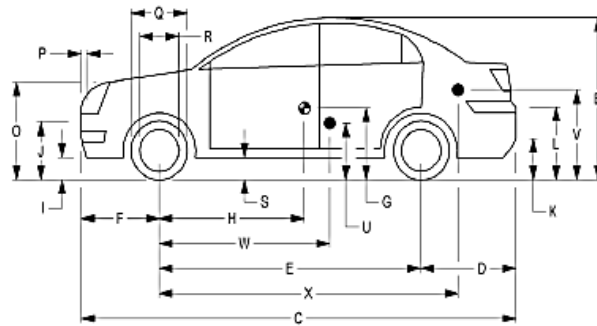
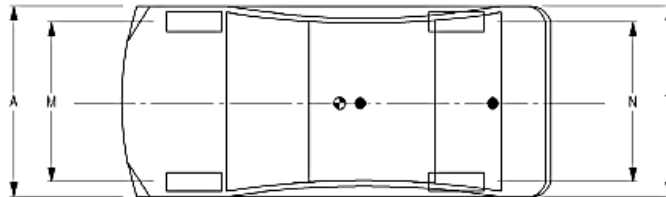
None

Dummy Data:

Type: 50th Percentile Male

Mass: 165 lb

Seat Position:



Geometry: inches

A 66.70	F 32.50	K 12.50	P 4.50	U 15.50
B 59.60	G	L 26.00	Q 24.00	V 21.25
C 175.40	H 41.60	M 58.30	R 16.25	W
D 40.50	I 7.00	N 58.50	S 7.50	X 79.75
E 102.40	J 22.50	O 30.50	T 64.50	
Wheel Center Ht Front 11.50	Wheel Center Ht Rear 11.50	W-H -41.60		

RANGE LIMIT: A = 65 ±3 inches; C = 169 ±8 inches; E = 98 ±5 inches; F = 35 ±4 inches; H = 39 ±4 inches; O (Top of Radiator Support) = 28 ±4 inches
(M+N)/2 = 59 ±2 inches; W-H < 2 inches or use MASH Paragraph A4.3.2

GVWR Ratings:

Front	1750
Back	1687
Total	3389

Mass: lb

M _{front}	1434
M _{rear}	988
M _{Total}	2422

Curb

Test Inertial

1455
998
2453

Gross Static

0

Allowable TIM = 2420 lb ±55 lb | Allowable GSM = 2585 lb ± 55 lb

Mass Distribution:

lb LF: 735 RF: 720 LR: 510 RR: 488

Figure E.1. Vehicle Properties for Test 620281-01-1.

Date: 2025-10-16 Test No.: 620281-01-1 VIN No.: 3N1CN7AP2JL81826
 Year: 2018 Make: Nissan Model: Versa

VEHICLE CRUSH MEASUREMENT SHEET¹

Complete When Applicable	
End Damage	Side Damage
Undeformed end width _____ Corner shift: A1 _____ A2 _____ End shift at frame (CDC) (check one) < 4 inches _____ ≥ 4 inches _____	Bowing: B1 _____ X1 _____ B2 _____ X2 _____ Bowing constant $\frac{X1 + X2}{2} = \underline{\hspace{2cm}}$

Note: Measure C₁ to C₆ from Driver to Passenger Side in Front or Rear Impacts – Rear to Front in Side Impacts.

Specific Impact Number	Plane* of C-Measurements	Direct Damage		Field L**	C ₁	C ₂	C ₃	C ₄	C ₅	C ₆	±D
		Width** (CDC)	Max*** Crush								
1	AFB	9	19	14							-21
1	AFB	21	12	48							88
	Measurements recorded										
	☒ inches or ☐ mm										

¹Table taken from National Accident Sampling System (NASS).

*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

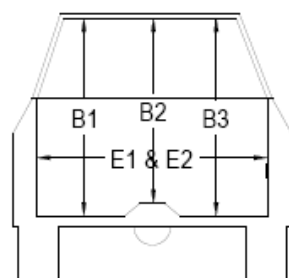
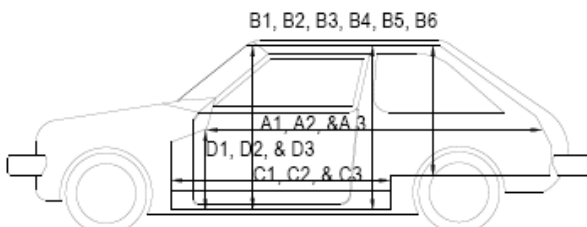
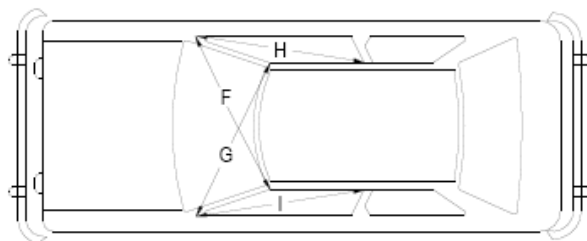
**Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

***Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

Figure E.2. Exterior Crush Measurements for Test 620281-01-1.

Date: 2025-10-16 Test No.: 620281-01-1 VIN No.: 3N1CN7AP2JL81826
 Year: 2018 Make: Nissan Model: Versa



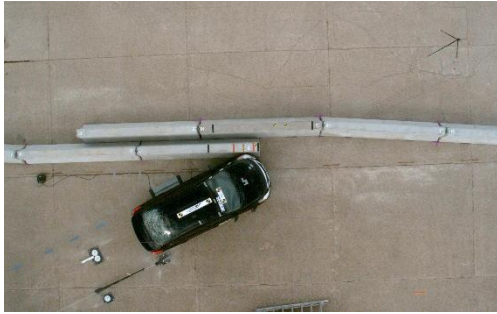
*Lateral area across the cab from driver's side kick panel to passenger's side kick panel.

OCCUPANT COMPARTMENT DEFORMATION MEASUREMENT

	Before	After (inches)	Differ.
A1	67.50	67.50	0.00
A2	67.25	67.25	0.00
A3	67.75	67.75	0.00
B1	40.50	40.50	0.00
B2	39.00	39.00	0.00
B3	40.50	40.50	0.00
B4	36.25	36.25	0.00
B5	36.00	36.00	0.00
B6	36.25	36.25	0.00
C1	26.00	24.50	-1.50
C2	0.00	0.00	0.00
C3	26.00	26.00	0.00
D1	9.50	9.00	-0.50
D2	0.00	0.00	0.00
D3	9.50	9.50	0.00
E1	51.50	51.50	0.00
E2	51.00	51.00	0.00
F	51.00	51.00	0.00
G	51.00	51.00	0.00
H	37.50	37.50	0.00
I	37.50	37.50	0.00
J*	51.00	49.50	-1.50

Figure E.3. Occupant Compartment Measurements for Test 620281-01-1.

E.2.SEQUENTIAL PHOTOGRAPHS



(a) 0.000 s



(b) 0.1000 s



(c) 0.2000 s



(d) 0.3000 s



(e) 0.4000 s



(f) 0.5000 s



(g) 0.6000 s



(h) 0.7000 s

**Figure E.4. Sequential Photographs for Test 620281-01-1
(Overhead Views).**



(a) 0.000 s



(b) 0.1000 s



(c) 0.2000 s



(d) 0.3000 s



(e) 0.4000 s



(f) 0.5000 s



(g) 0.6000 s



(h) 0.7000 s

Figure E.5. Sequential Photographs for Test 620281-01-1 (Downstream In-line Views).



(a) 0.000 s



(b) 0.1000 s



(c) 0.2000 s



(d) 0.3000 s



(e) 0.4000 s



(f) 0.5000 s



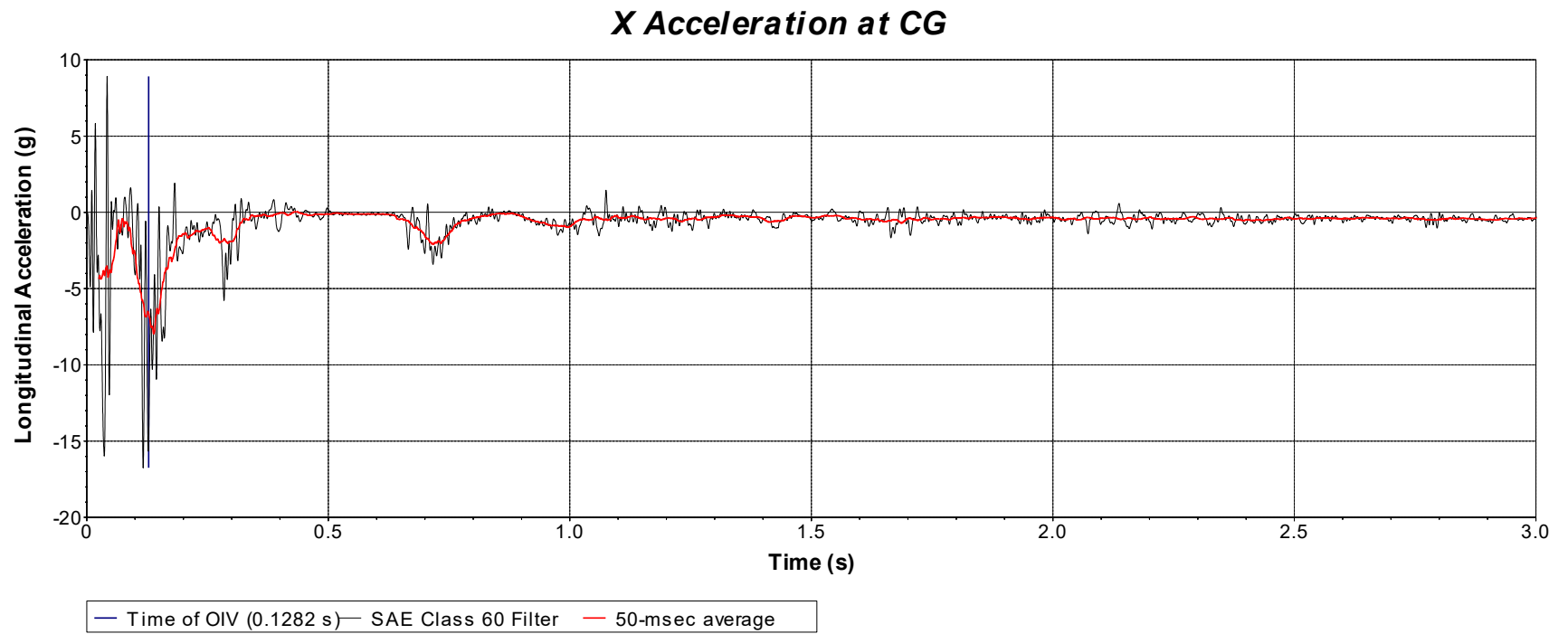
(g) 0.6000 s



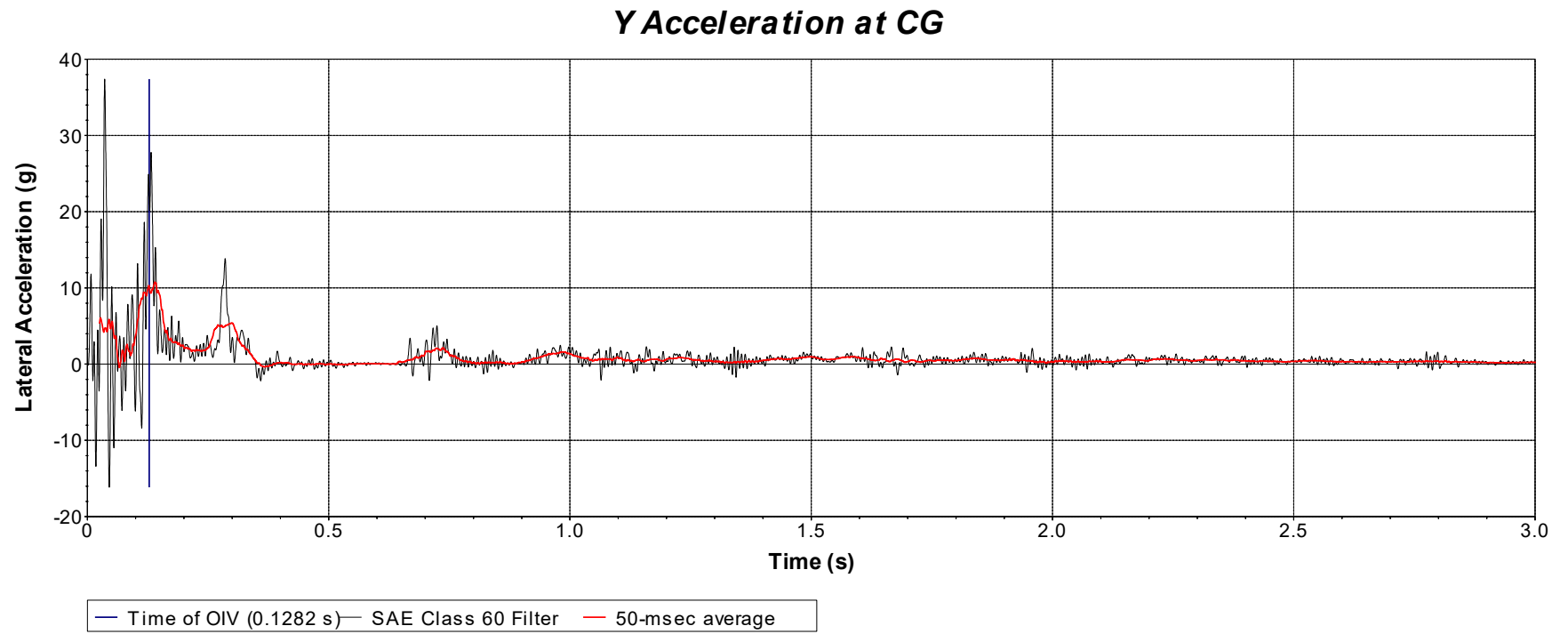
(h) 0.7000 s

**Figure E.6. Sequential Photographs for Test 620281-01-1
(Upstream Field Side Oblique Views).**

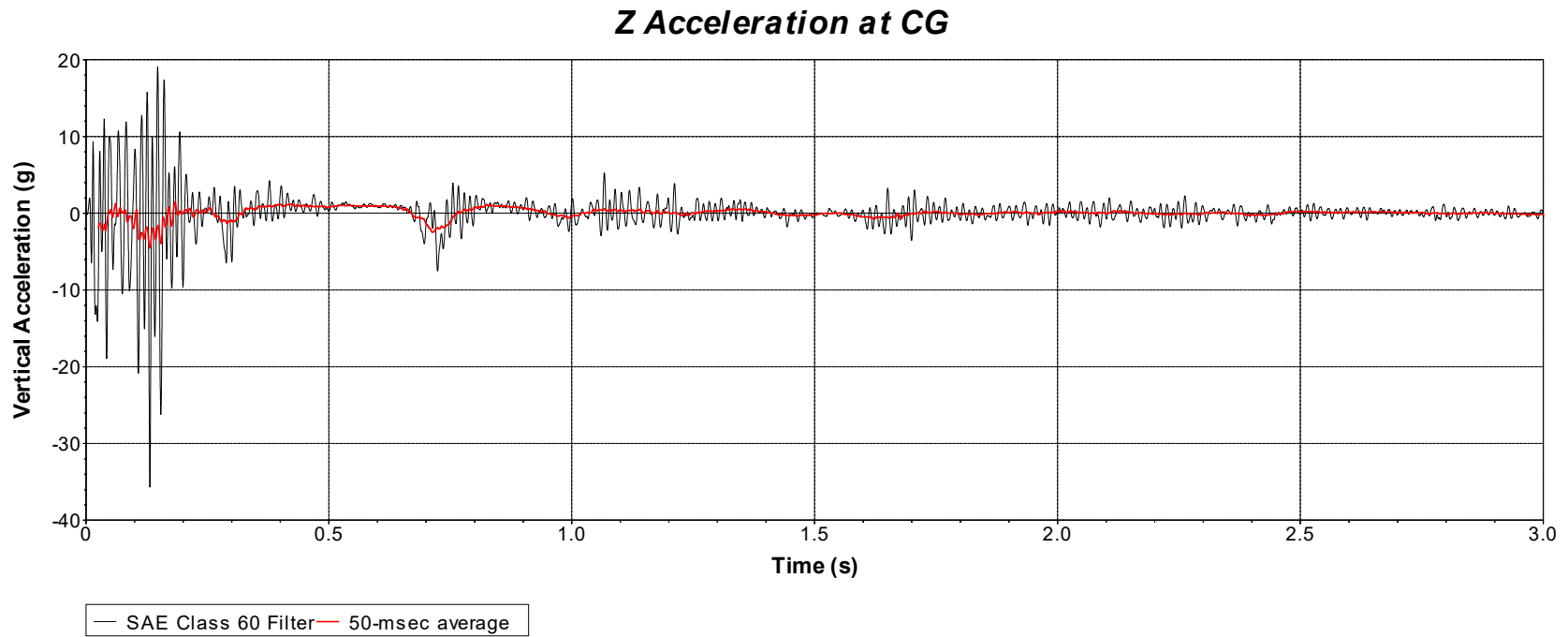
E.3.VEHICLE ACCELERATIONS



**Figure E.7. Vehicle Longitudinal Accelerometer Trace for Test 620281-01-1
(Accelerometer Located at Center of Gravity).**



**Figure E.8. Vehicle Lateral Accelerometer Trace for Test 620281-01-1
(Accelerometer Located at Center of Gravity).**



**Figure E.9. Vehicle Vertical Accelerometer Trace for Test 620281-01-1
(Accelerometer Located at Center of Gravity).**

APPENDIX F.

MASHTEST 3-11 (CRASH TEST 620281-01-2)

F.1. VEHICLE PROPERTIES AND INFORMATION

Date: 2025-10-23 Test No.: 620281-01-2 VIN No.: 1C6RR6FT2K5745736
 Year: 2019 Make: RAM Model: 1500
 Tire Size: 265/70 R 17 Tire Inflation Pressure: 35 psi
 Tread Type: Highway Odometer: 133,830
 Note any damage to the vehicle prior to test: None

• Denotes accelerometer location.

NOTES: None

Engine Type: V-8
 Engine CID: 5.7 liter

Transmission Type:
☒ Auto or ☐ Manual
☐ FWD ☒ RWD ☐ 4WD

Optional Equipment:
None

Dummy Data:
 Type: 50th Percentile Male
 Mass: 165 lb
 Seat Position:

Geometry: inches

A	78.50	F	40.00	K	20.00	P	3.00	U	26.75
B	74.00	G	28.75	L	30.00	Q	30.50	V	30.25
C	227.50	H	61.40	M	68.50	R	18.00	W	0.00
D	44.00	I	11.75	N	68.00	S	13.00	X	79.00
E	140.50	J	27.00	O	46.00	T	77.00		
Wheel Center Height Front	14.75	Wheel Well Clearance (Front)	6.00	Bottom Frame Height - Front	12.50				
Wheel Center Height Rear	14.75	Wheel Well Clearance (Rear)	9.25	Bottom Frame Height - Rear	22.50				

RANGE LIMIT: A=78 ±2 inches; C=237 ±13 inches; E=148 ±12 inches; F=39 ±3 inches; G=> 28 inches; H= 63 ±4 inches; O=43 ±4 inches; (M+N)/2=67 ±1.5 inches

GVWR Ratings:	Mass: lb	Curb	Test Inertial	Gross Static
Front	3700	M _{front}	2921	2839
Back	3900	M _{rear}	2051	2205
Total	6700	M _{Total}	4972	5044
				5209

(Allowable Range for TIM and GSM = 5000 lb ±110 lb)

Mass Distribution:
 lb

LF: 1459 RF: 1380 LR: 1080 RR: 1125

Figure F.1. Vehicle Properties for Test 620281-01-2.

Date:	2025-10-23	Test No.:	620281-01-2	VIN No.:	1C6RR6FT2K5745736
Year:	2019	Make:	RAM	Model:	1500

VEHICLE CRUSH MEASUREMENT SHEET¹

Complete When Applicable	
End Damage	Side Damage
Undeformed end width _____	Bowing: B1 _____ X1 _____
Corner shift: A1 _____	B2 _____ X2 _____
A2 _____	
End shift at frame (CDC)	Bowing constant
(check one)	$\frac{X1 + X2}{2} = \underline{\hspace{2cm}}$
< 4 inches _____	
≥ 4 inches _____	

Note: Measure C₁ to C₆ from Driver to Passenger Side in Front or Rear Impacts – Rear to Front in Side Impacts.

[illegible]

¹Table taken from National Accident Sampling System (NASS).

*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc.

Record the value for each C-measurement and maximum crush.

**Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

***Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

Figure F.2. Exterior Crush Measurements for Test 620281-01-2.

Date: 2025-10-23 Test No.: 620281-01-2 VIN No.: 1C6RR6FT2K5745736
Year: 2019 Make: RAM Model: 1500

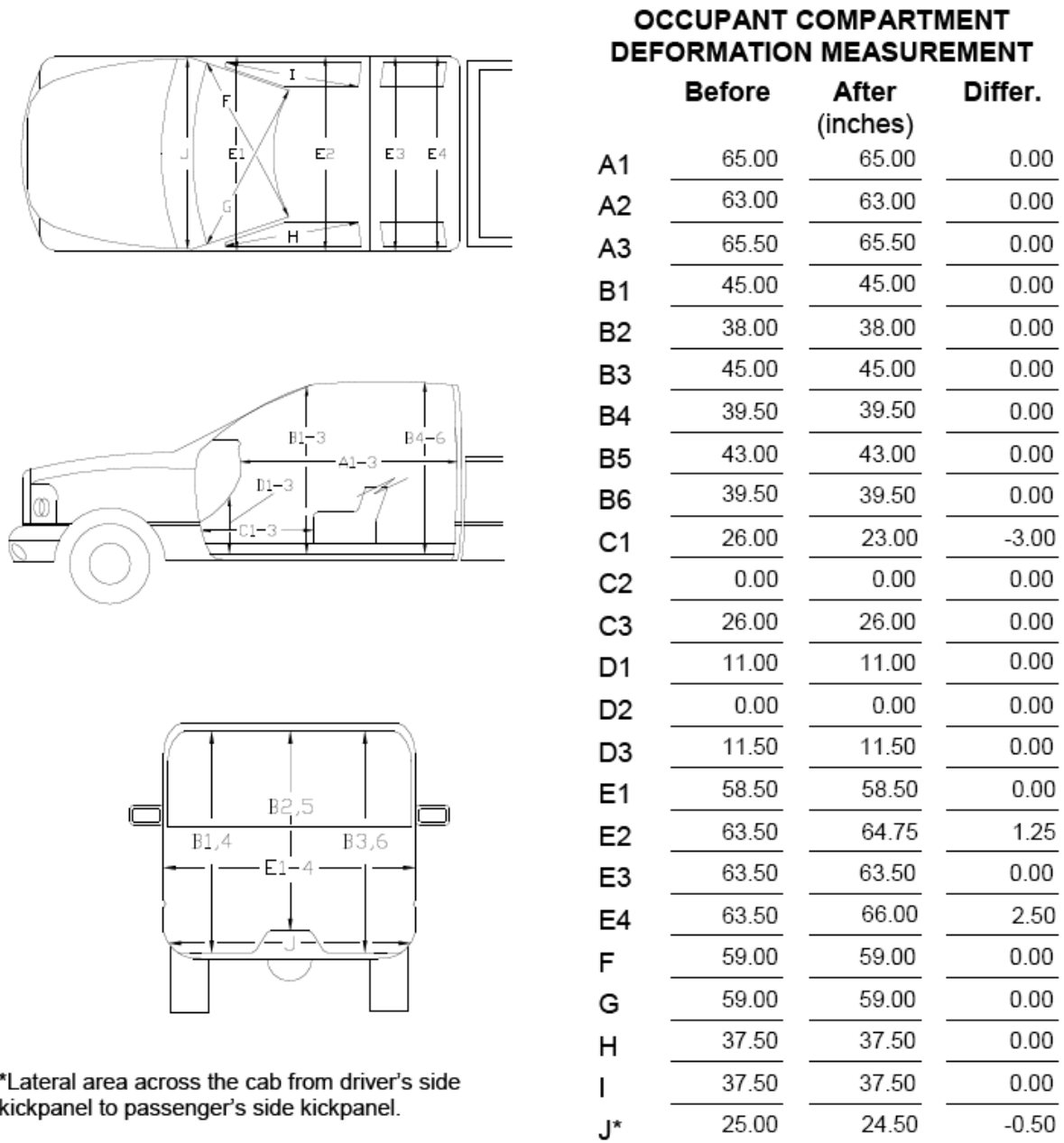


Figure F.3. Occupant Compartment Measurements for Test 620281-01-2.

F.2. SEQUENTIAL PHOTOGRAPHS



(a) 0.000 s



(b) 0.1000 s



(c) 0.2000 s



(d) 0.3000 s



(e) 0.4000 s



(f) 0.5000 s



(g) 0.6000 s



(h) 0.7000 s

Figure F.4. Sequential Photographs for Test 620281-01-2 (Overhead Views).



(a) 0.000 s



(b) 0.1000 s



(c) 0.2000 s



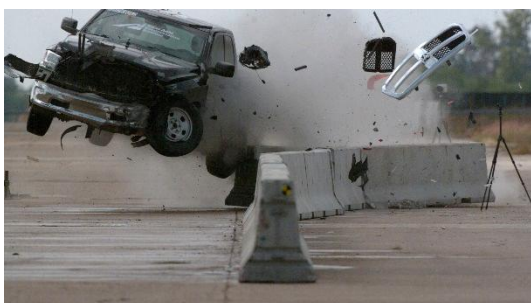
(d) 0.3000 s



(e) 0.4000 s



(f) 0.5000 s



(g) 0.6000 s



(h) 0.7000 s

Figure F.5. Sequential Photographs for Test 620281-01-2 (Downstream In-line Views).



(a) 0.000 s



(b) 0.1000 s



(c) 0.2000 s



(d) 0.3000 s



(e) 0.4000 s



(f) 0.5000 s



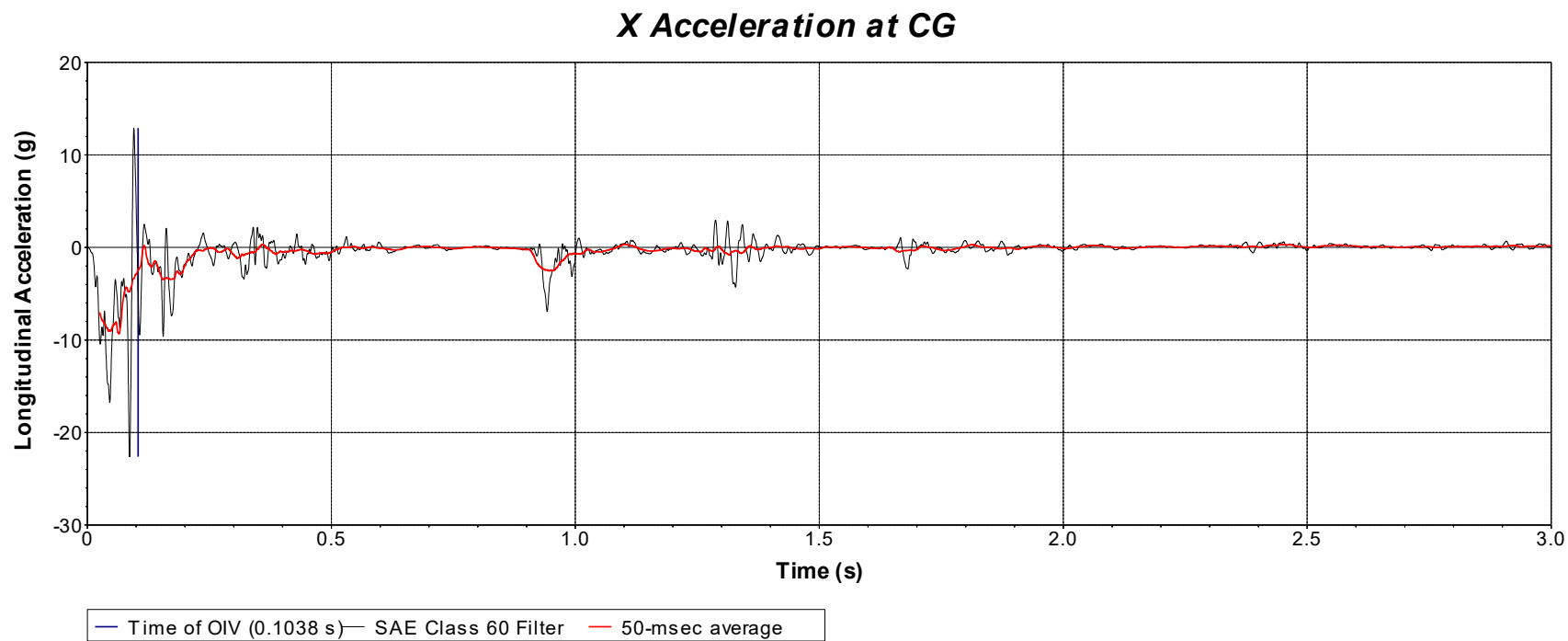
(g) 0.6000 s



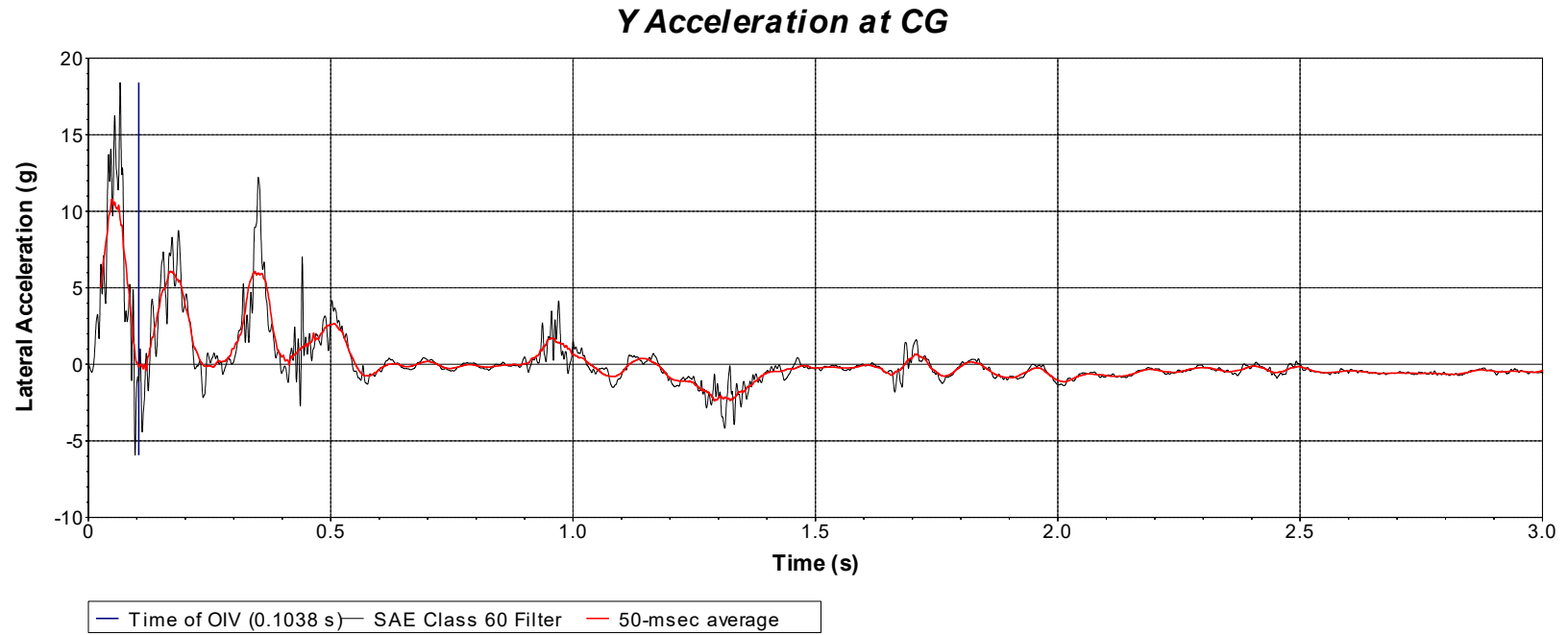
(h) 0.7000 s

**Figure F.6. Sequential Photographs for Test 620281-01-2
(Upstream Field Side Oblique Views).**

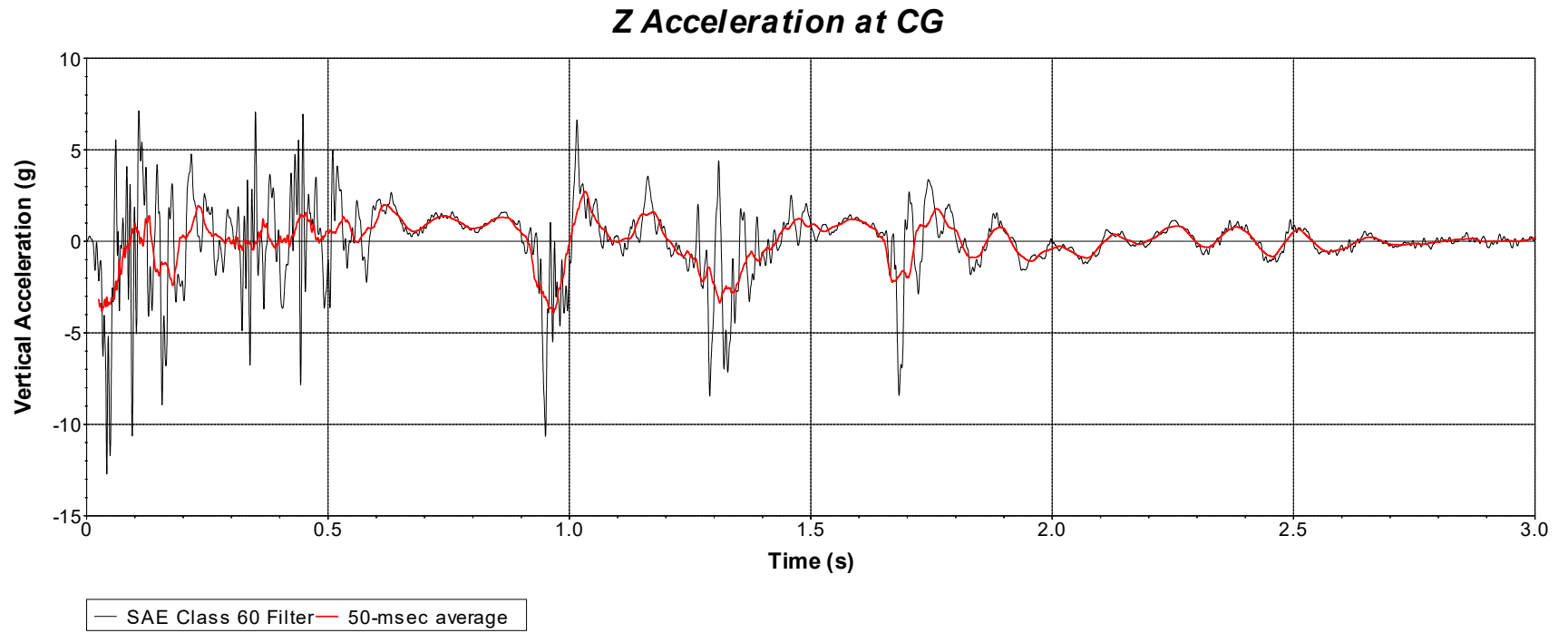
F.3.VEHICLE ACCELERATIONS



**Figure F.7. Vehicle Longitudinal Accelerometer Trace for Test 620281-01-2
(Accelerometer Located at Center of Gravity).**



**Figure F.8. Vehicle Lateral Accelerometer Trace for Test 620281-01-2
(Accelerometer Located at Center of Gravity).**



**Figure F.9. Vehicle Vertical Accelerometer Trace for Test 620281-01-2
(Accelerometer Located at Center of Gravity).**

